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Making Sense of Interaction Using a Model-Based Approach

by

Parisa Eslambolchilar, B.Eng., M.Eng.

Supervisor: Dr. Roderick Murray-Smith

Doctor of Philosophy

Hamilton Institute/Department of Computer Science

National University of Ireland, Maynooth

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Dedicated to my parents for all their love and support.

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Abstract

This thesis provides a theoretical method for developing and designing human computer interaction based on a continuous control process on mobile computing devices. This view provides a tight coupling between the user and system based on a continuous exchange of input/output dynamic information over a period of time, where continuous feedback from the display (visual/audio/haptic) influences the user's actions as more information becomes available and changes the user's perception. The proper representation and modeling of conceptual models in the interaction -via state-space model- and the explicit analysis of human behaviour and adaptability of the system to human behaviour -in the form of dynamic systems and probability theory are inherent to this framework.

This framework supports continuous interaction techniques based on tilt inputs and multimodal outputs with handheld devices because one-handed control requires less visual attention and multimodality in the interaction can compensate for the lack of the screen space. The dynamic systems approach to the design of such continuous interactive interfaces allows the incorporation of analytical tools and constructive techniques from manual and automatic control theory, probabilistic models—and thus many of the techniques of machine learning—into the interface and integrating multimodality in a principled manner.

Methods are presented for displaying the state of a system (visual/audio/haptic) with appropriate representation of a pseudo-physical model, via state-space model. Specifically, the use of predictive audio/visual-feedback for auditory/graphical display in a period of interaction is described, and it is shown how predictive elements can be introduced into goal directed displays, considering gains and delays present in the interaction loop. The use of these techniques in simulating the system behaviour before the actual implementation, and tuning and testing the system parameters are illustrated.

Viewing human behaviour as a control process, a general framework for supporting human behaviour is developed, which supports intermittent interaction by smooth and natural dynamic mode switching. This is a probabilistic approach and not only applicable on small screen devices but also in many range of computing appliances. It provides general design guidelines for dynamic interactive systems based on models for the dynamic system, probabilistic language model and a probabilistic audio feedback.

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The glory of friendship is not the outstretched hand, nor the kindly smile, nor the joy of companionship; it's the spiritual inspiration that comes to one when he discovers that someone else believes in him and is willing to trust him with his friend.

Ralph Waldo Emerson (1803-1882)

Declaration

I hereby certify that this material, which I now submit for assessment on the program study leading to the award of Doctor of Philosophy in Computer Science is entirely my own work and has not been taken from the work of others save and to the extent that such work has been cited and acknowledged within the text of my work.

(Parisa Eslambolchilar)

Contributing Publications

Large portions of Chapter 4 have appeared in the following papers:

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If our designs are failing due to the constant rain of changing requirements, it is our designs that are at fault. We must somehow find a way to make our designs resilient to such changes and protect them from rotting.

*Robert C. Martin,
Design Principles and Design Patterns,
objectmentor.com, 2000*

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Chapter 1

Introduction

In this introductory chapter we highlight interaction with small screen computing devices. We discuss novel interaction methods and argue the need for a theoretical model of continuous interaction. We also provide an overview of the major contributions that will run through this thesis, highlighting the issues of control theory, human operator modeling and multimodality; and finally present an outline of the thesis.

This dissertation provides a theoretical method for developing and designing human computer interaction, with particular attention to small screen devices.

The next sections describe advantages and disadvantages of current interaction methods on handheld devices and motivate the principles which will be focus of this work.

1.1 Interaction with Small Screen Devices

As the popularity of cellular phones and in general handheld devices has increased rapidly in recent years, more and more computers are being used in mobile environment. Nowadays millions of people use mobile phones, and people carry them everywhere in their hand, pocket and bag. For many of us these devices are not perceived as computers, but rather as augmented elements of the physical environment (Streitz, 2001). Therefore, interaction shifts from an explicit paradigm, in which the user's attention is on computing, towards an implicit paradigm, in which interfaces themselves drive human attention when re-



Figure 1.1: Different models of portable computational appliances.

quired (Schmidt, 2000). However, current interface design methods for portable computational “appliances,” such as handheld devices (Personal Digital Assistants (PDAs), most notably the Palm series of handheld devices) and the recent wave of electronic books or e-books, for example SONY (2005) (Figure 1.1), follow the conventional design pattern for desktop computers, which interact with the user via a large display, a mouse and a keyboard.

Fishkin et al. (2000) have identified and summarised features of these new devices as (a) “portability” and “graspability”, (b) “supporting a limited set of specific tasks”, (c) “embodiment, i.e., the work materials are stored inside the devices”, (d) “The device casings are physically designed to make these tasks easy and natural to do”, (e) “The devices are metaphorically related to similar non-computational artifacts.”

For example, mobile phones (Figure 1.1(c)) are light, small, we can hold them in one hand, carry them in the pocket and new phones have touch screen (e.g., iPhone). Usually mobile phones have a phone book, calendar, and reminder list, for example, Nokia 66 series have a calendar organiser and to-do lists. The user’s calendar is in the phone, so the phone is their calendar.

In order for a mobile device, such as a 3Com Palm PilotTM (Figure 1.1(b)), to provide a “mobile office” (Fishkin et al., 2000), users need to be able to produce new data and view and browse the information space via peripheral devices.

1.1.1 Peripheral Devices for Handheld Devices

While the computational power of portable systems increases for every new generation being produced, there are still some concerns regarding Human-Computer Interaction (HCI) issues on these devices. In the literature of Mobile HCI, two main problems in the usability of mobile devices have been highlighted. First, text entry methods (i.e., there is still no way of entering text at a reasonable speed in these devices), second, limited screen size (Fishkin et al., 2000; Harrison and Fishkin, 1998; Norman, 1998).

The main idea behind the design of the mobile/smart phones is that people use them as mobile offices (Fallman, 2002b). Hence, users need to enter or edit text data and browse through a large information space. Large screen devices, for example desktop computers, provide enough screen space to open and handle several documents at once, and the keyboard and mouse are used as input tools. In comparison, small screen devices, for example HP Pocket PCs running windows CE, do not have a physical keyboard and the keyboard has been replaced by a “stylus” pen and a pressure sensitive screen, which operate a virtual keyboard. The “stylus” pen obscures the small screen, hides the information the user wants to interact with, and engages both hands. Stylus input of characters and text recognition algorithms, for example graffiti text entry and hand writing recognition, are still crucial issues; because they both require the user to adapt to the device. They are fine for entering small amounts of text in almost every environment, but as soon as it comes to entering large amounts of text they are not very satisfactory (Ward et al., 2000; Fallman, 2002b; Williamson and Murray-Smith, 2005a; Partridge et al., 2002).

Automatic Speech Recognition (ASR) has become an important component of modern Human-Computer Interface (HCI), appearing as a natural way to interact with computers, improving the ergonomics of man-machine dialogues (Ris and Couvreur, 2004). However, the integration of accurate ASR is still difficult on small screen devices. The main problem comes from the hardware and the processor limitations in mobile phones, which generally have low processor power whose design rarely takes into account the real-time capabilities necessary for the

fast-running algorithms required for automatic speech recognition.

Traditional interaction design methods based on WIMP (Windows-Icon-Menu-Pointer) for desktop computers cannot be fully employed for portable devices. Therefore, these devices must be able to accept input and provide output via other means than WIMP. Such a means of achieving this can be gestures and audio/haptic. Thus, ways of facilitating novel interaction techniques which do not fully rely on speech recognition or traditional interaction techniques must be created on portable computing appliances.

1.1.2 Novel Interaction Methods

As described before, portable computing devices have been designed to be like a mobile office (Fallman, 2002b); Fishkin et al. (2000) argued that

“The physical interaction with [mobile] devices in comparison to a paper artifact, such as a notebook, is still quite limited; we can only write on these devices, but we cannot flip, thumb, bend, and crease its pages. We have highly developed dexterity, skills, and practices with such artifacts, none of which are brought to bear on computational devices. So, why cannot users manipulate devices in a variety of ways—squeeze, shake, flick, and tilt—as an integral part of using them?”

In the past ten years many researchers have focused on tilt-based inputs and audio and haptic outputs in Mobile HCIs (Dong et al., 2005; Fallman, 2002a,b; Harrison and Fishkin, 1998; Hinckley et al., 2005; Oakley et al., 2004; Partridge et al., 2002; Rekimoto, 1996; Sazawal et al., 2002; Wigdor and Balakrishnan, 2003). The results of these studies have proved that one-handed control of a small-screen device needs less visual attention than two-handed control, and that multimodality in the interaction can compensate for the lack of screen space.

Such novel interaction techniques with computers and handheld devices are examples of interactive dynamic systems, and the development of these systems explores a range of possible solutions for overcoming some problems of interaction design on computing devices, including the limited sources of input/output media, adaptability, predictability, disturbances and individual differences. We should include dynamics because we experience our environment in the way we

want it by our actions or behaviour. Thus we control what we perceive and while, in principle, interaction with handheld devices is rich in the variety of tasks supported, from computation and information storage to sensing and communication, we are dependent on the display of feedback (either visual, audio or haptic) to help us pursue our changing goals. In such dynamic systems, feedback influences the user's actions as more information becomes available (Faconti and Massink, 2001).

The concept of “*Continuous Interaction*” (Doherty and Massink, 1999) was brought about by advances in technologies in the past 15 years. Novel interaction techniques, gesture recognition, audio and haptic devices, provide a tight coupling between the user and the system based on a continuous input/output exchange of dynamic information, which happens over a period of time and we cannot model this coupled human-system interaction as a series of discrete events and static models (Doherty and Massink, 1999; Faconti and Massink, 2001). In continuous, dynamic interactive systems, the most important issue is the system's adaptability to user behaviour and dealing with sensing different inputs in real-time, coupled activities and additionally providing quick and rich information to the user (Faconti and Massink, 2001).

1.2 Human-System Interaction Model

What distinguishes interactive systems from other classes of system is the user, and the general focus of research in interactive systems has been the need to accommodate the user, and specifically the “usability” of the system. One area of research within this has been concerned with the development of models of interactive systems, and sometimes of the user, in order to analyse the behaviour of the user and the system.

At the human-computer interaction level we can distinguish four categories of I/O modalities (or channels), as illustrated in Figure 1.2 (Clow and Oviatt, 1998; Schomaker et al., 1995). The “*Human Output Channels*” and “*Computer Input Modalities*” define the input flow, while the “*Computer Output Media*” and

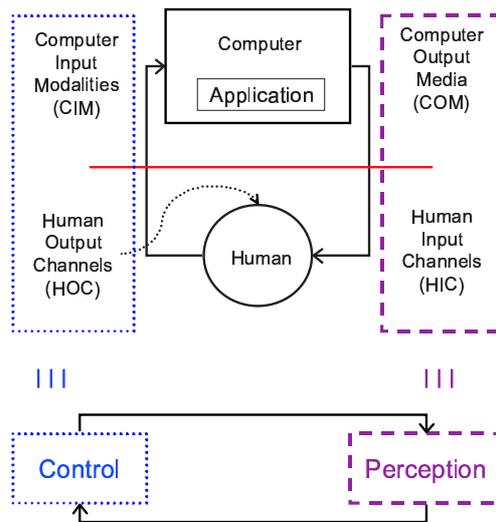


Figure 1.2: Human-System interaction model. Adapted from Schomaker et al. (1995).

“*Human Input Channels*” define the feedback flow. A more familiar terminology for interaction designers is “(*sensorial*) *feedback*” for computer output media and “(*modal*) *input*” for computer input modalities.

The two processes involved at the human side of the interaction are perception and control (Figure 1.2). Perception refers to the human input channels, i.e., visual, auditive and somatic (haptic, olfactory, gustatory, vestibular) (Schmidt and Lee, 2005; Schomaker et al., 1995) and computer output media. Control refers to the human output channels, i.e., gestures, speech and gaze (Schmidt and Lee, 2005; Schomaker et al., 1995) and computer input modalities. The dotted line accounts for I/O channel coupling of the human information processing system. Two streams of information complete the human-system interaction loop: the user receives feedback from the system through “*computer output media (COM)*” while the computer gets input information from the human output channels through computer “*input media (CIM)*” (Popescu et al., 2000). Something to note about the feedback the user receives from the system is that the computer output media and human input channels might be mismatched or subject to disturbances.

“*Multimodality*” is the quality of our body which allows more than one modality (channel) to be used during human-computer (in general, human-human

/ environment) interaction. In a multimodal computing system the user controls and communicates with computers via several modalities such as voice, gesture, gaze, visual, auditory, and haptic. These new environments are a great challenge for the future of the Human Computer Interaction studies, specially in portable computational devices. More senses (vision, hearing and touch) and more means of expression (gesture, facial expression, eye movement, speech) can be involved in interaction from the human side with respect to traditional WIMP based applications (Cohen, 1999; Cohen et al., 1999; Flanagan et al., 1999).

A wide variety of novel sensors, inertial sensors, light and pressure sensors and many others, create the potential for new methods of interaction with all range of computing devices and in different contexts. These sensors also have different information capacities, delays, bandwidths and support different modalities. Designers of interfaces which use these devices need a model to create usable communication media (CIM and COM) as well as supporting human/device capacity and human behaviour. Current models are severely limited: for example, Fitts' law predicts the time required to rapidly move from a starting position to a final target area but cannot make any predictions about human behaviour or how to get to the target. Furthermore, this model is only applied to untrained movements in a single dimension using visual display. Moreover, it is unclear whether other communication channels, for example audio, are sufficiently similar to the visual channel for Fitts' Law to be applicable (Friedlander et al., 1998).

1.3 A Theory for Designing Interaction

Beaudouin-Lafon (2004) has argued:

...if we are to create the next generation of interactive environments, we must move from individual point designs to a more holistic approach. We need a solid theoretical foundation that combines an understanding of the content of use with attention to the details of interaction, supported by a robust interaction architecture.

This characteristic has been described as “*designing interaction*” rather than *designing interfaces*, which simply means “*to control the quality of the inter-*

action between user and computer; because interfaces are the means, not the end” (Beaudouin-Lafon, 2004).

Physics, chemistry, and in general natural sciences are established on a base of solid and falsifiable theories to analyse, understand and control a phenomenon (Beaudouin-Lafon, 2004). Many successful computer interfaces have been designed and developed based on many experimental tests over a considerable amount of time but there is no solid and falsifiable theory to generalise those experimental results even to similar interfaces (Beaudouin-Lafon, 2004; Thimbleby, 1990). Additionally there is no theory of continuous interaction for designing and developing interfaces based on dynamic systems, continuous technologies and multimodal integration (Faconti and Massink, 2001).

Currently, there are few theoretical frameworks for interaction. For example, a few theories in psychology which provide insights into human behaviour have also been applied in designing interfaces (e.g., Fitts’ law). Also, there are many physiological models of human body motion (Schmidt and Lee, 2005). These models are incomplete in that they only focus on the human in the interaction while the coupling between the user and the system has not been taken into account. However, models established based on mathematics and dynamics, for example “*control theory*” have been overlooked in HCI research.

In 1970 William Powers suggested (Powers, 1989, 1992) that many kinds of behaviour can be described as continuous control problems, and he showed that this viewpoint provides a method for the estimation of a subject’s intention interacting with a computing system. He gave several examples which show that for identifying controlled variables in an interaction we can apply disturbances, directly or otherwise, to variables which are under the user’s control. If these variables are corrected by the user after applying disturbances, then those variables are assumed to be controlled. Based on the solid evidence Powers provides in his work he argues that “*control theory is a theory of behaviour.*”

A branch of control theory that is used to analyse human and system behaviour when operating in a tightly coupled loop is called *manual control theory* (Jagacinski and Flach, 2003; Poulton, 1974). The theory is applicable of to a wide

range of tasks involving vigilance, tracking and stability and creates a framework for modeling dynamic systems. The general approach followed in manual control theory is to express the dynamics of the combined human and controlled element behaviour as a set of linear differential equations in the time domain, called *state-space* modeling (Poulton, 1974). A state space representation is the mathematical realisation of control theory. This representation provides a convenient and compact way to model and analyse systems with multiple inputs and outputs. Also, it can incorporate sensor noise, disturbance rejection, sensor fusion, changes in input/output devices, and calibration challenges.

Several models include human related aspects of information processing explicitly such as delays for visual process, motor-nerve latency and neuro-motor dynamics. Control theory can be linked to Fitts' Law (Fitts, 1954) by viewing the pointing movements towards the target as a feedback control loop based on visual input and the limb as a control element allowing most of Fitts' law results to be predicted by a simple control theory (Jagacinski and Flach, 2003).

Machine learning techniques and probability theory can potentially be coupled with control theory to classify and predict user behaviour in the interaction. Probability theory provides theoretical models for the classification of evidence and machine learning techniques provide algorithms for inference (MacKay, 2003). For example, a probabilistic classification of the likelihood of different models of user behaviour can be used to alter the dynamics of the controlled system, rendering the user's task easier.

Throughout this thesis we use dynamic system and manual control theory as a theoretical framework for the design and analysis of interaction between human and system, giving particular attention to instrumented handheld devices with multimodal feedback.

1.4 Thesis Aims and Contributions

The overall aim of this research is to create an interaction metaphor and provide a framework that designers can use to model system and user behaviour

and integrate them into multimodal human-computer interfaces. Additionally, this framework should be platform free and can be used for all computing devices from desktop computers to PDAs. This thesis uses manual control theory as a formal modeling approach to provide appropriate concepts to deal with issues of continuous interaction, human operator modeling, and human performance data analysis.

Using the continuous control dynamic system approach and manual control theory we can *simulate* the model and observe the behaviour of the system. This approach makes tuning and calibration a lot easier, especially when we use a higher degrees of freedom input; because we can find proper settings for the interface only by observing the behaviour of the simulated system before the actual implementation and test its stability when coupled with a manual control model of user behaviour. Using the theory, we can make consistent *conceptual models* (Liddle, 1996) using real-world effects such as haptic feedback of springs, viscous effects linked to motion in the liquid, or friction linked to speed of motion, which are easy to reproduce in a dynamic system, and we can choose to explicitly use these features to design the system to encourage interaction to fall into a comfortable, natural rhythm.

This thus provides a few hidden real “*affordances*” because the presence of feedback effects the usability and understandability of the system and lets the user experience them. The word *affordance* was invented by the perceptual psychologist Gibson (1979) to refer to the actionable properties between the world and an actor (a person or animal). To Gibson, affordances are relationships. They exist naturally: they do not have to be visible, known, or desirable. For example, in a tilt-controlled visualisation application running on a PDA, the tilt sensor allows tilting but this tilting must be a meaningful, useful action, with a known outcome. The application presents changes in the speed of scroll and degree of magnification according to tilt angles as a(n) audio/visual output to the user. Presenting the current status of the controlled variables via audio, vision or haptic to the user makes their action more clear and the design model (i.e., how the designer understands how the system works) more *visible* (Norman,

1999; Preece et al., 2002). Furthermore while there is a feedback the user can determine the relationship (*mapping*) between actions and perceptions (Preece et al., 2002). Lastly, the natural constraints of human hand motion add some *constraints* to the interaction. For example, a roll tilt angle of -200° is not a convenient angle for holding the PDA and looking at the screen.

The dynamic system approach has the potential to provide a very general framework for the development, analysis and optimisation of interfaces which induce complex, but convenient coupling among multiple states, in order to cope with few degrees of freedom in input. This approach concurs with the argument of Norman (1986) who stated that in an ideal interactive systems three interacting components, the design model, the system image and the user model, should map onto each other. The dynamic system approach helps to bring these three components close together by providing “*visibility*”, range of “*affordances*”, “*constraints*”, “*mappings*” and most of all “*feedback*”.

The theme that runs through the next chapters outlines the fundamentals of continuous control and manual control theory, and how it can be developed and extended to multimodal interaction. In the later chapters, we support our arguments by providing implemented examples from auditory to graphical user interfaces on handheld devices. The implementations have been specifically chosen to illuminate the most important principles to augment the more limited approach of, demonstrating only usability that is common in HCI research.

1.5 Thesis layout

The remainder of this thesis is organised as follows:

Chapter 2 introduces a new point of view to the analysis of behaviour proposed by William Powers, discusses the effect of this new definition in psychology and computing science and some of its applications in interaction design. This chapter will focus on *perceptual control theory* and its contribution to *motor control* and *designing interaction*.

Chapter 3 introduces continuous interaction as a requirement of interactive

systems to support natural human behaviour. The initial sections of this chapter introduces the basic definitions and terms of manual control theory for the analysis of the continuous aspects of the interface and human behaviour. Subsequently it addresses a framework of modeling notations and tools to drive design decisions during the development of interactive systems. Lastly, this chapter will consider control inputs for small screen devices.

Chapter 4 outlines model-based sonification and human perception and action when s/he is interacting with auditory interfaces on small screen devices using a tilt sensor. This chapter highlights the pros and cons of different audio feedback and control strategies in browsing the audio space and one possible way of improving performance based on models of human control behaviour in few example applications.

Chapter 5 presents a dynamic system interpretation of the coupling of internal states involved in speed-dependent automatic zooming (SDAZ), followed by testing of an implementation on a text browser on a Pocket PC instrumented with a tilt sensor. This approach to the design of a continuous interaction interface allows the incorporation of analytical tools to analyse and simulate the system behaviour before the actual implementation, calibration and tuning of the parameters, model generalisation and stability testing of the controller when coupled with a manual control model of user behaviour. It shows that the reference signal exists in control systems as an input and according to these reference variables the controller switches among different modes. Also, it is shown that a model-based sonification approach for the tilt-controlled SDAZ provides a general design guideline to add multimodal feedback to the interaction that also support intermittent interaction.

Chapter 6 introduces a continuous interactive system to support human behaviour in browsing a multilingual text based on a language model, focus-in-context method and manual control theory. It is argued that to design interaction we need models of key aspects of the process, here for example, we need models for the dynamic system, a probabilistic language model and a probabilistic model of an audio feedback space as an example of a multimodal approach to sensing

different languages in a multilingual text. This example illustrates a general framework, which brings the usefulness of quickened displays and prediction of user behaviour and the importance of multimodality in the intermittent interaction scenario, together along with the use of probabilistic model for classifying human behaviour in browsing tasks.

Chapter 7 concludes the thesis, reviews its contributions and outlines possible avenues of future work.

Chapter 2

Purposeful Behaviour, Motor Control and Analysing Interaction

Behaviour is often described as the computation of a response to a stimulus (Cisek, 1999). This description is incomplete in an important way because it only examines what occurs between the reception of stimulus information and the generation of an action. Powers (1989) has described behaviour as a control process where actions are performed in order to affect perceptions or actions are motivated by organic needs and they affect an organism's perception about their needs. This chapter will focus on perceptual control theory and its contribution to motor control and designing interaction.

2.1 Introduction

To control movement, multi-cell organisms developed a nervous system. This began when multi-cell organisms began to move. Movement is the only way we have of interacting with our environment, i.e., shaking hands, eating, drinking. We communicate with other people using speech, body gestures, and touch. From this viewpoint, the purpose of the human brain is to use sensory representations to determine future actions (Wolpert et al., 1999).

Movement takes many forms. Some forms can be classed as genetically defi-

ned movements, such as the way in which people control their limbs or the rapid eye-blink in response to a strong flashlight (Schmidt and Lee, 2005). A second form of movements can be described as “learned”—for example, those involved in controlling a car or operating a typewriter. These learned movements are often termed “*skills*”. They are not inherited and require long periods of practice and experience to be acquired (Schmidt and Lee, 2005). Skills are especially critical to the study of human behaviour, as they are involved in operating machines in industry, controlling vehicles, playing games, and so forth.

In this thesis we consider only the second category of movements or *skills*. We will be concerned with how these movements are controlled and can be modeled in interactive tasks with computing systems. Thus, in this chapter we look at the definition of motor control, the theory of living systems’ behaviour as a theory of system control and human behaviour and its contribution to perceptual control theory. The following section provides key definitions before progressing on to the detailed exposition of the control paradigm.

2.2 Background

This section introduces definitions for “motor control”, “control” and “behaviour” and their contribution to control systems.

2.2.1 What is Motor Control?

Brooks (1986) defines motor control as “*the study of posture, movement and functions of the mind and body that govern posture and movement.*” Thus, motor control models the complexity of any movement we perform for any task, for instance how we sit down, or walk.

2.2.2 What is Control and Control Systems?

Marken (1995b) has described control as “*the process of producing consistent results in the face of unpredictable disturbances.*” So any simple task, for example keeping a car in a lane in a highway on a windy day, is a control process. Control

refers to both a phenomenon and the theory designed to explain it.

Control systems are systems that control their actions or control what they perceive through their sensory systems. Thus we can classify all living organisms (and some non-living artifacts, such as thermostats) in the class of control systems (Marken, 1995b).

2.2.3 What is Behaviour?

Millikan (2002) defines behaviour as a biological function, which is “*fulfilled normally via mediation of the environment, or via resulting alterations in the organism’s relation to the environment.*” This definition distinguishes behaviour from physiological processes and allows other ways of interaction, which does not involve movement, to be behaviour, for example, emission of sounds, pheromone, changes of colour and so forth. Also, if human purposes are a species of biological purposes or proper functions, then human actions are behaviours (Millikan, 2002).

In spite of behaviour’s diversity, however, there is one obvious, and often ignored, characteristic of most behaviour: it *repeats* (Marken, 2002). The events that are labeled behaviour based on the definition presented by Millikan (2002)—lifting, walking, eating, writing—happen over and over again: there is regularity. Scientific psychology is built on the assumption that behaviour is *output* but Powers (1989, 1992) has argued that “*behaviour is not output but a controlled consequence of input: behaviour is control.*” Behaviour is control because the events called behaviour are consistent results of continuously changing effects produced, simultaneously, by the organism and the environment (Powers, 1989, 1992, 2005) and control theory is an explanation of the phenomenon of control, which is now called *Perceptual Control Theory (PCT)*. In the following section we look at the basic structure of controlled systems and their important functions, using riding a bicycle as an illustrative example.

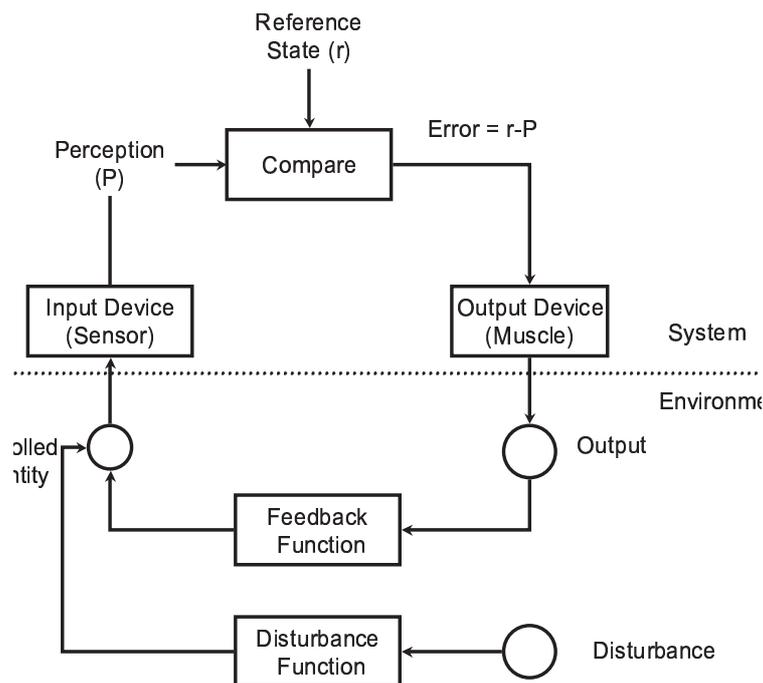


Figure 2.1: The basic control system describing any living system’s behaviour. Adapted from Powers (1989).

2.3 The Control System Architecture

A control system, as described before, can produce reliable and repeatable results in an unpredictable environment, i.e., in the real world. In the “*cause and effect*” point of view of behaviour it is hard to see reliable, reproducible end-results if the processes that lead to that result are unpredictably variable (Powers, 1992). In daily life, we do tasks a little differently each time because initial conditions or the environment changes. Control system tolerates variations in initial condition or the environment, either small or large, including disturbances. However, control systems have limitations like all physical systems, but their limitations are less restrictive than “*cause and effect*” point of view (Powers, 1992, 2005).

Figure 2.1 presents important functions of a generalised control system model. This model can involve any sensory input, i.e., audition, vision, and proprioception, and muscles as output. In the following sections we explain these functions in more detail under appropriate headings.



Figure 2.2:

Perceiving

The most important issue in a control system is identifying the “*controlled variables*” (Powers, 1989). A controlled variable should remain stable in the face of variability, i.e., noise and *environmental* effects. The situation is illustrated in Figure 2.2 which shows a controlled variable, q , whose value depends on system outputs (s) and environmental influences (e) (or disturbances). This implies some sort of sensor that can detect the state of the controlled variable and represent it as a signal inside the controlling system. It is shown as *sensor* box, the “*perceptual input function*,” in Figure 2.1 where the perceptual signal is at the output. The perceptual signal varies and its variations represent variations in the controlled variable. For example, the position of the bicycle in its own lane during a race is the controlled variable, where that position can vary continuously from far to the left to far to the right.

Comparing

The stabilised value of the controlled variable, q (Figure 2.2), is called its “*reference state*,” q^* . For an observer the reference state appears to be the value that the system is *trying* to maintain. Environmental effects (e) which would act to move q away from q^* have almost no influence since they are resisted by the system outputs. When there is control, the value of q is kept in the reference state, q^* , protected from the environment (Poulton, 1974; Powers, 1989).

Now, we can compare the difference between perception and reference signals. “*This difference indicates by its sign which way the discrepancy went, and by its magnitude how big the discrepancy was.*” The comparison function actually generates a physical signal representing the difference or error (Powers, 1989). In the example of riding a bicycle, the reference signal represents that sense of how the position should look in the lane and the perceptual signal represents how it

actually looks, and the cyclist is minimising the error between these two signals.

Acting

The output of the comparison function, or error, is transferred to the muscles to keep the bicycle in the lane by applying forces to the steer.¹ A positive error signal means that if the bicycle is too far to the right relative to the reference condition, then it should be connected to the motor signals that make the arm muscles twist the wheel to the left. The opposite should hold for negative error signals. These connections are always correct and applied in driving a car, bus and other vehicles. So “*if we could wire positive error signals to one set of muscles and negative error signals to the opposing set, and if we did not get the wrong sets hooked up, then the muscles would always respond in a way that tends to make the error signal smaller*” (Powers, 1989).

The “*Output Device*” box in the block diagram (Figure 2.1) represents this function. It converts the error signal into a physical effect on the environment.

The Environment

In riding the bicycle, the bicycle is part of the cyclist’s environment. Steering efforts applied to the steer and pedaling force generated by muscles applied to the pedals let the bicycle move forward and sideways. On windy days, the way the bicycle and the lane looks like changes, and it causes changes in the perceptual signal. So through a feedback connection, the “*environment function*” links the action of the control system back to its perception (Powers, 1989). In fact, the environment completes the closed loop of causation from perception, to comparison, to action, and back to perception again, and this closed loop makes the control system a fundamentally different organisation from either conventional stimulus-response or cognitive behaviour theory.

¹It is also called counter steering. Counter steering is the technique of changing the direction of travel of the motorcycle by gently steering the bike in the opposite direction to which the cyclist wants to go. If s/he wants to turn right s/he pushes gently on the right side of the handle-bar. Or in other words subtly steer left.

The Disturbance

Controlled variables are affected not only by the actions of the control system via a closed loop of action and perception, but also by other influences. For example, only the position of the bicycle in its lane is affected by anything that can apply a sideward force to it, like a wind or a ramp in the road. In Figure 2.1, the sum of all such independent effects has been presented as a single equivalent disturbance, and it affects directly the controlled variable. *“No model of a control system is complete without a representation of the disturbance, because it is the way actions vary in response to disturbances that provides strong evidence that we are dealing with a control system”* (Powers, 1989).

In this section we provided a general and basic structure for the controlled systems using a bicycle as an example. This simple example can be extended to computing devices (which will be discussed in more detail in Chapter 3). With computers, humans are no longer exposed to the physical world governed by the laws of physics, however we can make consistent *“conceptual models”* using real-world effects based on pseudo-physical models.

2.4 Interaction Model and Motor Control

One important issue in the interaction design is that the interface should match with the users’ capabilities or conceptual models.

2.4.1 Conceptual Models

In Chapter one we discussed a need for a solid and falsifiable methodology for designing interaction. As Liddle has highlighted (Liddle, 1996), *“the most important thing to design is the user’s conceptual model. Everything else should be subordinated to making that model clear, obvious and substantial.”* By a conceptual model he meant:

...a description of the proposed system in terms of a set of integrated ideas and concepts about what it should do and look like, that will be understandable by the users in the manner intended (Preece et al., 2002).

One popular way of describing conceptual models is in terms of interaction metaphors. By this is meant a conceptual model that has been developed to be similar in some way to *aspects* of a physical entity (or entities) but that also has its own behaviours. Such models can be based on an activity or an object or both, for example spreadsheets and search engines (Preece et al., 2002). The search engine tool has been designed to invite comparison with a physical object – a mechanical engine with several parts working – together with an everyday action – searching by looking through numerous files in many different places to extract relevant information (Preece et al., 2002).

Dynamic control theory models the conceptual approach a user brings to an interaction based on pseudo-physical models which are familiar to the user from real-world effects such as the haptic feedback of springs, viscous effects linked to motion in the liquid, friction linked to speed of motion, or weight of mass which are easy to reproduce in a dynamic system as a set of mass-spring-damper. These models provide a general framework for guiding designers and developers to create interactive systems. Unlike ergonomic rules, which are not conceptual and are often limited to post-hoc evaluation of a design, these interaction models are usable from the early stages of the design and the final behaviour of the model can be simulated and observed before the actual implementation and is therefore proactive.

2.4.2 Instrumental Interaction

We use tools, instruments and devices to control, interact and operate on the physical objects rather than using our bare hands (Kelley, 1968). In modern computing scenarios we are not manually controlling power flows, but controlling information flow. “*Instrumental interaction*” (Beaudouin-Lafon, 2000) is an interaction model that operationalises the computer-as-tool paradigm. It is something to extend human powers: a piece of technology or applied intelligence for overcoming the limitations of the body (McCullough, 1998). Two important issues in instrumental interaction are: (a) how is the relationship between the instruments and the objects those instruments operate on (Beaudouin-Lafon, 2004;

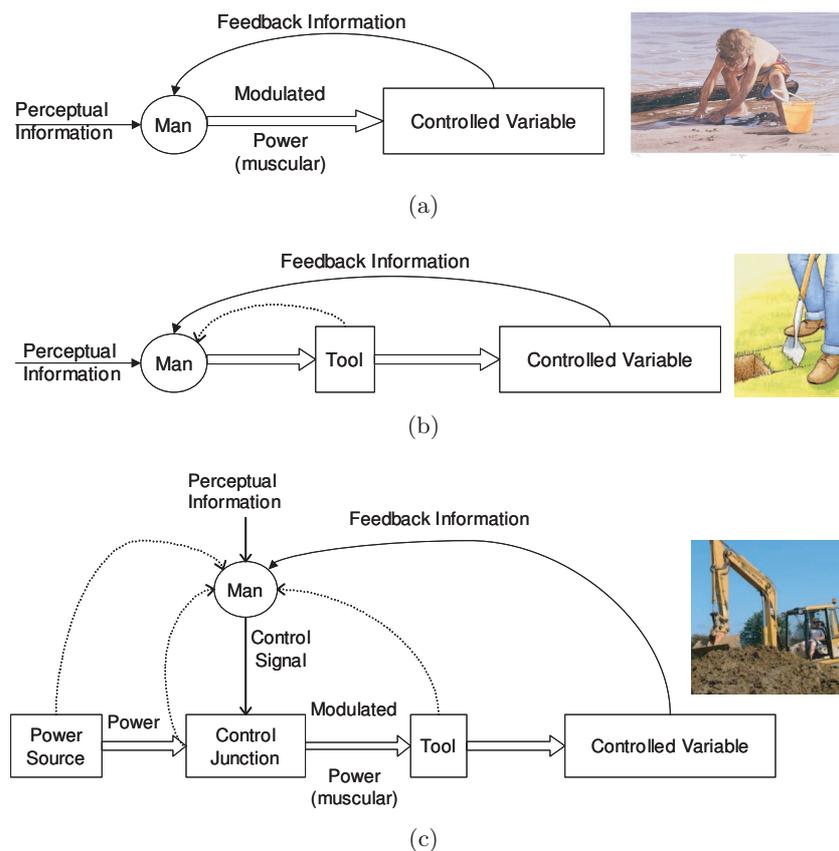


Figure 2.3: Modification of the environment by means of: (a) direct muscle power, (b) a tool, and (c) a powered device. Adapted from Kelley (1968).

Heckmann, 2005), for instance, creating, transforming, selecting, or navigating the object. (b) how is the relationship between the user and the instrument he is using (Beaudouin-Lafon, 2004)? Some instruments, like paint brushes, are held in the hand. Some, like scrollbars, sit on the screen. In either of these taxonomies the tool is “a moving entity whose use is initiated and actively guided by a human being, for whom it acts as an extension, toward a specific purpose and continuous control is at the very heart of tool usage in the interaction between the human and tool” (McCullough, 1998) (Figure 2.3).

The concept of instrumental interaction highlights designing interaction rather than just interfaces, but it also needs to address sensory-motor performance, i.e., matching the interface with the users’ capabilities (close loop of action and perception), and “situated interaction,” i.e., supporting the user’s activities in the context of use (Beaudouin-Lafon, 2004; Heckmann, 2005). We discuss this part in more details in the next few lines.

Situated Interaction

The definition of situated interaction depends on the interaction model. For example, in the desktop computing devices, a user interacts locally with a computer, but in the mobile computing devices, a mostly moving user interacts with a small portable device and has to cope with various contextual distractions, for example ambient noise. The goal in situated interaction is to combine a range of techniques for designing interactive systems that are better adapted (and adaptable) to their context of use. It also provides a range of physical and perceived affordances which can be discovered by the user via feedback and a mutual relationship between the perception and action (McCullough, 2001). For example many objects in everyday environments possess inherent degrees of freedom that have to be actuated to perform their function. Such objects include door handles, doors, drawers, and a large number of tools, such as scissors and pliers (Katz and Brock, 2007; Thimbleby, 2001).

2.4.3 Examples from HCI

As discussed in Section 2.4.2, we use tools to control. A software tool gives visible form and physical action to a logical operation. Like a physical tool it modifies the effect of the hand, which it accomplishes by modifying the functionality of the visible cursor that we operate with the physical pointing device (i.e., the mouse). For example, a paint software tool offers pencils, brushes, and so forth for applying colour to a surface. This plays on the fact that a tool can be conceptual, and indirectly controlled. Whether direct or indirect, what matters is manipulation (Beaudouin-Lafon, 2000, 2004; McCullough, 1998).

Selection without the use of pointing is of particular interest because of challenges faced in designing interaction with hand-held devices and wearable computers, where input and output are often limited, or only unconventional means of interaction are available. These devices might be instrumented with sensors for which pointing may not be a natural method of selection, (e.g., accelerometers), or may have displays (such as audio displays) that are not suited to pointing. The display may also just be too small to allow convenient pointing.

Dasher is an information-efficient text-entry interface, driven by natural continuous pointing gestures. Moreover, *Dasher* is a competitive text-entry system wherever a full-size keyboard cannot be used (Ward, 2001; Ward et al., 2000). *Dasher* offers a dynamic selection technique based on continuous one dimensional movement. *Dasher* is a very efficient entry system, especially where control is difficult, or the language or other structure is unfamiliar, however the dynamic layout of letters reduces the opportunity for learning highly optimised strategies for entry, and requires continuous attention to control.

Williamson and Murray-Smith (2004b), (Williamson, 2006; Williamson et al., 2007) designed an example interface built on methods from perceptual control theory and dynamic systems. They presented a method for performing selection tasks based on the continuous control of multiple, competing agents who try to determine the user's intentions from their control behaviour without requiring an explicit, visible pointer. In this example, there are several objects on the screen and each object has a position to which a small white noise is added (disturbance) and the displayed position of the object is the sum of the object's position and the mouse position. The variance of this sum and the variance of the object's position in each time step is calculated. The probability of each object i being selected is the ratio of the variance of the sum the object's position and the mouse position to the variance of the object's position. The object with higher probability is selected. These methods are close to those used in perceptual control theory, proposed by Marken (1995b) and Powers (1989). This earlier work suggested that many kinds of behaviour can be described as continuous control problems, and Powers proposed that this viewpoint provides an empirical method for the estimation of a subject's intention. This can be done by designing an experiment to identify which variables the subject is controlling, by introducing changes (disturbances in control theory nomenclature), directly or otherwise, to variables which are under the subject's control. Variables for which disturbances are corrected are assumed to be controlled by the subject.

Furthermore, there is an evidence that correct display of uncertainty lead to appropriately regularised control behaviour in human motor control, in reaching

and targeting actions. For example, [Kording and Wolpert \(2004\)](#) showed that in a target acquisition task, where a disturbance was artificially added to the user's control input, uncertain display (Gaussian point clouds) lead to behaviour that was consistent with Bayesian integration of the uncertain sensory inputs and prior beliefs about the system. Modeling human operator, such as those proposed in ([Jagacinski and Flach, 2003](#)), which incorporate Kalman filters imply that uncertainty is modeled in user control behaviour.

2.5 Modeling Perceptual-Motor Performance

From the literature on perceptual-motor performance ([Powers, 1989, 1992, 2005](#); [Schmidt and Lee, 2005](#)), the time taken for the user to complete a task in response to a stimulus is divided into three components: (a) “*perceptual delay*,” which is the time taken by the user to notice that the stimulus has occurred. It is also affected by the modality, for example, audio, vision or tactile, (b) “*decision making time*”, which is based on both the number of possible stimuli, and on the possible responses to the stimulus, (c) “*movement time*”, which is the time taken by the user to carry out the response which will be described later in this section. It is this movement time which many HCI studies focus on.

2.5.1 Movement Time

“*Movement time is the time from response initiation to the end of the response*” ([Schmidt and Lee, 2005](#)). Here, speed of movement becomes important. One of important functions in the movement time is the “*speed-accuracy*” trade-off function and is considered in situations in which the goal is to move a limb (or some other effectors) as quickly as possible to achieve a target, doing so with a minimum number of errors ([Schmidt and Lee, 2005](#)). For example, typing, moving a mouse-driven cursor to a desktop icon, and numerous other activities that require rapid movements to push, touch, or displace an object.

A very well known, and widely applied rule for the estimation of motor time is Fitt's Law:

2.5.2 Fitts' Law

Fitts' law models human movement and predicts the time required to rapidly move from a starting position to a final target area, as a function of the distance to the target and the size of the target. This model was introduced by Paul Fitts (1954), and many researches since then have been carried out in applying Fitts' law to evaluate the human-computer interfaces.

Fitts' law in its general form, sometimes called the Shannon formulation (MacKenzie and Ware, 1993), states a logarithmic relationship between the movement time to the target and the ratio of the distance to the target to the size of the target.

$$MT = a + b \log_2\left(\frac{D}{W} + 1\right) \quad (2.1)$$

where MT is the average time taken to complete the movement, a and b are empirical constants, and can be determined by fitting a straight line to measured data, D is the distance from the starting point to the centre of the target, W is the width (size) of the target.

$ID = \log_2\left(\frac{D}{W} + 1\right)$ is the index of difficulty (measured in bits), the amount of information necessary to specify the target width (W) relative to the distance (D) to be covered. From the equation, we see a speed-accuracy tradeoff associated with pointing, whereby targets that are smaller and/or further away require more time to acquire (Jagacinski et al., 1980; MacKenzie and Ware, 1993).

Is Fitts' Law successful in all HCI application?

Fitts' law is a well-studied model of human psychomotor behaviour (Bootsma et al., 2004; MacKenzie, 1991). Fitts' law's first HCI application was by Card et al. (1978), who used the index of performance ($IP = \frac{1}{b}$) to compare the performance of different input devices, with the mouse coming out on top. Fitts' law has been shown to apply under a variety of conditions (a , b , and IP have different values under each of conditions), with many different limbs (hands, feet, head-mounted sights, eye gaze), different input devices (mouse, joystick, track-ball, keyboard, etc), different users (young, old, and mentally disabled).

Recently, several researchers have tried to “beat Fitts’ law” or obtain a better pointing performance than in the real world. For example, McGuffin and Balakrishnan (2002) show that when the target expands as the cursor approaches it, the performance depends on the target’s final size even when the target only begins expanding as late as after 90% of the distance to the target. An example of expanding targets is MacOS dock (Apple, 2002), however Zhai et al. (2003) show that relative motion of the targets makes targeting difficult. “*Semantic pointing*” or manipulating the control-display ratio was introduced by Blanch et al. (2004). They argued that the visual size of targets can be independent from their size in motor space. A visually-small target can be made easier to point to, for example, without the user even noticing the manipulation. In a joint work Beaudouin-Lafon and Guiard (Guiard et al., 2001), have pushed the limits of Fitts’ law even further. Pointing with one’s arm in physical space is limited to an index of difficulty of about 10 bits (1mm at a 1m distance). However, on a computer, and with the help of zooming, one can point to targets that are arbitrarily small at an arbitrarily-long distance.

Fitts’ law has proven to be an invaluable tool in studying interaction as a sensory-motor phenomenon (Beaudouin-Lafon, 2004). This model is restricted, however, because it has been designed to evaluate pointing actions in a single dimension of movement not in two dimensions (MacKenzie and Buxton, 1992); Additionally it describes untrained movements only, not skilled movements. It is also unclear whether for auditory interfaces this communication channel is sufficiently similar to the visual channel for Fitts’ Law to apply (Friedlander et al., 1998). With visual feedback, the user is constantly aware of the exact position of the target. In contrast there is no analogy in the non-visual model. With auditory feedback, the user can only approximate the position of the target; given the distance s/he has already moved the pointer and the speed at which the pointer is moving (see Chapter 4).

Aside from these drawbacks, Fitts’ law remains one of the most reliable human-computer interaction predictive models, joined more recently by the Accot-Zhai steering law (Accot and Zhai, 1997, 1999, 2001, 2002), which is derived from

Fitts' law. There are other laws in interaction design, for example Hick's law or the Hick-Hyman law (Hick, 1952; Hyman, 1953), Moore's law (Moore, 1965),² Tesler's law³ and Poka-Yoke principle (Shingo, 1986),⁴ but few studies have been done to apply them in human-computer interaction.

2.6 Fitts' Law and Control Theory

Fitts' Law uses the logic of information theory to account for both movement time and the associated error rates (Mackinlay et al., 1991). The speed-accuracy tradeoff seen for continuous movements is qualitatively very similar to that seen for reaction times (MacKenzie and Ware, 1993). This suggests that using the information statistic taps into an invariant property of the human controller. Also, Fitts' model of movement time uses an information metric. This metric is very useful for characterising the noise properties of a communication channel. The arm is viewed as a channel through which an intention to move to a specific location is communicated. The output variability reflects the signal-to-noise properties of the communication channel. However, the problem with this metaphor is that it ignores kinematics. Kinematics is a branch of dynamics that deals with aspects of motion apart from considerations of mass and force (Webster dictionary definition). It provides a description of the movement, independent of the forces that causes the movement.

Crossman and Goodeve (1983) were among the first researchers to consider control theoretic descriptions as an alternative to Fitts' information theoretic model of human movements. They described a first order continuous control system where the instantaneous velocity is proportional to the current error (i.e., the distance left to traverse). The settling time for this system yields Fitts'

²Moore's law is extended to wireless hardware on mobile devices. Hardware components in such devices have been decreasing in size considerably and can nowadays be placed on small microphones. As the size gets smaller the traditional interaction design techniques become more difficult to be fully applied on small computing appliances.

³For any process there is a base level of complexity that is inherent to that process. Once the designer hits that base, he cannot simplify the process anymore.

⁴Poka-Yoke principle roughly means "mistake-proofing," or designing constraints into products that prevent users from making mistakes—and ultimately into influences, or approaches such as Direct/Indirect Manipulation, Feedback/Feed-forward.

law. Jagacinski and Flach (2003) explain and illustrate it fully with respect to movement time. That both the limited capacity communication channel and the first-order lag metaphors are equivalent when modeling the data from Fitts' experiments. However the first-order lag is a stronger model, because there are more ways to falsify it. The first-order lag predicts the time history of the movement time. Thus, this model can be rejected if the time histories for human movements differ in significant ways from those that would be generated by the first-order lag. The information-processing channel metaphor does not make any predictions about time histories.

Langolf et al. (1976) describe a second-order underdamped control system whose settling time also corresponds to Fitts' law. In addition, Langolf et al. (1976) describe a discrete response model, originally developed by Crossman and Goodeve (1983). Jagacinski and Flach (2003) (chapter 6) show the second-order system can be used to predict Fitts' Law and for validity checking.

Bootsma et al. (2004) compared Fitts' law with continuous control models. They realised changes in ID (see Section 2.5.2 on page 26) give rise to systematic changes in the kinematics patterns that determine MT in Fitts' law tasks. In a reciprocal aiming task, participants produced a series of back-and-forth movements between targets with different index of difficulties (ID s). The resulting pattern of movement had a continuous, sinusoidal form: The movement pattern was harmonic in low ID s. When task difficulty increased, systematic deviations from harmonicity came to the fore. Over the past few years, Bootsma et al. (2004) explored the typical pattern of change in the kinematic forms, as found in a variety of settings, and sought to capture its characteristics through dynamical systems modeling. In their experiments averaging over (half) cycles allowed detection of the regularities in the pattern of movements produced. They developed a method of analysis based on both qualitative inspection and quantification of the forms produced. Portraying the data, Hooke and Phase portraits, (after averaging over consecutive cycles) proved to be particularly useful and, Bootsma et al. (2004) introduced them using a pure sinusoidal signal as an exemplary case. They concluded that observation of the shape of the Hooke portrait of a signal

allows an assessment of the nature of the dynamics that may be hypothesised to underlie the movements observed. It is with this logic that they addressed the patterns observed in a reciprocal aiming task under different levels of task difficulty. They showed that a limit-cycle model captures all these changes and provided further evidence for the organising role of the informational flow in task space by differentially manipulating task space and effector space.

These theoretical and empirical findings about the predicting the time-histories of the movement time and the structure of the aimed movement are also applicable to human-computer interaction to improve the efficiency of the interface.

2.7 Conclusions and Summary

Studying interaction at the level of a sensory-motor phenomenon has led to important advances in HCI, for example Fitts' Law provided a scientific basis to evaluate the performance of interaction techniques. However, these results must be taken with care since they are easy to misuse or overgeneralise (Gibson, 1979; Norman, 1999). Controlled experiments only simulate real situations and they run in a restricted environment and take into account only untrained movements in order to operationalise the phenomenon being observed.

This chapter argues that computer as a tool extends human powers and continuous control is at the very heart of tool usage in the interaction between the human and tool. Yet the applications of control theory in *designing interaction* are still considered novel and, to some, revolutionary (Powers, 1989).

A control system can produce reliable and repeatable results in an unpredictable environment. Control theory can model human information processing and is an analytical tool for partitioning and modeling human performance (Jagacinski and Flach, 2003). Consistent behaviour patterns are created by variable acts, and generally repeat only because detailed acts change. The stimulus-response tradition is incapable of dealing with such novel situations.

Control theoretic analysis is able to model movement time with the same accuracy as information theory (Bootsma et al., 2004; Jagacinski and Flach, 2003).

However, control theory allows predictions about the space-time properties of movements that cannot be addressed using information statistics. The language of control theory also provides a perspective for looking at the world in a way that enhances our appreciation and understanding of the dynamic coupling of perception and action with biological systems. The essentials of the theory as will be discussed in more details in the following chapter are simple but “*this does not mean control theory deals only with simple behaviour. Control theory is a theory of behaviour*” (Marken, 1995a).

Chapter 3

Continuous Interaction and Human Behaviour Control

This chapter introduces continuous interaction as a requirement of interactive systems to support natural human behaviour. This development requires some term definitions from manual control theory for the analysis of the continuous aspects of the interface and human behaviour. Subsequently it addresses a framework of modeling notations and tools to drive design decisions during the development of interactive systems.

3.1 Introduction

In novel interaction techniques, i.e., gesture recognition, audio/haptic feedback, continuous interaction is at the heart of the interaction between the human and system; because the human is tightly coupled to the computing system via interaction over a period of time and exchange continuous input/output of dynamic information at a relatively high speed with the system (Doherty and Massink, 1999).

In the following sections we review manual control in brief and how we may bring ideas from manual control in novel interactions with small screen devices and modeling human operator.

A key reference in this Chapter is (Jagacinski and Flach, 2003). We refer to that to clarify and explain basic techniques they discuss about control theory

and human operator models in the context of design and development of Human-Computer Interaction.

3.2 Manual Control

Manual control theory was originally developed by feedback control engineers for modeling tasks such as tracking for anti-aircraft gunners, and vehicles of all kinds, including aircraft, spacecraft (Baskett, 2000; Blakelock, 1991), automobiles (Kiencke and Nielsen, 2000), bicycles, and ships (Fossen, 1994). However, the theory is applicable to an even wider range of tasks such as vigilance, tracking, and stabilising. The theory, particularly that branch developed from control theory, has been refined to a very high degree over the years. In general an approach that is used to analyse human and system behaviour when operating in a tightly coupled loop is manual control (Brogan, 1991; Kelley, 1968; Poulton, 1974). The general approach followed in manual control theory is to express the dynamics of the combined human and controlled element behaviour as a set of linear differential equations in the time domain. In order to obtain a solution, this set of equations is transformed into a set of linear algebraic equations in the complex frequency domain by well-known mathematical techniques. The focus of the approach is on the perception and transformation of signals representing, for example, the actual and desired state of a process. Motor performance is viewed in terms of information transmission, with inaccuracy viewed as additive noise (this was described in Section 2.6 on page 28). The following sections will explain the key definitions in manual control theory, which are important in designing interaction.

3.2.1 Discrete and Continuous Control

“Discrete movements are those with a recognisable beginning and end” (Schmidt and Lee, 2005). Kicking a ball, pressing a button, and shifting gear in a car are examples. The end of the movement is defined by the skill in question not arbitrarily by the time at which an observer ceased examining it. Discrete skills can

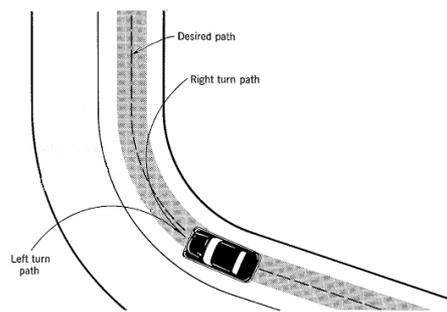


Figure 3.1: An example of a continuous skill, steering a car. From Kelley (1968).

be very rapid; but they can also require considerable time for completion, as in writing one's signature (Schmidt and Lee, 2005).

“Continuous movements are defined as those that have no recognisable beginning and end, with behaviour continuing until the movement is arbitrarily stopped” (Schmidt and Lee, 2005). Examples are swimming, running and steering a car. *“Continuous tasks tend to have longer movement times than do discrete tasks. But this not should be taken as the basis of their definition”* (Schmidt and Lee, 2005).

A common class of continuous skill consists of tracking tasks. The tracking task is characterised by a pathway (or track) that the individual intends to follow and a device that the person attempts to keep on the track via certain limb movements. In steering a car, for example in Figure 3.1, the track is the road, and the device is the car (Poulton, 1974). Two kinds of tracking tasks that are used in motor behaviour research will be discussed later in this section.

3.2.2 Open and Closed Loop Control

“In open loop control, the environment is constantly and unpredictably changing and the user cannot effectively plan the entire movement in advance” (Schmidt and Lee, 2005). So in this control method only the target signal is available to the user; thus there is no ability to account for noise or environmental interference (Figure 3.2a). One of the main disadvantages of this type of controller is the lack of sensitivity to the dynamics of the system under control. As an example, consider cruise control (Bosch, 2003; Davis, 2004). In this case,

the system is a car. The goal of cruise control is to keep the car at a constant speed. Here, the output variable of the system is the speed of the car. The primary means to control the speed of the car is the air-fuel mixture being fed into the engine. A simple open-loop control system to implement for this system is to lock the position of the throttle the moment the driver engages cruise control. There is an add-on device available for motorcycles that uses a thumb switch to lock the twist-grip throttle in place. This is fine if the vehicle is driving on perfectly flat terrain. On hilly terrain, the vehicle will slow down when going uphill and accelerate when going downhill (environmental interference); something its driver may find undesirable (Bosch, 2003; Poulton, 1974).

In closed-loop control both the target and output signal (fed back) are available, giving the user the opportunity to compensate for error (Figure 3.2b). In a target acquisition task for example, the target signal is the desired position on the screen; the fed-back signal is the current position of the mouse cursor. In a feedback control implementation of the cruise control the speed is monitored and the amount of throttle is increased if the car is driving slower than the intended speed and decreased if the car is driving faster. This feedback makes the car less sensitive to disturbances to the system, such as changes in slope of the ground or wind speed (Bosch, 2003; Powers, 1989). One of the main advantages of this controller is guaranteed performance even with model uncertainties, even when the model structure does not match perfectly the real process and the model parameters are not exact (Ogata, 1990; Poulton, 1974). Feedback may be negative, which tends to minimise errors caused by disturbance (Figure 3.2b); or positive, which tends to amplify disturbance which can lead to instability (Figure 3.2b). While positive feedback may be useful in the design of experiments, the vast majority of manual control scenarios involve negative feedback systems (Jagacinski and Flach, 2003).

3.2.3 Compensatory and Pursuit Systems

In tracking tasks the user is asked to minimise the error between the control object (e.g. a cursor pointer) and the target (e.g. a simulated path). This simple

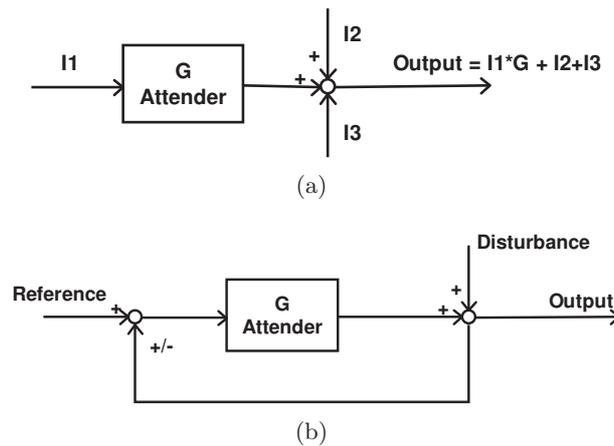


Figure 3.2: (a) A simple open-loop system, (b) A simple closed-loop system, negative/positive feedback.

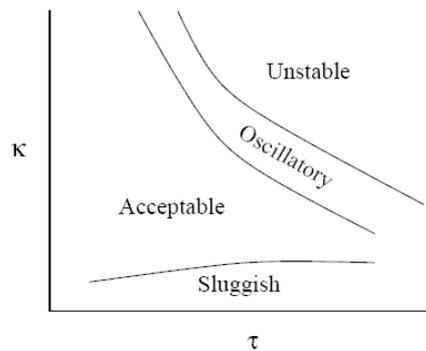


Figure 3.3: Effect of gain and time delay parameters on control. From Jagacinski and Flach (2003).

tracking task can be presented in a compensatory or pursuit display.

A system (or display) where only the error signal is available to the human operator is a compensatory system. A system (or display) where both the target and current output are available is called a pursuit system. Performance is generally better for pursuit tasks—it is sometimes possible to convert a compensatory system to a pursuit or preview system. Time is an important factor in the performance of pursuit systems. For tracking tasks, the initial phase where the input is brought into line with the target is called the acquisition phase (Doherty and Massink, 1999; Jagacinski and Flach, 2003).

3.2.4 Gain and Time-delay

A closed loop negative feedback system's (Figure 3.2b) behaviour is based on two parameters, firstly a delay or latency τ which is the time taken by the controlled element to react to its input, and secondly the gain K which determines the rapidity of adjustment. When K is low the system responds very sluggishly, moving only slowly towards the target signal, and when K is high the system oscillates. The delay τ can also affect the system behaviour – a high delay makes oscillatory behaviour much more likely. For example, in a concert where the music is output, τ must be low (of the order of 20ms) to produce a perceived immediate output. If τ is much higher, most musicians become unwilling to perform (Doherty and Massink, 1999; Jagacinski and Flach, 2003; Kelley, 1968).

3.2.5 Order of Control

Jagacinski and Flach (2003)(Chapter 9, pp. 87) describe order of control as a “*property of the controlled system (e.g., a computer input device).*” In this case, the order of control (or control order) refers to the “*dynamic relation between displacement of a control device*” (e.g. a mouse, tilt sensor, joystick) and the “*behaviour of the system being controlled.*” Usually the number of integrations between the input and output of the control system specifies the order of control. The term *order* refers to the order of the highest derivative in a differential equation or to the number of linked first-order differential equations used to model a system. “*In discrete positioning tasks such as those modeled by Fitts’ Law, the human operator produces a step-like output from the plant (e.g. mouse or other input devices), which is the task of moving the cursor pointer from one position to another in minimum time and with the accuracy specified by the target width.*”

Zero Order

A system with no integration between input and output is a zero-order system. Such a system (also called position control system) provides a proportional relationship between the displacement of the input and the output of the sys-

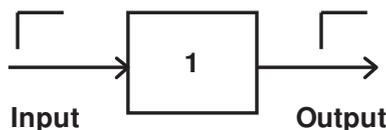


Figure 3.4: A zero-order system. The proportional relation between input and output is determined by the gain. Here the gain is equal to one. Adapted from Jagacinski and Flach (2003).

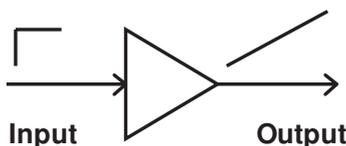


Figure 3.5: A first-order system. Adapted from Jagacinski and Flach (2003).

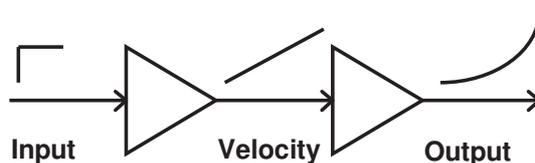


Figure 3.6: A second-order system; Adapted from Jagacinski and Flach (2003).

tem (Figure 3.4). For example, mouse controls typically employ a zero-order of control such as manipulation of the scroll-thumb. The mapping is from position to position and as the mouse position changes the scroll position changes proportionately (control-display gain determines the magnitude and acceleration of the mapping) (MacKenzie and Riddersma, 1994).

First Order

A system with one integration between control input and output is a velocity control system. Thus, there is a proportional relationship between the displacement of the input and the velocity of the output (Figure 3.5). Similar to position control, the gain of the velocity control system determines the proportionality between the position of input and the velocity of the output. When the input is stopped in any position (not null), the output continues in motion at a velocity proportional to the displacement from the null position.

Spring-centred joystick and in general input devices that have a well-defined null or zero position employ velocity control. The most important advantage of a velocity control is that it allows a limitless range of motion on the output

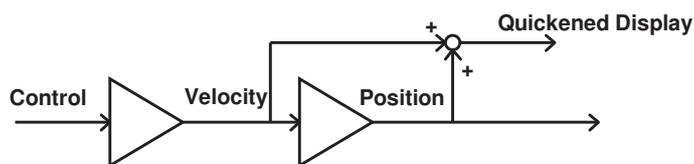


Figure 3.7: A block diagram for a second-order system with a quickened display. The output to the quickened display is the sum of position and velocity. Effectively, the quickened display projects the output into the future based on the current velocity. Adapted from Jagacinski and Flach (2003).

even when the range of the input motion is limited. But position control requires a limitless range of the input motion for a limitless range of the output motion (Jagacinski and Flach, 2003).

Second Order

A system with two integrations between control input and system output is called an acceleration control. A second order system provides a proportional relationship between the displacement of the input and the acceleration of the output (Figure 3.6). Second-order systems are more difficult to use than either zero- or first-order control systems; because the *“reversal of the input must be made in anticipation of the final stopping position.”* But practice makes most people to become skilled at using these system. This dynamic is typical of vehicular control, and video games which simulate vehicles (Jagacinski and Flach, 2003).

3.2.6 Quickening and Prediction

‘Quickening’ is a method for reducing the difficulty of controlling second-order or higher order systems, by changing the display to include predictions of future states (Birmingham and Taylor, 1954). *“A quickened display for an acceleration control system shows the operator a weighted combination of output position and velocity”* (Figure 3.7). This weighted summation foresees the future position of the system. Thus, when the operator responds to the position of the quickened element on the display, s/he reacts to the position and velocity of the vehicle or plant. This means having a quickened display reduces the control task order to zero order; although the dynamic response of the vehicle is not changed

“In general, quickening is a prediction of the future position of the vehicle based on the current position, velocity, acceleration, and so on.”

“A predictive display makes some guess about the future state of a system. This guess can be based on a direct or indirect measure of the system derivatives.”

Quickened and predictive displays are different in presenting information to the operator. A simple quickened display only displays position but a predictive display shows combination of predictions with other information (Jagacinski and Flach, 2003).

3.2.7 Control Order and Design Issues

“In a target acquisition task, the goal is to move a control system output into alignment with a fixed or moving target.” In this task, the final position of the system output (e.g. cursor) is more important than the method is used to reach the target. For example, moving a cursor to a menu option (menu selection) is an example of a target acquisition (Hancock and Booth, 2004).

In target acquisition tasks the target can be either stationary or non-stationary (moving target). For example, in acquiring a target with a fisheye lens (described in Chapter 6), moving and positioning the pointer relative to the underlying data can be difficult, since the data appears to move in the opposite direction of the moving focus point. This effect has been shown to cause significant problems in targeting tasks (Gutwin, 2002). Another example is expanding targets in MacOS dock (Apple, 2002) and Zhai et al. (2003) show that targeting is difficult due to relative motion of the targets. Moreover, the difficulty in learning and using a control system increases with increasing order of control. For most human-computer interfaces, a position or velocity control results in the best target acquisition performance.

In some interfaces the order of control is a design option and it depends on in which task the control input is going to be used. For example, position control (e.g. mouse) offers a precise placement but it requires space (like a mouse pad) to map the cursor movement on the screen to the movement of the actual input device. Velocity control offers a limitless range of motion on the

output even when the range of the control device is limited (Buxton et al., 2002), and when the relative range of movement is an issue velocity control should be considered (Jagacinski and Flach, 2003).

Scrollbars include both a position and a velocity control. Clicking on one of the up/down arrows in the scrollbar with the mouse cursor moves the text up or down at a constant rate, and thus is a velocity control system. However, the mouse cursor can be placed directly over the scroll handle, and drag it to the desired position in the document. When the position is acquired the handle is released and the text is then updated on the screen. This mode is a position control. However, in browsing long documents, this position control can become very sensitive because many pages map into a limited range of control movement. In this case, the handle position control is commonly used for approximate positioning, and the less sensitive velocity control arrows are used for fine positioning.

Additionally, moving target acquisition can work better with velocity control. For example, Jagacinski et al. (1980) found that velocity control had higher performance than position control in capturing small fast moving targets.

3.2.8 Control Devices

Another issue in designing systems is the type of input and control device that is used. The prominence of the null (zero) position is one important consideration for the input device, especially those who operate with velocity or higher order control systems; “*because the stick must be in this position for the output to stop on a target*”. Null position is not a problem in position control systems; because the output stops whenever the control input stops moving. So, a mouse is better suited for a position control system, but not a first order system. Spring-centred joysticks are generally better suited for velocity and higher order control systems.

“*One way to make the null position more distinct is to include a nonlinear dead-band or dead-zone in the zero region*” (Figure 3.8). Rockway (1957) reports that dead-space reduces the mean time on a target acquisition task using a spring-

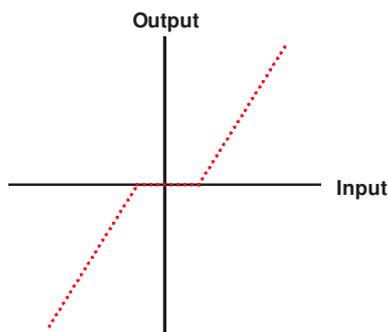


Figure 3.8: A dead-band (dead-zone) that can be used to insure that there is a well-defined null position for a control device. In the dead-zone, the output is zero for a range of input positions. Outside the zone, output is proportional to input.

centred joystick. A high gain reduces the range of movement required to keep the pointer on target. The effect of dead-space is particularly determined, when the gain of the control system is high. “*The dead-space is therefore a larger proportion of the range of movement*” (Kelley, 1968).

Another common nonlinear feature of a control device is *hysteresis*. When we push on something it yields and when we release it it does not spring back completely, then it is exhibiting hysteresis. A small amount of hysteresis is considered in the design of keys in a computer keyboard. Thus, the pressure required to activate the key is smaller than the pressure is required to deactivate it. So, the key remains in the active state, even if the pressure is partially released. The advantage of this nonlinear hysteresis is that it prevents accidentally double-clicking on the same key (Figure 3.9).

One important issue in evaluating and comparing particular control input devices is that these devices should be tested with the same dynamics; because dynamic aspects of the designed controller is sometimes independent from the task they are going to be used and tested. For example, comparing a mouse with a joystick in a target acquisition task may produce confusing results; because the dynamics are different (Jagacinski and Flach, 2003).

3.2.9 State-space Modeling

In control engineering a state space modeling is another way of presenting differential equations describing a dynamic system. It uses a set of first-order

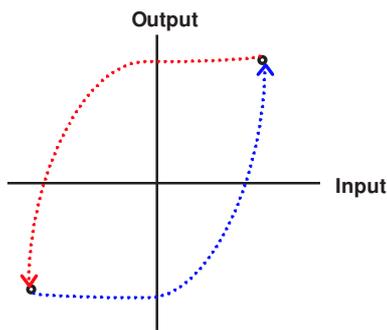


Figure 3.9: A typical hysteresis loop, increases only on the blue curve, decreases on the red curve.

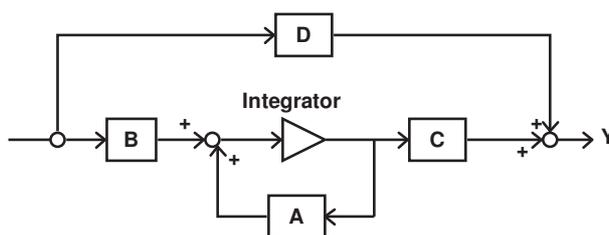


Figure 3.10: A typical state space model.

differential equations, i.e., input, output and state variables. The differential and algebraic equations are written in matrix format. State space modeling provides a convenient and compact way to model and analyse systems with multiple inputs and outputs (Ogata, 1990; Poulton, 1974). The general form of a state space model can be written as two functions:

$$\begin{aligned} \dot{x}(t) &= f(t, x(t), u(t)) \\ y(t) &= g(t, x(t), u(t)) \end{aligned} \tag{3.1}$$

The first is the state equation and the second is the output equation. The $u(t)$ is the input to the system, $x(t)$ is the state vector, t represents time and $f(\cdot)$ and $g(\cdot)$ state functions can be linear or nonlinear. Figure 3.10 illustrates a typical state space model.

State Variables

The internal state variables are the smallest possible subset of system variables that can represent the entire state of the system at any given time. State

variables must be linearly independent. The minimum number of state variables required to represent a given system, n , is usually equal to the order of the system's defining differential equation (Brogan, 1991; Ogata, 1990).

Linear Systems

The most general state space representation of a system with p inputs, q outputs and n state variables is written in the following form as shown in Figure 3.10 (Brogan, 1991; Ogata, 1990):

$$\begin{aligned} \dot{x}(t) &= A(t)x(t) + B(t)u(t) \\ y(t) &= C(t)x(t) + D(t)u(t) \end{aligned} \tag{3.2}$$

$x(t)$ is called the *state vector*, $y(t)$ the *output vector*, $u(t)$ the *input (or control) vector*, $A(t)$ the *state matrix*, $B(t)$ the *input matrix*, $C(t)$ the *output matrix*, and $D(t)$ the *feedthrough (or feedforward) matrix*. Note that in this general formulation all matrices are time-variant. The time variable t can be a *continuous* (i.e., $t \in R$) or *discrete* (i.e., $t \in Z$): in the latter case the time variable is usually indicated as k which involves the evaluation of a matrix exponential $\Phi = e^{Ak}$ and $\Gamma = \int_0^k e^{As} ds B$.

$$\begin{aligned} x(k+1) &= \Phi x(k) + \Gamma u(k) \\ y(k) &= Cx(k) + Du(k) \end{aligned} \tag{3.3}$$

For nonlinear state functions (3.1) we can locally linearise them around any given state leading to time-varying matrices $A(t)$, $B(t)$. One common technique in solving first-order linear differential equations is Euler's formula (Polyanin and Zaitsev, 2003). We can analytically investigate the local dynamics for different operating points by, for example, looking at the eigenvalues of the A and B matrices to check for oscillatory (eigenvalues are complex conjugate pairs) or unstable behaviour (the real part of the eigenvalues are in the right half plane - i.e., eigenvalues are positive) (Åström and Wittenmark, 1997; Brogan, 1991).

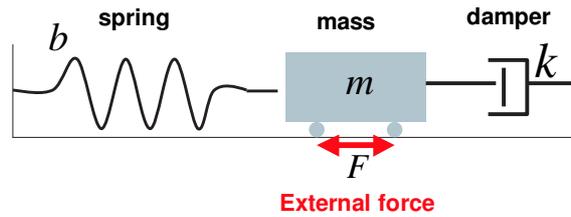


Figure 3.11: A Spring-Mass-Damper system.

Controllability

A continuous time-invariant state-space model is controllable if and only if

$$\text{rank}[B|AB|\cdots|A^{n-1}B] = n \quad (3.4)$$

Rank is the number of linearly independent rows in a matrix (Brogan, 1991; Ogata, 1990).

Control Mode

We can introduce transitions among control modes which alter the dynamics and the way user inputs are interpreted. A simple example of this approach uses state feedback to augment control behaviour: by making the state variable move towards some reference value r , we can create a control law such that the new state equations are (Ogata, 1990):

$$\begin{aligned} \dot{x} &= Ax + Bu = Ax + BL(r - x) = Ax - BLx + BLr \\ &= (A - BL)x + BLr \end{aligned} \quad (3.5)$$

such that the system dynamics have changed from A to $(A - BL)$. In classic control this method is called “*Proportional Control*.” In the next few chapters it will be shown how this control mode can be applied in designing interaction.

In the next section a state-space model for a simple moving object is provided to clarify the idea about state variables and controllability. We illustrate the system behaviour when the coefficient settings are changed in the model.

Moving Object Example

A classical linear example is a one-dimensional mass moving horizontally on a plane and attached to a wall with a spring and a damper (Figure 3.11). Newton's laws of motion, *Cause of change = Resistance to change × Rate of change* or *Force = Mass × Acceleration*, for this object:

$$m\ddot{y}(t) = u(t) - k\dot{y}(t) - by(t) \quad (3.6)$$

where

- y_0 is initial position; $y(t)$ is position; $\dot{y}(t)$ is velocity; $\ddot{y}(t)$ is acceleration,
- $u(t)$ is an applied force, F ,
- k is the damping coefficient,
- b is the spring constant,
- m is the mass of the object.

The state equation would then become

$$\begin{aligned} \begin{pmatrix} \dot{x}_1 \\ \dot{x}_2 \end{pmatrix} &= \begin{pmatrix} 0 & 1 \\ \frac{-b}{m} & \frac{-k}{m} \end{pmatrix} \begin{pmatrix} x_1 \\ x_2 \end{pmatrix} + \begin{pmatrix} 0 \\ \frac{1}{m} \end{pmatrix} u \\ y(t) &= \begin{pmatrix} 1 & 0 \end{pmatrix} \begin{pmatrix} x_1 \\ x_2 \end{pmatrix} \end{aligned} \quad (3.7)$$

Where

- $x_1(t)$ represents the position of the object
- $x_2(t) = \dot{x}_1(t)$ is the velocity of the object,
- $\dot{x}_2(t) = \ddot{x}_1(t)$ is the acceleration of the objection,
- the output $y(t)$ is the position of the object

Figure 3.12 presents this system's behaviour to different damping coefficient settings. In MATLAB ([MathWorks, 2005](#)) we can solve these first-order differential

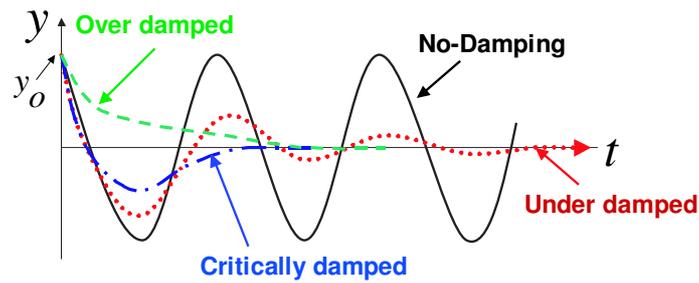


Figure 3.12: The Spring-Mass-Damper system behaviour (only position, y , is shown) for different damping coefficient. In this system $m = 10$, $b = 3$, initial position is 0.5 and there is no initial velocity. The oscillatory behaviour is generated when k is zero. When k is set to 4 the system behaviour is under-damped and changing k to 8 has generated critically damped behaviour. For very large damping coefficient, for example 20 here, over-damped behaviour is observed.

equations using three different solution schemes (Polyanin and Zaitsev, 2003): (1) “continuous analytical solution,” which constructs the continuous matrix exponential form of the solution from the state-space model, (2) “discretisation of the system” using matrix exponential with sampling time T (uses “ss” and “lsim” commands), and (3) “numerical integration of the state equations using ode45”, which employs Runge-Kutta-Fehlberg method. Matlab code of the moving object simulation is available in Appendix A. This simulation employs “lsim” command in MATLAB with sampling time 0.1 se to solve the linear system.

The controllability test is

$$\begin{aligned} \text{rank}(B|AB) &= \text{rank} \left(\begin{array}{c|c} 0 & \begin{pmatrix} 0 & 1 \\ -b & k \end{pmatrix} \\ \frac{1}{m} & \begin{pmatrix} 0 \\ \frac{1}{m} \end{pmatrix} \end{array} \right) \\ &= \text{rank} \begin{pmatrix} 0 & \frac{1}{m} \\ \frac{1}{m} & \frac{k}{m^2} \end{pmatrix} = 2 \end{aligned} \quad (3.8)$$

which has full rank for all k and $m \neq 0$. Thus, a wide range of values for both k and m exists to make system controllable and stable.¹ In the next section we answer the question “how can we define state-space coefficient settings to achieve the best performance measure?”

¹A system is stable where the state matrix A is full rank.

3.2.10 Performance Measures

The “*performance criteria*” provide a value system for identifying an optimal path. “*The performance criteria are typically expressed as a function to be minimised.*” The differential and algebraic equations in the state-space mode can be used to determine the path through state space (or the control law) that minimises (or maximises) the performance criterion. Typical criteria include time, distance, or resource consumption.

In Fitts’ law experiments, the goal is to capture the target in minimum time (refer to Section 2.5.2 on page 26). Thus, the performance in this discrete positioning can be described as minimising the function:

$$J = \|t_f - t_0\| \quad (3.9)$$

t_0 and t_f are initial and final time in Fitts’ Law task respectively.

In continuous tracking tasks, “*performance is typically scored in terms of an integrated or average mean squared error*”. Thus, the performance can be described as minimising the tracking error $e_1(t)$ as below:

$$J = \frac{1}{t_f - t_0} \int_{t_0}^{t_f} e_1^2(t) dt \quad (3.10)$$

A general form for the performance measure is:

$$J = h(\bar{x}(t_f), t_f) + \int_{t_0}^{t_f} g(\bar{x}(t), \bar{u}(t), t) dt \quad (3.11)$$

The first term in this function reflects the value (or cost) of the final state and final time. The second integral term represents a cumulative function of the states, the control actions, and time (Brogan, 1991; Jagacinski and Flach, 2003; Kirk, 1970; Ogata, 1990).

3.2.11 Conceptual Models and State-Space Modeling

In this section we showed that the laws of physics (e.g., Newton’s law of motion) can be incorporated in building dynamical systems using state-space re-

presentation. The laws of physics are invariant when translated from one place to another, i.e., Newton’s laws of motion remain a good approximation at least on the Earth. That is they have translation symmetry (Thimbleby, 2001). Furthermore we perceive the laws of physics in the same way at different times. Translation in time and translation in space together capture the notion of consistency and if a system is perceived in the same way at different times and different places, then the “symmetry-affordances” suggest the same set of actions on the system are available (Thimbleby, 2001).

In Chapters 5 and 6 we show that the laws of physics and real-world effects such as haptic feedback of springs, viscous effects linked to motion in the liquid, or friction linked to speed of motion, which are easy to reproduce in a dynamic system using state-space representation encourage the interaction to fall into a comfortable, natural rhythm.

The next section explores how the key definitions we provided throughout Section “manual control” can be used to build quantitative models for human operators.

3.3 Human Operator Modeling

Manual control is the study of humans as operators of dynamic systems. Early research focused on the human element in vehicular control (Kiencke and Nielsen, 2000). Designers of these systems realised that the human was an important element in the system control loop. In order to predict the stability of the full system, they had to include mathematical descriptions of the human operators along with the descriptions of the vehicle dynamics. However, the applications of manual control theory has been modified and extended to applications in HCI. Humans are regularly asked to position the cursor on a menu, drag the scrollbar and other tracking and positioning tasks. Thus, the human operator can be modeled using the tools of manual control theory. It has further benefits: “*First, quantitative models of the human operator may provide insights into basic properties of human performance*”. “*Second, the ability to derive transfer function*

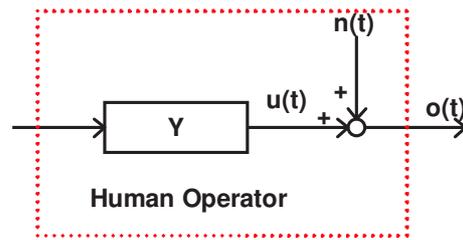


Figure 3.13: A quasi-linear model of the human operator. Y_h is the linear transfer function; $u(t)$ is the linear response; $n(t)$ is internal noise (reflected noise in the perceptual and motor systems of the operator); and $o(t)$ is the quasi-linear response. The noise is generally presumed to be uncorrelated with any input signal. Adapted from Jagacinski and Flach (2003).

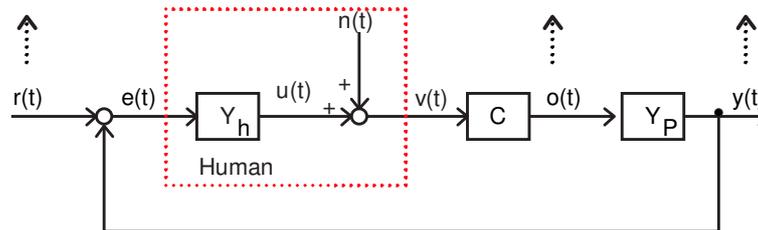


Figure 3.14: A typical 1D compensatory tracking task. Adapted from Jagacinski and Flach (2003).

for human operators would greatly facilitate the ability to predict the performance of human-machine systems”.

Human behaviour is nonlinear but linear analysis still provides important insights into human performance and linear models may be able to give reasonable predictions for some situations. Many researches have been done to develop a quasi-linear model of the human operator (Figure 3.13). “The quasi-linear model is an attempt to represent the human operator as a constant coefficient linear differential equation [...] plus internal noise which is assumed to arise from perceptual or motor processes internal to the human operator” (Jagacinski and Flach, 2003).

Figure 3.14 illustrates a typical 1D tracking experiment. The human operator, represented as Y_h and $n(t)$, is instructed to follow a quasi-random input signal, $r(t)$. The error, $e(t)$, is displayed in a compensatory tracking task. Control responses, $o(t)$, are typically made with a joystick or in general a controller, $C(t)$, and these control responses are input to a plant (e.g., computer) Y_p . The output of the system, $y(t)$, is the response of the computer.

To build a describing function for the human operator “Bode analysis” is

a strong candidate because it is possible to create the human transfer function, Y_h , from the patterns in the Bode space.

3.3.1 Describing Functions in Bode Diagram

The Bode diagram can provide useful information about both: how a given process will behave when a controller is provided, how a particular human + controller + plant combination will behave (Ogata, 1990). This plot is a useful method for presenting the change in amplitude (output amplitude/input amplitude) and the phase shift (output phase-input phase) that is produced by a particular linear system. The power of the amplitude ratio (i.e., magnitude squared) is plotted in decibels ($10\log_{10}$). This is plotted against log frequency (in radians/s). The phase shift is plotted in degrees against log frequency (radian/s) (MathWorks, 2005).

Figure 3.15 presents a Bode diagram example that illustrates typical results of a one-dimensional compensatory tracking study. In this study the plant was a simple gain ($Y_p = 4$). That is, the response of the simulated vehicle was proportional to the control input-it was a zero-order control system. First, note the amplitude ratio presents a 10 dB/decade slope (10 dB/ \log_{10} Hz) at high frequencies; this is a characteristic of integration. The phase response goes down continuously with increased frequency suggesting a time delay. Thus, the human transfer function can be a gain, a lag, or an integrator at higher frequencies, and a time delay (Jagacinski and Flach, 2003; Poulton, 1974).

$$Y_h(j\omega) = \frac{K e^{-j\omega\tau}}{j\omega} \quad (3.12)$$

The gain K is a scaling factor that influences the bandwidth of the control system. The time delay τ reflects human reaction time. In simple tracking tasks the range of the time delay is between 20 ms to 150 ms, which overlaps with measures of reaction time in response to continuous stimuli (refer to Section 3.2.4 on page 37). The lag $\frac{1}{j\omega}$ suggests that the human tracker has a low pass characteristic – that is, the human responds to low frequency components of errors and

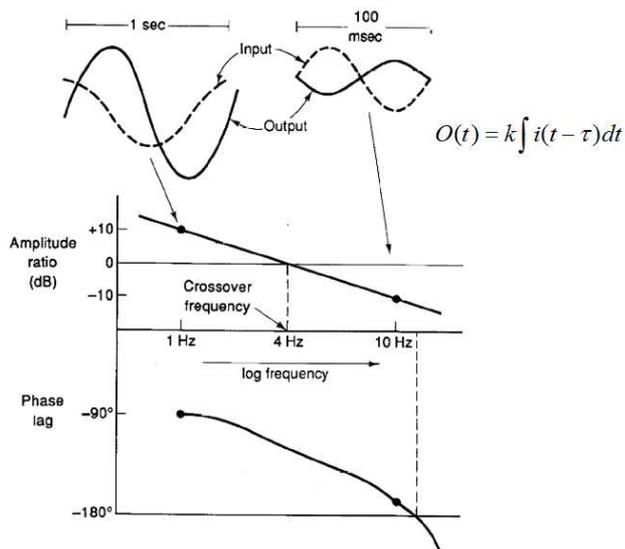


Figure 3.15: Top—A Bode plot representation of a first-order lag with gain k and time delay τ . Bottom—The frequency response for a human operator controlling a zero-order system ($Y_p = 4$)

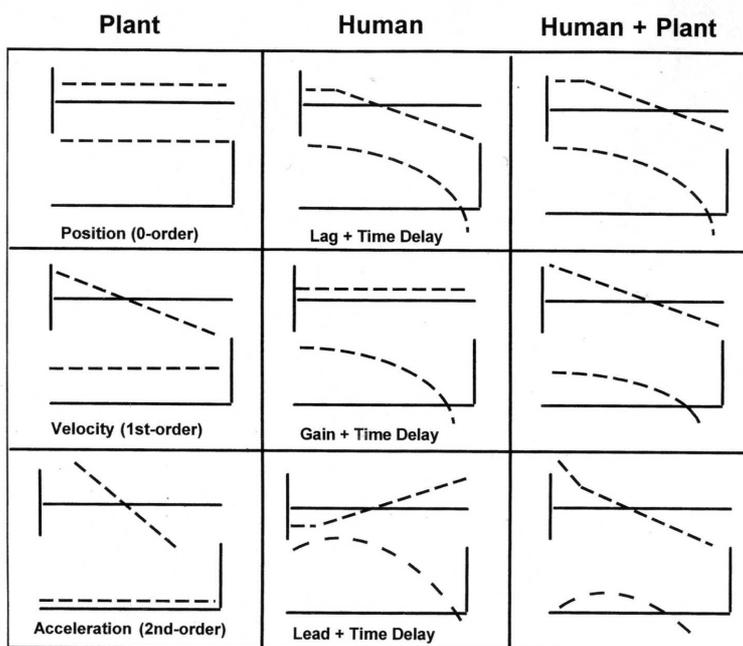


Figure 3.16: The schematic illustrations shows the adaptive nature of the human controller. The human transfer function (amplitude ratio and phase shift) changes depending on the system being controlled. From Jagacinski and Flach (2003).

ignores (or filters out) the high frequency components of error (MacKenzie and Ware, 1993).

Figure 3.16 illustrates Bode plots of the human controller adapting to the plant dynamics (Sheridan and Ferrell, 1974). For example, humans adjust their

gain to compensate increases or decreases in plant gain (e.g. pilots change their gain behaviour when they switch from Boeing 747, which is heavy to an aerobatic airplane), so the total open-loop gain in Figure 3.14 remains constant in a way that reflects the constraints on stable control (Jagacinski and Flach, 2003; Sheridan and Ferrell, 1974):

$$Y_h(j\omega)C(j\omega)Y_p(j\omega) = \text{constant} \quad (3.13)$$

However, the human operator model is different for each different plant. In Figure 3.16 in one case, the human looks like an approximate integrator or lag, in another the human looks more like a gain, and in another the human looks more like an approximate differentiator or lead. In all cases, a time delay is evident. In all three cases, the transfer function for the forward loop Y_hCY_p (see Figure 3.14) looks similar, i.e., approximately like a gain, a time delay, and an integrator in the region of the crossover² (Jagacinski and Flach, 2003):

$$Y_h(j\omega)C(j\omega)Y_p(j\omega) = \frac{\omega_c e^{-j\omega\tau}}{j\omega} \quad (3.14)$$

Note that at the crossover frequency, $\omega = \omega_c$, the net gain of human + controller + plant is 1.0, so the open-loop gain parameter in the numerator is equal to ω_c . Furthermore, in designing the controller, $C(j\omega)$ should be chosen such that the

- The closed-loop system should remain stable;
- The phase margin and amplitude ratio should be maximised;
- The cost function, J , should be minimised Jagacinski and Flach (2003); Ogata (1990); Sheridan and Ferrell (1974).

The control loop between perception and action is almost always closed through an environment (see Chapter 2). So, constraints such as stability reflect global properties of this control loop. “*Models of behaviour are likely to include terms*

²The point where the open-loop response goes through the zero db is referred as crossover frequency. The crossover frequency ω_c is a measure of the dynamical quality of the control loop. The higher ω_c the higher the bandwidth of the closed loop, and the faster the reaction on command inputs or disturbances (Ogata, 1990).

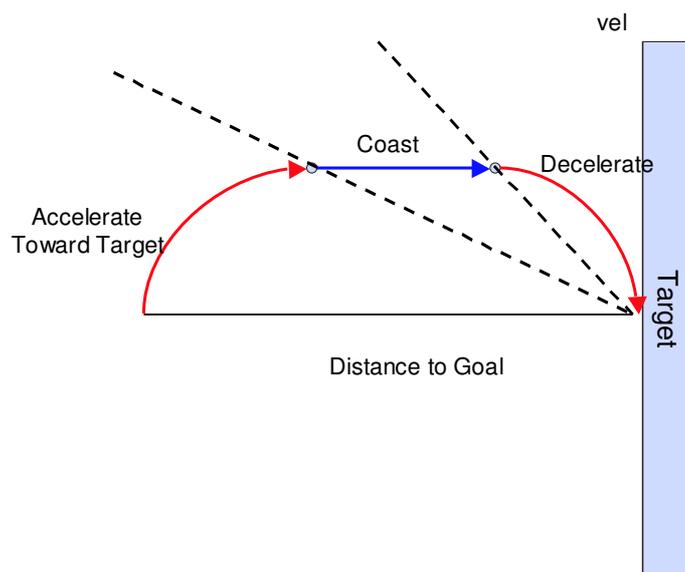


Figure 3.17: A finite state controller. The switching criteria are diagonal lines (constant time-to-contact). Three controllers are an acceleration toward the goal (bang), a coast (zero control input) resulting in a constant velocity, and a deceleration (bang) into the target. Adapted from Jagacinski and Flach (2003).

like the control strategy in the crossover model, whose parameters depend on the task context. It suggests that behaviour is “situated”. Behaviour is just an adaptive response to situation constraints” (Jagacinski and Flach, 2003).

3.3.2 “Bang Bang” Models of Human Controller for High-Order Systems

In Fitts’ law tasks, where the user is asked to move the cursor from a starting position to a target area, the hand is also moving from one position to another, or in rotating the eye from one fixation to another, the human operator has to vary the location of a mass using the force exerted by his muscles which is limited in its maximum value. Dynamically, the hand or eye is virtually a pure mass, with low dissipation of energy through friction, and low storage of potential energy through spring-like behaviour. A simple servomechanism, in controlling the location of an object, applies a force to it proportional to the deviation of the location from the desired one, in such a direction as to reduce the deviation (Gaines, 1967b,a). Bushaw (1953) showed that the control policy of the linear servomechanism was not time-optimal, in that it did not reduce the error in location to zero

as rapidly as possible, and he showed that a “bang bang” controller, applying maximum available force in one direction for half the time and then applying it in the other, gave improved performance. Figure 3.17 illustrates an example of a discrete style of control that might be used to point a target (Jagacinski and Flach, 2003). The switching boundaries are set at constant ratios of position and velocity. From an initial position a thrust command (i.e., thrust generated by mouse movement) causes the pointer to accelerate toward the target. The first diagonal boundary occurs, where the thrust command is terminated and allows the pointer to coast toward the target at a constant velocity. For many control situations (e.g., stopping at a target on the screen) the coast region may show some deceleration due to friction drag. The second diagonal boundary happens, where a reverse thrust is initiated causing the craft to decelerate as it approaches contact with the target (Fuller, 1960a,b; Jagacinski and Flach, 2003).

Li et al. (1965), reviewed in (Gaines, 1967a), described qualitatively the variation of the human operator’s switching boundary in learning to control an unstable second-order system (see Chapter 5). Weir and Phatak (1967) measured the time-variation of the switching boundary in response to step changes in the controlled element dynamics. However, as yet, there does not appear to have been any detailed study published of the learning of a high-order control skill, where a “bang bang” control policy is either forced by the nature of the controls, or expected to appear (Gaines, 1967b).

In this section we explored quantitative models for a human operator interacting with a control system. This interaction requires a control device. An important contribution of this thesis is to designing interaction on small screen devices, which require novel sensors and control devices.

3.4 Control Devices for Small Screen Devices

In this section we introduce new styles of interaction with mobile computers most prominently tilt-based input method. Two-handed input, which is the most common form of interaction with “*Palmtop*” computers, is not suitable in

the context of mobile applications (Dong et al., 2005; Fallman, 2002a,b; Harrison and Fishkin, 1998; Oakley et al., 2004; Partridge et al., 2002; Rekimoto, 1996; Sazawal et al., 2002; Wigdor and Balakrishnan, 2003). Two-handed input requires the user's complete attention, both in terms of physical attention (where both hands are confined), as well as cognitive attention (reading the screen, pointing and clicking on interface widgets, etc.). Hence, we want to explore if there are other means of interaction that would free up at least one hand as much as possible, making mobile users able to use their hands for doing other tasks and the notion of embodiment is implicitly considered in our design through interaction by pointing, scrolling and zooming. Instead of touching the screen and selecting targets and using both hands we can connect these through the notion of tilt and audio feedback. These ideas will be discussed in more details in Chapters 4 to 6.

Within such work, tilt has been suggested as an input method to ease interaction with Palmtops, where the devices are understood as embodying their interfaces (Fishkin et al., 2000; Harrison and Fishkin, 1998). Tilting the device itself is here the means of interaction, which has largely been concerned in scrolling and pointing on a graphical user interface or for menu selection (Fishkin et al., 2000; Harrison and Fishkin, 1998; Norman, 1998). In this thesis, we explore the use of tilt as an input method to allow both one handed input to the system, as well as contributing to the design vision of embodiment. Our contribution in this area is to find embodiment not only in terms of the specific input method of tilting, but also in terms of the feedback given to the user through the screen output.

3.4.1 Tilt Sensor: Accelerometer

The construction of devices which are used to sense acceleration may be classified as either mechanical or solid-state. Mechanical sensors are well established and can provide highly accurate measurements of acceleration even down to a few micro-g in some cases (Luinge, 2002). These sensors though are generally fairly large, larger than an average mobile device, we must find a suitable alternative. New applications that have demanded low-cost sensors for providing

measurements of acceleration have provided a major incentive for the development of micro-machined electromechanical system (MEMS) sensors. In the last 25 years these devices have overcome many of the features that have impeded the adoption of inertial systems by many potential applications, especially where cost, size and power consumption have been governing parameters ([Titterton and Weston, 2004](#)). For this reason we focus on solid-state (MEMS) sensors here.

At a low level, accelerometers are essentially mimicking the human vestibular system. This system is essential for stable posture control and enables humans to move freely since it is not earthbound. This is also the system utilised by our brain to measure head movements without a frame of reference. MEMS sensors can be worn on the body and, like the vestibular system, the working principle of these sensors is based on inertia, enabling measurement anywhere without the need for a frame of reference ([Rekimoto, 1996](#)). These advantages have a trade-off though, in that they are less precise than the traditional mechanical sensors ([Analog Devices, 2000](#); [Horton and Kitchin, 1996](#); [Zhao, 1997](#)).

MEMS devices may be divided into two distinct classes, reflecting the manner in which acceleration applied to the case of the device is sensed ([Titterton and Weston, 2004](#)):

- The displacement of a proof mass supported by a hinge or flexure in the presence of an applied acceleration, that is, a mechanical sensor using silicon components (Figure 3.18);
- The change in frequency of a vibrating element caused by the change in tension in the element as a result of the mechanical loading that occurs when the element is subjected to acceleration.

These MEMS devices are analogous to the force feedback accelerometers and the vibrating-beam sensors (For more details refer to [Titterton and Weston \(2004\)](#)).

Our applications used two different tilt sensors XSENS and MESH. Figure 3.19 presents the XSENS P3C 3 degree of freedom linear acceleration sensor attached to the serial port. Its effect on the balance of the device is negligible (its weight is 10.35 g). The accelerometer is used to detect tilt magnitude around

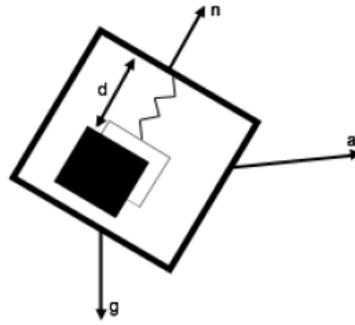


Figure 3.18: This figure conveys the ‘mass in a box’ representation of an accelerometer whereby a mass is suspended by a spring. This mass is allowed to move in one direction which is the sensitive direction of the accelerometer. The displacement of the mass with respect to the casing is proportional to the difference between acceleration and gravity in the sensitive direction.



Figure 3.19: Left: XSENS device alone, Right: The XSENS attached to an HP5500 Pocket PC.



Figure 3.20: Left: Mesh device alone and attached to an HP5500 Pocket PC. Right: The MESH circuit board showing the main components related to the navigation task.

the x , y and z axis of the mobile device, sampling at a rate of 35 samples per second.

Figure 3.20 presents the MESH (Oakley et al., 2004) inertial navigation system (INS) backpack consisting of 3 Analog Devices ± 2 g dual-axis ADXL202JE accelerometers, 3 Analog Devices ± 300 deg/s Single chip gyroscopes, 3 Honeywell devices HMC1053 magnetometers and a vibrotactile device used for feedback

purposes. A standard orthogonal inertial sensor arrangement is used with the sensitive axis of the respective inertial sensors mounted coincident with the principle device axes providing us with direct measures of lateral accelerations, turn rates and magnetic field strength as well as the current Global Positioning System (GPS) latitude and longitude.

The accelerometers in this system have a 10-bit accuracy with a bandwidth of 30 Hz over a 5 g range (an accuracy of approximately 0.005 g). For use in these studies, this is filtered in software to 12-bit accuracy at 8 Hz (approximately 0.00125 g). This in turn can accurately measure the orientation of gravity (and therefore of the device) at the level of a ninth of a degree. This sensor system is capable of detecting orientations considerably more accurate than the human body is capable of reliably producing (Oakley and O'Modhrain, 2005). The sampling frequency plays an important role in the performance of the user. For example, in the accelerometer in this system, sampling frequency below 70 Hz is not comfortable and the user receives slow responses from the input device. So in all our applications presented in this thesis we have used sampling frequency 100 Hz.

The vibrotactile display within MESH consists of two main elements: a vibrotactile transducer, and a sample playback circuit. The transducer is a VBW32 (Oakley et al., 2004), sold as an aid for hearing impaired people. It is modified (by rewinding the solenoid with a larger gauge wire) to operate at a lower voltage, which enables it to be powered by the IPAQ's battery. This display can produce vibrotactile samples with different sampling frequencies and intensities.

3.4.2 Calibration

Before it is possible to work with any sensor data it is necessary to perform some simple calibrations. Calibration of the accelerometers is not necessary in all situations. For a gesture recognition application it may actually be better to work with raw accelerometer data whereas for a tilt application, if we are not

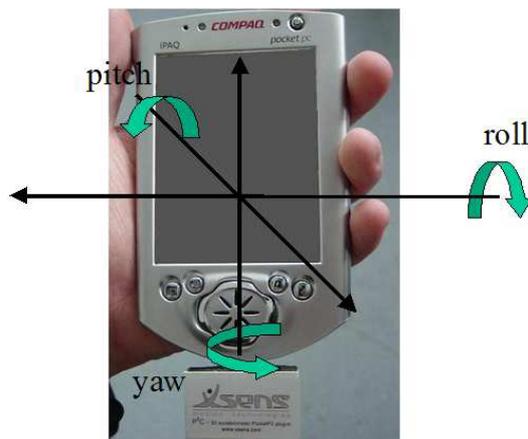


Figure 3.21: Rotational motion of a PDA and roll, pitch and yaw tilt angles measured by accelerometer.

working with the fully derived “*strapdown*” equations³ (Roth, 1999; Titterton and Weston, 2004), the data needs to be quickly calibrated or *zero’d* at the beginning of each use. Zeroing the data essentially just involves defining the rest point of the device, i.e., the values from the accelerometer where the device is flat in the users hand. Any tilting of the device will then give a deviation from these ‘zero’ values which are then used as indicators that the device is being tilted (Roth, 1999; Strachan, 2007; Walchko, 2002).

3.4.3 Continuous Interaction via Tilt Sensor

In a tilt controlled interaction, the tilt sensor provides a continuous interactivity between the user and the device. Tasks such scrolling and browsing in mobile devices as being that it should provide appropriate feedback to allow the user to control their position and velocity compared to their goals. In the case of tilt-based scrolling, this will typically be roll and pitch tilt angles (Figure 3.21). On a mobile device, the user perceives the feedback via audio, vibrotactile and visual displays.

We also need to give the user some predictive ability to know, if they keep

³A strapdown INS is an inertial navigation system where the sensors are attached to or ‘strapped down’ without any mechanical complexity. Modern systems have removed most of the mechanical complexity of old systems and the sensors are smaller, lower cost and more reliable and are physically strapped to the host vehicle, such as a missile or plane, but we are penalised in that strapdown systems are generally less accurate than the older mechanical systems. The strapdown equations are basically the navigation equations developed for this type of system (Titterton and Weston, 2004).

scrolling or browsing in a certain direction, they will get to the goal. ‘Quickening’ (or ‘predictive’) display (see Section 3.2.6 on page 39) is one method for reducing the difficulty of controlling second-order tilt-controlled system.

3.5 Conclusions and Summary

The advent of a number of modern interaction technologies means that techniques must be developed to allow designers to consider issues raised by continuous interaction between users and computer systems. In this chapter, we reviewed the main concepts of manual control theory. This approach requires that special consideration is given to control and feedback signals, and transformations of these signals. This approach to modeling can cope with the diverse challenges of traditional interaction design which allows us to view the operation of the system at many different levels, from low level device control to high level human operator modeling and task analysis (Jagacinski and Flach, 2003). By building on work from control theory, human behaviour modeling and interactive systems, and developing a framework for relating analysis at different levels, we hope to provide the designer with a richer modeling capability for continuous interaction.

In the next chapters we will investigate the applications of this view to interactive system design by considering systems for mobile situations. In this context, we will look at characterisation of control the aspects of user, device and controlled process, some of the tradeoffs involved in designing a control system, and simple graphical representations of control system configurations.

Chapter 4

Model-based Target Sonification in Small Screen Devices: Perception and Action

This chapter investigates the use of audio and haptic feedback to augment the display of a mobile device controlled by tilt input. The questions we answer in this chapter are: how do people begin searching in unfamiliar spaces? What patterns are visible or techniques are employed to accomplish the experimental task? What effect(s) do a prediction of the future state in the audio space and modeling human operator have on subjects' behaviour? In the pilot study we study subjects' navigation in a state-space with seven randomly placed audio sources, displayed via audio and vibrotactile modalities. In the main study we compare only the efficiency of different forms of audio feedback. We run these experiments on a Pocket PC instrumented with an accelerometer and a headset. The accuracy of selecting, exploration density and orientation of each target are measured. The results quantify the changes brought by predictive or 'quickened' sonified displays in mobile, gestural interaction. Additionally they highlight subjects' search pattern and the effect of a combination of independent variables and each individual variable in the navigation patterns.

4.1 Introduction

One of the main goals of interaction design is to render the interfaces as intuitive as possible. In our everyday environments humans receive a variety of stimuli playing upon all senses, including aural, tactile and visual, and we respond to these stimuli. Even though hearing and vision are our two primary senses, most interfaces are today mainly visual.

As stated in the introduction chapter, visual interfaces have crucial limitations in small screen devices. These devices have a limited amount of screen space on which to display information. Designing interfaces for mobile computers is problematic as there is a very limited amount of screen resource on which to display information and users' eyes are often needed on the environment rather than the interface (i.e. that they can look where they are going), therefore, output is limited (Blattner et al., 1992; Brewster and Murray, 2000; Brewster, 1997; Johnson et al., 1998; Kramer et al., 1999; Rinott, 2004; Smith and Walker, 2005; Walker and Lindsay, 2006). Also, low graphics resolution and few colours in these devices do not help designers to design complicated interfaces.

One way around these problems would be sonically enhanced interfaces that require less or no visual attention, therefore the size of visual display and portable device can be decreased. Moreover auditory interfaces potentially interfere less in the main activity in which the user is engaged. Consequently, the user may be able to perform more than one task at a time, such as driving a car while using a telephone or grabbing a cup of coffee while waiting for a mobile phone to finish downloading an image. Auditory feedback can often be a necessary complement, but also a useful alternative to visual feedback. When designing a mobile electronic device, it is difficult to predict all possible scenarios when it might be used. Obviously, visual feedback is preferred in many situations such as in noisy environments or when the user has to concentrate on a listening task. However, as there might be numerous occasions when a user cannot look at a display, versatile devices such as mobile phones or handheld computers benefit from having flexible interfaces.

Chapter 4 outlines model-based sonification and human perception and action when s/he is interacting with auditory interfaces on small screen devices. In Chapter 4 we investigate the usability of non-speech sounds and haptic feedback to augment the display of a mobile device controlled by a gesture input. Non-speech sound has advantages over speech in that it is faster and language independent. We use control strategies of users in browsing the audio/haptic state space. Lastly, we explore one possible way of improving performance based on models of human control behaviour in two example applications.

4.2 Background

4.2.1 Hearing and Vision

Vision and hearing are our two primary senses for obtaining information about the outside world. Hearing has often been considered secondary to vision, as it seems that in many situations we use our ears merely to tell us where to turn our eyes (Gaver, 1997). However, it is important to emphasise that sound is a unique medium that can provide information which vision cannot. Our eyes perceive light, which is reflected from objects around us. Vision hence tells us about the surface, size and shape of objects. Our ears, on the other hand, perceive patterns of moving air that vibrating objects generate. Sound can carry information about the consistency and hollowness of objects. Hearing can therefore provide understanding about the interior of objects, which is a domain where vision is limited. Another feature of sound is that it can communicate information quickly (Brewster, 1997). Sound is of a fundamentally different temporal nature to that of visual objects; what we hear become more transitory than what we see. In the words of Gaver (1989), “*sound exists in time and over space, vision exists in space and over time.*” Spatially, sound has the advantage of not being bound to a certain location. To see something, say a screen, we need to face it. However, the sound from a speaker can be heard in darkness, from far away and facing any direction. A drawback of this is that one cannot turn away from sounds. Neither can one close one’s ears from an unpleasant sound. In our everyday lives, sound

and vision interact smoothly. Hearing and vision complement one another in the natural world around us and could also do so in films, multimedia and other environments created by human beings. People prefer to communicate face to face, being able emphasise words with facial expressions and body language. Naturally, almost every form of communication – e-mail, letters or even talking on the phone – has characteristic limitations. For example, written words cannot convey intonation as well as a spoken voice. Human-machine interaction ought to benefit from using sound because it is central to human communication. If the possibility of conveying information sonically were used to its full potential, it would be a powerful complement to visual interfaces (Brewster and Murray, 2000). A strong argument against the use of sound in interfaces is that it easily can become annoying both for the user and other people around them, since it is more intrusive than visual impressions. It is not useful in noisy environments, for instance, train stations, underground, so forth. However, by skilfully designing auditory interfaces or using haptic feedback, this can be avoided.

4.2.2 The Potential of Auditory/Tactile Interfaces

The single audio output channel has been little used to improve interaction in mobile devices. Speech sounds are, of course, used in mobile phones when calls are being made but are not used by the telephone to aid the interaction with the device (Blattner et al., 1992; Brewster, 2002; Gaver et al., 1991). Non-speech sounds and vibrotactile devices are used for ringing tones or alarms but again do not help the user interact with the system beyond this. Some signals provide feedback that some event has been successful, such as when buttons are pressed or devices are switched on. Selecting items with a stylus in PDAs is often confusing for the users without tactile feedback because it is hard to know they have hit the target or not, especially if used in a mobile setting (Brewster, 2002). In this case vibrators in mobile phones could be a good haptic feedback. This feedback assures the user that s/he is in the target, and if the user wants to select a target s/he can then press a key in the vibration area to select it.

If using continuous sounds as opposed to the more common brief signals,

auditory interfaces do not need to be more transitory than visual interfaces. However, such sounds probably benefit from being quite discreet. While, most existing sound feedback today occurs in the foreground of the interface, subtle background sounds can be a useful complement in advanced auditory interfaces. Films and computer games generally make use of music and sound effects. Film sound theorist [Chion \(1994\)](#) has made the following statement concerning sound in film: *there is no soundtrack*. An extreme statement coming from a researcher of sound, Chion means that there is no way to separate the auditory and visual channels of a film. We experience them only through a unified sense which he terms “audio-vision.” In a similar way, an interface that uses sound cleverly can enhance the user’s immersion and improve interaction. [Gaver \(1997\)](#) found that during an experimental process control task, the participants’ engagement increased when he provided relevant sound feedback. There is now evidence that sound can improve interaction and may be very powerful in small screen devices ([Brewster, 2002](#)). By developing more efficient auditory interfaces, interaction with machines can become easier, and hopefully more pleasant.

The most advanced auditory/haptic feedback seems to exist in computer games and multimedia products. [Gaver \(1997\)](#) claims that memory limitations in the technical product is one reason why sound feedback has not been used on a larger scale. Until quite recently it has been too expensive computationally to use sound of good quality in computers and handheld devices. Today, only lightweight electronic devices, such as mobile phones or handheld computers have limited memory capacities, although this is rapidly changing with the development of memory cards and effective compression algorithms for sound. However, nowadays these devices give various choices of discrete audio/haptic ring tones and alarms and to their users. The potential to use sound and haptics in small electronics is growing fast.

4.3 Model-Based Sonification

As there are many ways in which sound can be employed in interfaces, it is important to define the purposes of every sound at an early stage in the design process. A sound that conveys crucial information should have different attributes to one that serves as a complement to visual information. It is important to distinguish between two very different approaches (Chion, 1994): the *practical* and the *naturalistic* approach. The “practical” approach to auditory interfaces deals with sound as the main feedback. This can be the case when designing interfaces for visually impaired people, who must rely on sound feedback to provide sufficient assistance in performing a task. Furthermore, sound is often the only means of communication when using a portable hands-free device with a mobile phone. Auditory interfaces based on a practical approach should be comprehensive and simple (Brewster, 2002; Brewster and Murray, 2000; Smith and Walker, 2005; Walker and Lindsay, 2006). The drawback of this approach is sound might be noisy and tiresome over time. The “naturalistic” view regards sound mainly as a complement to a visual interface. A naturalistic interface combines sound and vision in a way as similar as possible to corresponding phenomena in the natural world. Such auditory interfaces are supposed to enhance interaction between the user and a machine, especially in situations where the visual interface is ineffective on its own. Sounds that complement a visual interface can generally be subtle background events that do not disturb. In a way, such sounds correspond to the background music of films, since they convey information to the audience without interfering with the main events. Sound feedback based on the naturalistic strategy is thus very subtle and might only be recognised subconsciously. The focus of Chapter 4 is on the “practical” approach.

Sonification is a method suggested in “practical” domain, which is defined as the use of non-speech audio to convey information. More specifically, sonification is the transformation of data relations into perceived relations in an acoustic signal for the purposes of facilitating communication or interpretation (Gaver, 1989; Beaudouin-Lafon and Gaver, 1994). Many of the major current research

areas in sonification are similar in that they focus on the identification of applications for which audition provides advantages over other modalities, especially for situations where temporal features are important or the visual modality is over-taxed. The main issues that will move sonification research forward include (1) mapping data onto appropriate sound features like volume, pitch, timbre, (2) understanding dynamic sound perception, (3) investigating auditory streaming, (4) defining and categorising salience in general auditory contexts and understanding where highly salient sonic events or patterns can surpass visual representations in data mining, and (5) developing multimodal applications of sonification (Kramer et al., 1999). Thus, sonification is a way to help in the exploration of complex data. Various kinds of information can be presented using sonification, simply by using different acoustic elements (Hermann et al., 2000).

Studies such as (Cook, 2002; Cook and Lakatos, 2003) have investigated the human ability to perceive various physical attributes of sound sources and have proved that feature-based synthesis is of use in studying the low-level acoustical properties that human listeners use to deduce the more complex physical attributes of a sound's source. The generated sounds from a set of features are correlated with the listener's perception of, e.g., size, speed, or shape of the source. Two methods of sonification have been used in this chapter, the Doppler effect and derivative volume adaptation. Both of these methods create a continuous sound for each data point. Thus, the relative position to the targets is perceived by a change of volume when passing the data point and pitch shift for Doppler effect as well. From the data points obtained in this way, we may be able to discover consistent relationships between acoustical and human-generated features that can be used to predict how a sound manifesting certain acoustic feature values will be perceived.

4.3.1 Quickening

In section 3.2.6 'Quickening' was discussed. A quickened display for a tilt controlled system like our handheld device shows the user a weighted combination of position and velocity. This weighted summation effectively anticipates the

future position of the system. An example of this is based on the Doppler effect, which highlights the user's approach to a target, or a target's movement from the current state. Another example could be derivative of volume of sound source. When the user is further from the audio source, the sound is quieter than when the user is close to it. Another predictive method that has been investigated in (Williamson et al., 2006) include *Monte Carlo* simulation in a tilt-controlled navigation system.

4.3.2 Doppler Effect

The auditory system is responsible for constructing a map of the auditory scene around us, using information from audio input. Sound localisation is the act of using aural cues to identify the location of specific sound sources (Bregman, 1990; Smith, 2004). There are various types of cues that humans can use to localise the position of a sound source. These cues can be divided into monaural and binaural cues. The two different types of monaural cue are loudness and Doppler shift. The loudness cue relies on the fact that when a sound source is far away it is quieter than when it is close by. The Doppler shift corresponds to a frequency shift associated with a sound source moving through a homogeneous medium (Smith, 2004). Pressure wave crests emerge from the sound source at intervals corresponding to the acoustic wavelength. Each crest spreads spherically out from the point of origin at the speed of sound c (Figure 4.1). The successively generated spheres of wave crests are closer together ahead of the sound source but farther apart behind the source. For a stationary observer, the measured frequency corresponds to the number of crests per unit time, therefore the composite frequencies will be higher when the observer is in front of the moving sound source and less when behind the moving sound source (Hermann et al., 2000; Hermann and Ritter, 1999). A familiar example is the shift in frequency of an ambulance siren as the vehicle approaches, passes, and then recedes. The well known lawful dependence of the Doppler shifted frequency, here denoted Ψ_t ,

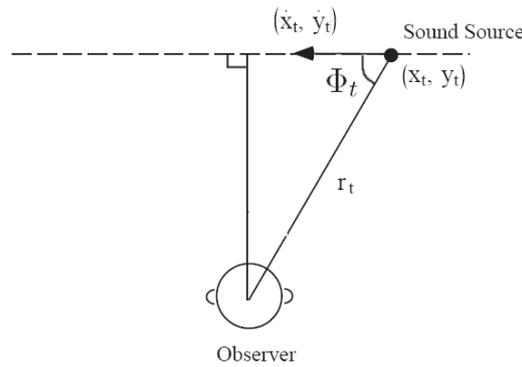


Figure 4.1: The geometry for the Doppler shift of a moving sound source relative to an observer.

on velocity of the sound source relative to an observer is:

$$\Psi_t = f \left(1 + \frac{v}{c} \cos \Phi_t \right) \quad (4.1)$$

where f is the intrinsic frequency of the sound source, v is the velocity magnitude (speed) and c is the speed of sound. The shifted frequency Ψ_t depends only on the velocity component directed toward the observer with angle Φ_t (see Figure 4.1). The shifted frequency has the maximum value when Φ_t is zero. As this angle reaches 90° , all motion is across the line of hearing and the Doppler shift is zero. This result holds true regardless of the time history of the trajectory (Jenison, 1997). These aural cues can be used to navigate through the virtual environment on a Pocket PC.

In the next sections we present advantages and disadvantages of different quickened methods and control strategies in browsing the state-space on a mobile device using tilt-input.

4.4 Experiment

4.4.1 Goals

There is a concept of accuracy explored in this chapter. The type of accuracy that is under primary consideration in this study is the capability of subjects to accurately identify audio sources in a large audio data sets with a PDA and tilt sensor using sound only. In navigating a computer display of data visually,

accuracy is seldom a concern. Using a scrollbar or clicking a 10x10 pixel icon using one's vision is trivial from the perspective of the accuracy needed to accomplish this task (Holmes, 2005). Designers of auditory displays, on the other hand, are in need of research into the accuracy that is possible in this environment. Establishing the accuracy with which humans can navigate using sound alone is an early step in integrating sound into a multi-modal information system.

The other questions we answer in this chapter are: how do people begin searching in unfamiliar spaces? What patterns or techniques are employed to accomplish the experimental task? PredictingHow will predicting the future state in the audio space change subjects' accuracy in targeting?

4.4.2 Apparatus

The experiment was conducted on a Pocket PC (hp5450), running Windows CE, with a 240×320 pixels resolution, colour display, an accelerometer Xsens P3C, 3 degree-of-freedom, refer to Section 3.4.1, attached to the serial port, which allows the users to navigate through the environment by tilting the device, and a stereo headset (Figure 4.2). The built-in vibrator unit in the Pocket PCs provides the haptic feedback in the experiment.

The experiment was written using the *FMOD* API (version 3.70CE) (FMOD, 2004), a visual programming environment with, an object-oriented language (Embedded Visual C++) used primarily to manipulate and control sound production and *GapiDraw* (version 2.04) (GAPI Draw, 2004), a runtime add-in to *FMOD* used to generate real-time Pocket PC graphics. *FMOD* and *GapiDraw* are available for free under the condition of the GNU General Public License (GPL).

Using *FMOD* and *GAPI*, an interface was developed with the following parameterisations: speed of sound, 340 ms^{-1} , Doppler factor 1.0, distance scale 100.0, minimum audible distance 80 m, full volume (255)(minimum volume is 0 and max volume is 255 in *FMOD*), and maximum audible distance 8000 m. Each pixel on the display represents 100 metres. These settings in *FMOD* simulate the Doppler effect on the PDA and provides insights about the direction of the sound source and the approximate distance from it but may not be useful in providing



Figure 4.2: (Left) Pocket PC, Accelerometer and experiment I running on the system (target sound sources displayed, for illustrative purposes). (Right) A user interacting with the system

information about the speed of the source, which humans usually guess in their everyday insights, as the distance scale is high (100 pixels) and any small tilt input causes quick changes in the volume.

An empty window (240×320 pixels) was centred on the screen. Audio sources represented by small (10×10 pixels) speaker icons are shown on the screen only for training (Figure 4.2). In the main experiment sound sources are hidden and an empty window is shown on the screen. Only the cursor, represented by a small (10×10 pixels) ear icon, is visible in both training and main experiment.¹

4.4.3 Experiment I

We first conducted a pilot study with 12 subjects, three women and nine men, all sighted, with a mean age of 29 years. Four participants were research fellows, and the rest were postgraduate students at the NUIM campus. All but one of the participants had neither experience of using Pocket PCs nor with accelerometer-based interfaces. Two of them were left-handed.

Task and Stimuli

The task in this study was to select the centre of individual targets that appear (in audio but not visually) in different locations on the screen as accurately

¹The author of this dissertation has programmed and coded all the developed applications in Chapter 4 (See Appendix D). Andrew Crossan, Frank Pollick and Sarah Dalzel-Job were great help and support in training users, running the experiments and collecting data from users.

as possible. The individual targets are audible when the cursor is in their locality, and they have full volume only in the centre of the target (imagine a Gaussian distribution of the volume centred on the target). For each target a vibration feedback has been assigned and whenever the user is in very close distance to the target, 10 pixels, s/he feels the vibration continuously. Our aim in using the vibration in this task is the vibration assures the user that s/he is very close to the centre of the target.

First, participants were asked to sit on a chair in a quiet office and were equipped with a headset and a Pocket PC in their palm. Then they were informed about the functioning of the accelerometer, Doppler effect, and the procedures of the experiment, in order to reduce the chance of any terminological misunderstanding. Subjects were asked to move the cursor to audio targets by tilting the PDA and select them by pressing a key on a small keyboard of the PDA. They were told to emphasise accuracy over speed.

Design

There were four experimental conditions: (1) No Doppler effect-no vibration feedback (2) No Doppler effect,vibration feedback, (3) Doppler effect, no vibration feedback and (4) Doppler effect, vibration feedback. The participants performed the conditions in a counterbalanced order. This resulted in 12 different orders of experiments for participants. In each experiment seven audio sources were used (a selection of different music) summarised in Table 4.1.

Table 4.1: Audio sources in first experiment in all conditions

Target Index	Music Type
1	Hip-Hop
2	Celtic
3	Arabic
4	Country
5	Jazz
6	Farsi
7	Opera

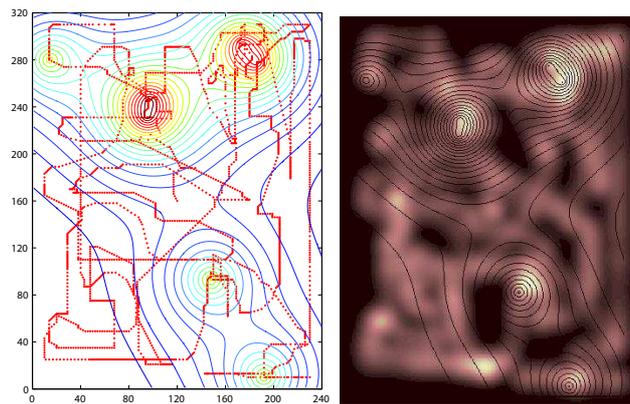


Figure 4.3: (Left) The cursor trace of the 4th participant in the “no Doppler-no vibration” condition, is plotted over the density of the local audio amplitude of the different tracks. (Right) the density contour plot and cursor trajectory density indicating the exploration of the space by the same participant in the same condition.

Visualisation

Matlab was used for visualising the logged experimental data. We use a number of techniques for investigating the users behaviour in these experiments.

Audio and Exploration Density Plots

These plots show the audio density (in pixels) at different points in the 2D space (Figure 4.3-Left). The contour indicates the density of the sum of the amplitude of the mixture components associated with the different audio tracks. The exploration density plot for visualisation of cursor trajectories used previously in (Williamson and Murray-Smith, 2004b) have been introduced here, which plots a density around the trajectory, which is a function of the position and the length of time spent in that position. These plots give some indication of how users navigated when completing the task. An example is given in Figure 4.3 (Right). This plot is created by placing a Gaussian distribution centred on the (x,y) position of the cursor for each point in the log file, with standard deviation proportional to that used in the audio sources. The Gaussians are summed for each pixel, and the resulting image gives an impression of the areas of the input space that were explored, and how long the user spent in them. The image can be summarised numerically by counting the percentage of pixels greater than a selected threshold e . In this experiment $e=5.0$. The image’s resolution is 240 by 320 pixels.

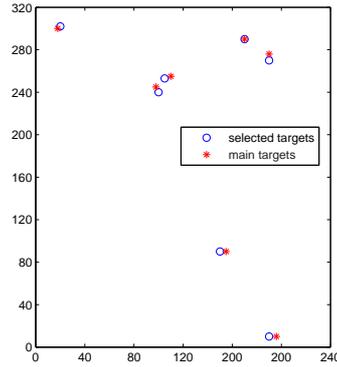


Figure 4.4: Hidden target positions (circles), and points selected by user 4 in the “no Doppler-no vibration” condition, as the best guess (crosses).

Distance to the Target

Whenever the user feels s/he is at the target, s/he presses a key indicating the selection of the target. For each selection made by the user, the distance to the nearest target is calculated as below, and recorded. An example plot is shown in Figure 4.4.

$$\text{Dist} = \sqrt{(x_{\text{source}} - x_{\text{selected}})^2 + (y_{\text{source}} - y_{\text{selected}})^2} \quad (4.2)$$

The distance to the location of the target (in pixels) gives some insight into the acuity with which the location can be perceived with the given display.

Results

Search Patterns Observed

In looking at the audio and exploration density plots, we are not attempting to establish a link between the search pattern used and the resulting measurement of accuracy. We simply make a subjective classification and qualitative assessment of the types of search patterns employed to accomplish the task. A subject may employ one of the search techniques and still not be very accurate, or they may be very accurate in spite of using no detectable systematic pattern. However, this factor gives an indication about the ease with which the audio environment could be clearly perceived by participants. In a clear and easy to navigate environment, with appropriate feedback, this should be similar to the

density of targets, and linked to the smoothing used.

Some of the terms and their basic definitions used here are taken from search theory, a sub-field within operations research ([Civil Air Patrol – Reserve Air Patrol, 1999](#)). The patterns developed by search theory are visual search patterns of physical space, but there is some crossover in the types of patterns used in the auditory interface used in the experiment to search in a virtual space.

1. Parallel Sweep – The parallel sweep is used when uniform coverage of an area is desired and the area is unfamiliar. It is an efficient method of searching a large area in a minimum amount of time. Several subjects used the horizontal parallel sweep, ‘raster scan’, similar to the one seen in Figures 4.5(a) or 4.6. This pattern can be related to the text reading pattern we learn in the childhood.
2. Quadrant Search – The quadrant search pattern is one in which the searcher mentally breaks down the screen into quadrants to divide the area into a more manageable size. Within the quadrants, the searcher may use another pattern to search each quadrant, such as a parallel sweep (Figure 4.7(a)).
3. Sector Search – A sector search pattern begins once the approximate location of the target is located. In this pattern, the searcher explores out from the approximate location of the target and returns again, then conducts another exploration in another area, and returns again. This is repeated until they are confident that the space is adequately explored (Figure 4.7(b)).
4. Perimeter Search – The perimeter search is one in which the boundaries of the space are explored, but little or none of the middle is traversed. The pattern of search can be a circle to circumscribe the border or a square shaped pattern turning at a 90° angle. This type of search pattern would typically lead to inaccuracy given that the target on all of the areas is not located at the perimeter. This search pattern was not observed in this research.
5. No Formulaic Search – For some searchers, no discernable systematic tech-

nique was employed in exploring the space to accomplish the task. For these search patterns, there is no attempt to thoroughly explore the information space. Figure 4.7(c) illustrates the path used in the only trial to actually select the target exactly.

The search patterns of each subject were analysed to see if there were any tendencies based on demographic characteristics. 48 total patterns were analysed. The most common technique employed was the sweep search (76%). The next most common was the no distinguishable pattern (14%), followed by quadrant (6%), and sector (4%). Participants' audio and exploration density plots show "Doppler-no vibration" has the least covered space with 34.5% and the rest have similar percentage of coverage, 37.6%.

Chosen Songs

The accuracy relative to the number of chosen songs is another factor in improving audio interfaces; because the type of songs may affect the perception of distortion due to the Doppler effect and affect the users' ability to recognise and locate them. We measured the number of audio sources participants have selected. The mean accuracy for each of these sources has been summarised in Table 4.2. Figure 4.9 shows the mean accuracy count of songs in all conditions for all participants. This result is based on the number of times each source was selected with the smallest distance to the target in each condition. There is a large amount of variability in the results. Jazz music was selected more than others on average. But Hip-hop music was chosen more accurately in the "no Doppler-no vibration" condition. Figure 4.10 shows mean error for songs in all conditions. In general "no Doppler-no vibration" has the lowest error among others and "Doppler-no vibration" has the highest error. Farsi and Arabic sources had high mean and maximum errors in the Doppler case.

Discussion

Post hoc examinations of the cursor's trace in this experiment showed that the subjects tended to use the same technique regardless of the sounds they heard and the audio condition. 6 subjects (50%) used one search technique exclusively.

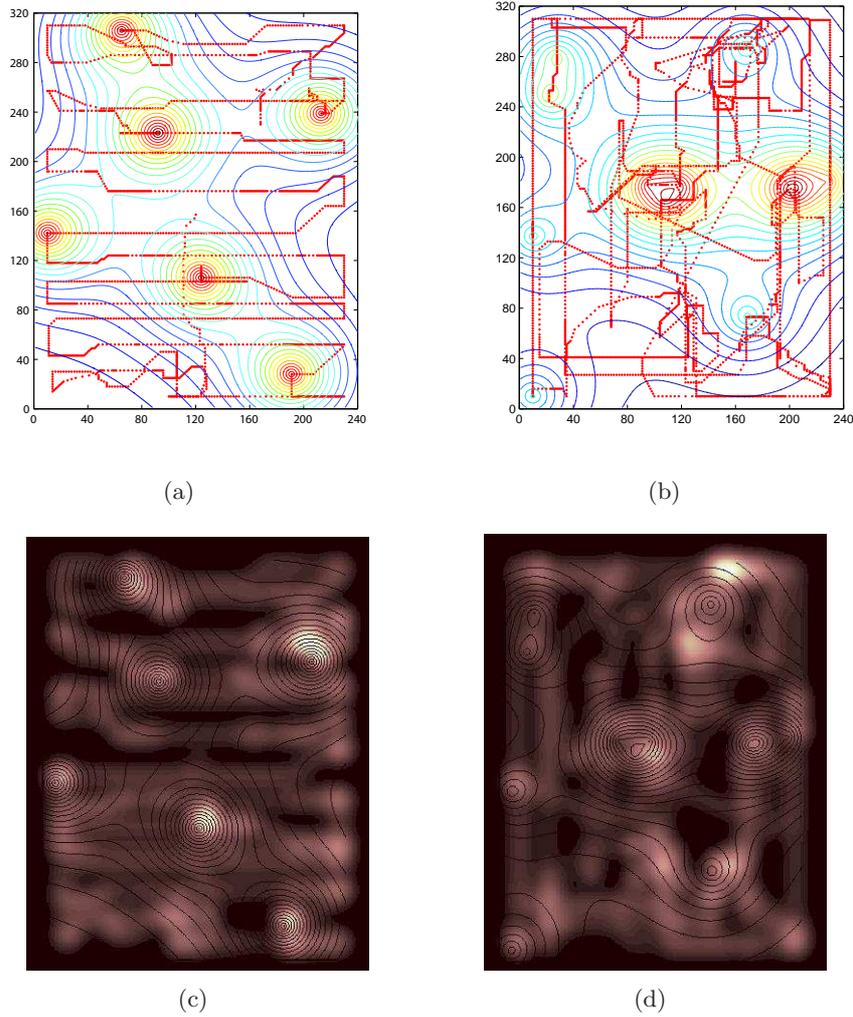


Figure 4.5: (Left) The traces of the cursor for participant 12 in “no Doppler with vibration” experiment (a) and its exploration density plot (c), (Right) The traces of the cursor for participant 6 in “Doppler with vibration” experiment (b) and exploration density plot of this experiment (d).

Of these 6 subjects, 5 used the sweep technique, 1 used no distinguishable pattern exclusively. Another 6 subjects (50%) used the same technique in 2 out of the 4 conditions. This consistency in the application of a searching technique has several notable points. First, the same technique was employed regardless of the sound treatment. This would indicate that the subjects brought with them a technique that was not altered by the change in the treatments used in the auditory interface. The subjects were given no experimental feedback that might prompt them to change their search pattern to one that might be more effective. Left to their own means, the subjects tended to continue with the application of

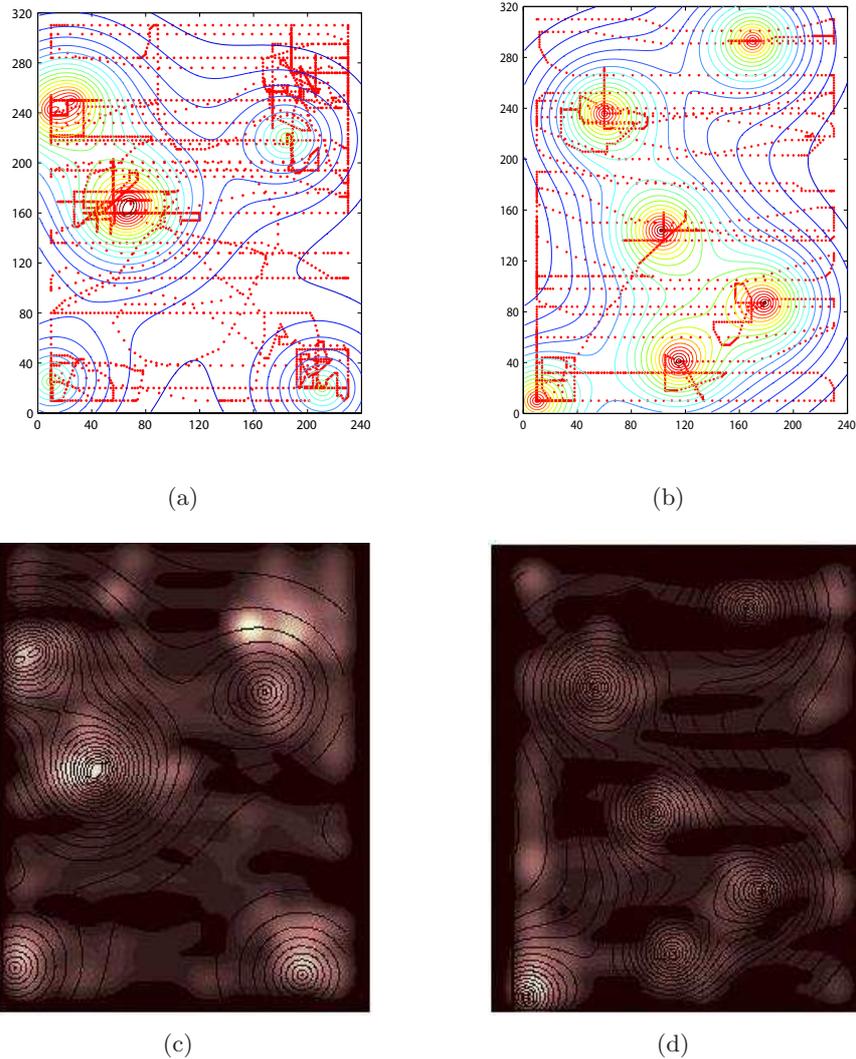
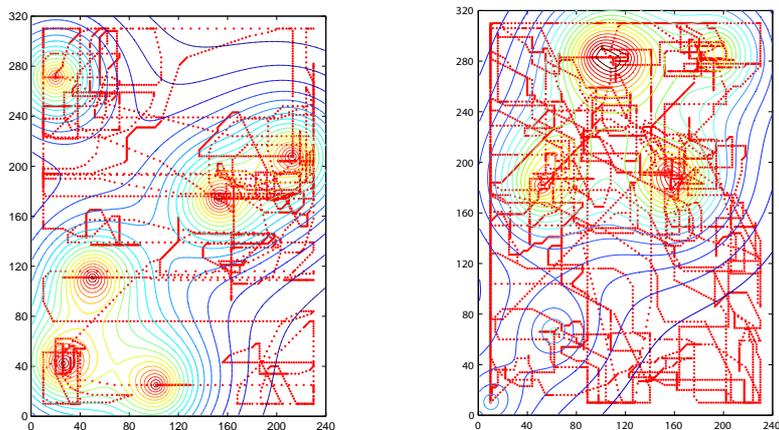


Figure 4.6: (Left) The traces of the cursor for participant 5 in “Doppler with vibration” experiment, (Right) The traces of the cursor for participant 9 in “no Doppler with vibration” experiment.

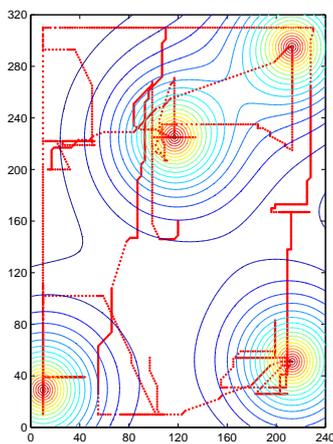
the search pattern they felt most comfortable. Second, the most common type of search pattern (sweep search) was also the least effective given the target in all four conditions was located towards the interior of the information space. In these cases, the subject was less likely to notice a change in the sounds they were hearing because of the low intensity of the sounds generated at the borders of the information space. Because they typically did not explore the interior they would not hear the more intense sounds that might lead them to the target. In conditions with vibration feedback sweep search is combined with circular movements around the vibration source (Figures 4.5(a), 4.6(a), and 4.6(b)) and has

4.4 Experiment



(a) Example of quadrant search:
Subject 9, “Doppler-no vibration”

(b) Example of sector search: Sub-
ject 1, “no Doppler-no vibration”



(c) Example of no formulaic search:
Subject 7, “Doppler-no vibration”

Figure 4.7: Examples of few search patterns in different conditions.

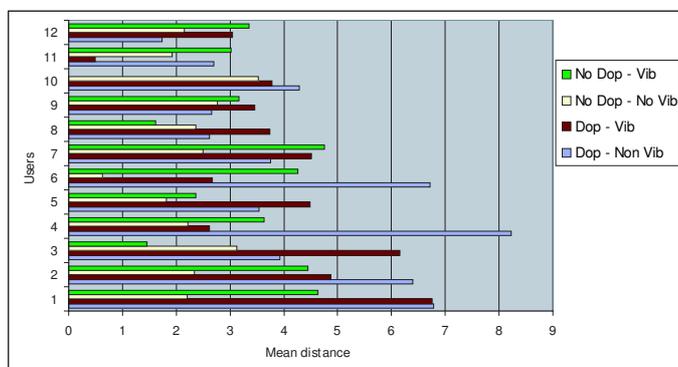


Figure 4.8: Mean distance in pixels from target in different tasks.

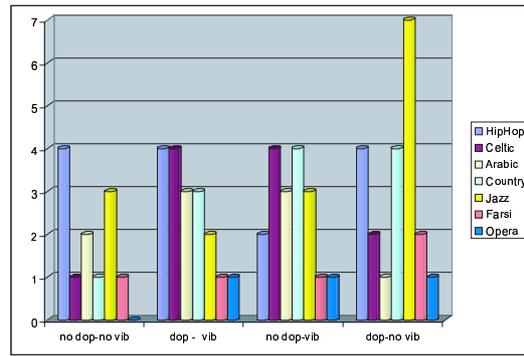


Figure 4.9: Count of most accurately chosen songs in different conditions for all users.

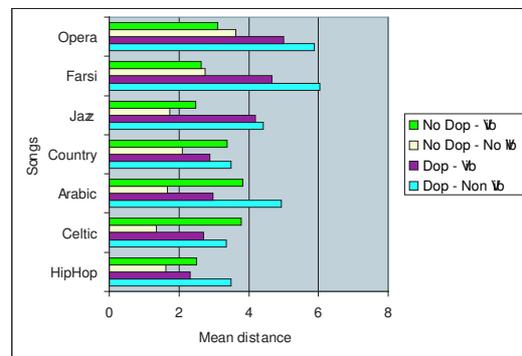


Figure 4.10: Mean distance (pixels) of selected songs in all conditions for all users.

Table 4.2: Accuracy score for audio sources in the first experiment.

-	no dop- no vib	dop-vib	no dop-vib	dop-no vib
Hip-Hop	4	4	2	4
Celtic	1	4	4	2
Arabic	2	3	3	1
Country	1	3	4	4
Jazz	3	2	2	7
Farsi	1	1	1	2
Opera	0	1	1	1

led the users to the target. This suggests that the vibration was more important for the users in locating a target and whenever they felt they are close to the song they looked for the vibration source before clicking, thus feeling a vibration source meant they were at the centre of the audio source. This might, however, also explain the fact that errors are not smaller, as the user may often have selected the location as soon as the vibration was perceived, at the edge of the circle, rather than at the centre of the target itself.

The “no formulaic search” is the least thorough of the systematic techniques. Even though there was essentially no effort involved in exploring more thoroughly by applying a different search pattern, the subjects tended to use the no distinguishable search pattern. This could be accounted for by assumptions the subjects made about the nature of the information space. It would seem that some subjects took the experimental task seriously by systematically exploring the information space. Other subjects did not seem to be interested in exploration, but instead made a quick “stab” in the general direction of the audio source. The case could be made that those subjects who explored liked the sonic interface and those who did not explore did not like the interface. It may well be the case that auditory display is not for everyone. Some will like it and make use of it, others will not.

Furthermore, the results show that the mean distance from the selected position to the target in “no Doppler-no vibration” is less than other experiments (Figure 4.8). The extra clicks and navigation activities in the cursor trajectories for Doppler might be an effect of the extra sensitivity of the feedback to movement, which makes the users explore by varying their velocity vector. Variability in localisation accuracy is greater with the Doppler effect for the Farsi and Arabic sources, suggesting that for the mainly western European participants, their poorer familiarity with these sources made the distortions introduced by the Doppler effect more difficult to perceive. Opera also had larger errors, again suggesting that less familiarity with the target sources can affect the usefulness of this approach. The large number of falsely placed points for the Doppler method might be because of the amplification involved in moving towards something and potentially frequency and speed of sound, which makes people feel they are getting a stronger response, and they over-interpret the quickened signal, believing they are already at the point – a common cited risk associated with quickened displays (Poulton, 1974).

4.4.4 Experiment II

24 paid participants (8 male, 16 female), all sighted with normal or corrected vision and normal hearing with mean age 24 were recruited through sign up sheets in Glasgow University Psychology department and through e-mail. Two of the participants were left-handed. Three participants had experience using a Pocket PC, and of these, one had frequent use. None had experience using an accelerometer as an input device.

Design

Given that the results of the pilot study showed we had possible confounding factors, i.e. four different audio conditions, haptic feedback, few subjects, unfamiliar songs and random located targets, the next experiment reduced the number of independent variables. This resulted in 3 different types of audio feedback without haptic feedback:

1. Doppler feedback,
2. Derivative volume adaptation,
3. No Quickening.

There were 8 possible audio sources (targets) arranged in a circle (radius = 100 pixels) around the centre at 45° intervals (Figure 4.11). The audio feedback at the centre was jazz music, which played continuously for all conditions. When an outside target was to be located, the audio feedback was “Hotel California” played in a loop. The audio source to be located alternated between the centre (jazz music) and one of the outside targets (“Hotel California”), and always began with the centre target. The audio sources around the outside were presented in a random order, twice for each target for the training session (16 trials in all), and five times for each target for the experimental trial (40 trials altogether). Once one target had been located, a button was pressed. For each key pressing there was a screen colour change and a short “beep” sound. Audio was noticeable within a radius of 90 pixels from sources (3δ) in conditions 1 and 2 but audio

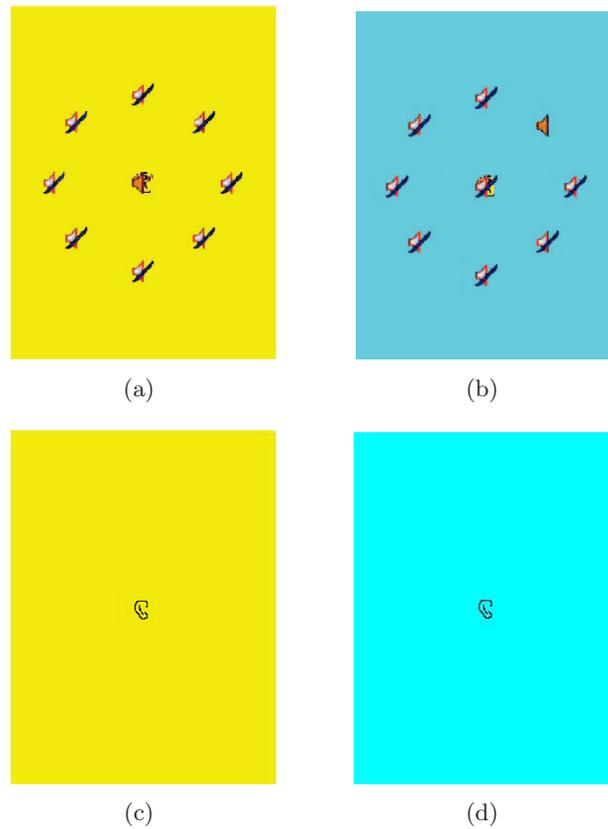


Figure 4.11: The state space in experiment II and corresponding angles. Top pictures show the training application and bottom ones show the main application. Left pictures show the screen before pressing the button for Jazz music and right ones show the screen after pressing the button (colour changes and covered speakers are indicated in training application).

was noticeable just within a radius of 15 pixels from the sources in condition 3 and there was no feedback at any other locations in this condition. Each participant was tested individually and participants were told to commence the training session when they felt ready, and after the training session it was ensured that they understood the procedure fully and that they felt comfortable using the equipment. They were given a break between the training and experimental sessions if they wanted one.

Visualisation

In addition to exploration and audio density plots and distance to the target, we used another visualisation method which measures the orientation of each target with respect to the centre point, showing which angles in the state space

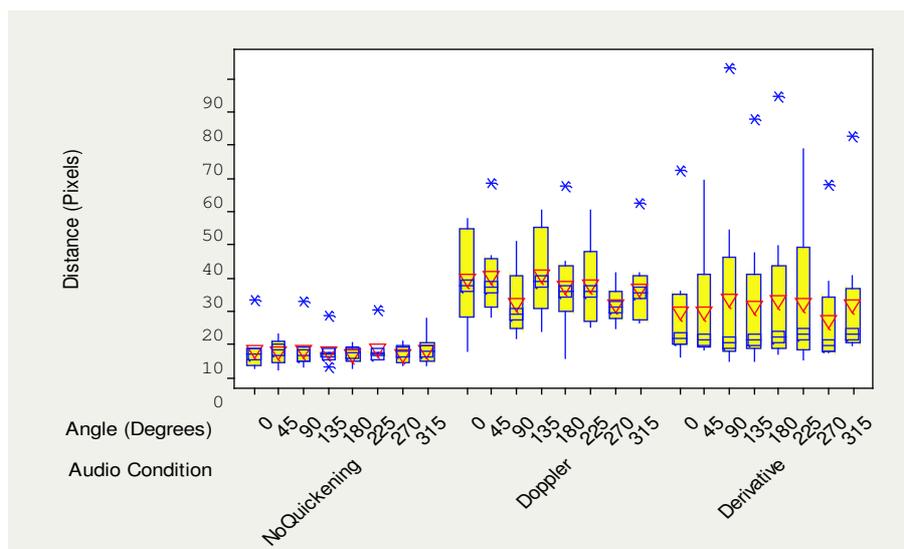


Figure 4.12: Boxplot of distance versus audio conditions and angles.

have had the most accurate data in selecting targets. This measurement is important in this experiment to see whether the orientation of audio sources has any effect on targeting task. Results in this experiment were analysed using a *GLM ANOVA* test.

Results

Proportion of distance to the target

Figure 4.12 shows the box plot of medians, means and measures of spread of the distance between the audio sources and the position selected for each of the three audio feedbacks. The red triangle indicates the mean and the blue square indicates the median (50% of the observations lie below this line). The top of each box indicates the upper quartile (75% of the observations lie below this point) and the bottom indicates the lower quartile (25% of the observations lie below this point). The tops of the lines above the boxes indicate the highest observation, and the bottom of the lower line indicates the lowest observation. The blue stars indicate outliers: those observations that differ significantly from the mean. Figures 4.12 and 4.13 show a difference in the average distances between the actual audio source and the target selected (accuracy) for the three audio conditions. The most accurate target selection occurred in the no-quickenning

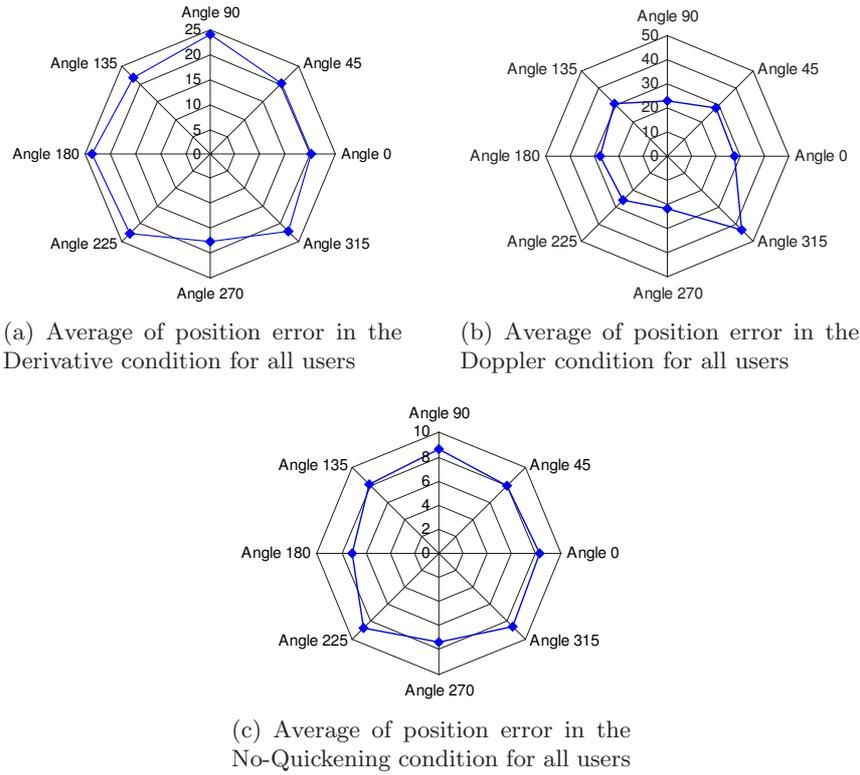


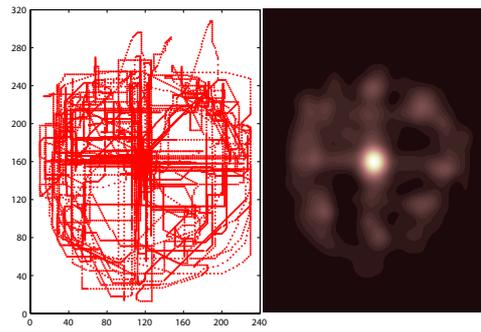
Figure 4.13: Average of position error in pixels for all participants in three audio conditions.

condition, and there was little difference between the levels of accuracy for each orientation. The spread for no quickening was very small, and the 5 outliers are not very far away from the median, suggesting that, overall, most people in this condition took approximately the same length of time to select a target. The derivative condition takes longer overall than the no-quickenning condition. The spread is larger (largest of all three conditions) and the outliers further away from the median than in the no-quickenning condition. The participants in the Doppler condition took longer on average to select the targets, compared with those in the other two conditions. The spread in the Doppler condition is smaller than in the derivative condition, but larger than in the no-quickenning condition. This shows that angles 90° and 270° have higher accuracy. In the *GLM ANOVA* analysis it was found that there was a significant effect of audio type on the distance ($F(2,21)=4.345$; $p<0.05$). There were, however, no significant differences between the 8 audio orientations. Post-hoc analysis using a *Tukey* test showed that there was a significant difference between the estimated mean distances

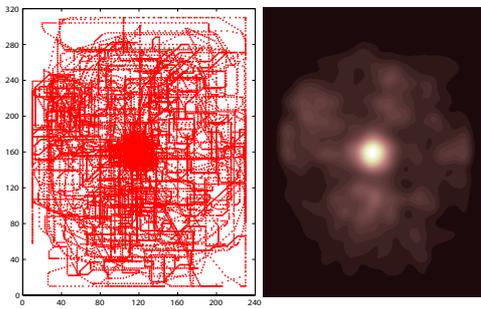
of the selected targets away from the audio sources in two of the three audio conditions. It was found that the mean distances were not significantly different between two quickening feedbacks and non-quickening condition ($p < 0.087$). The *Tukey* test showed that there was no significant difference between the estimated mean distances of the selected targets away from the audio sources in the derivative condition. Running this test on Doppler results revealed that a significant difference ($p < 0.025$) between the estimated mean distances of the two selected targets away from the 8 audio orientations (90° and 270°). In the no-quickening condition, the *Tukey* test showed that there is no significant difference among the estimated mean distances of the selected targets away from the audio sources.

Search Patterns and Covered Space

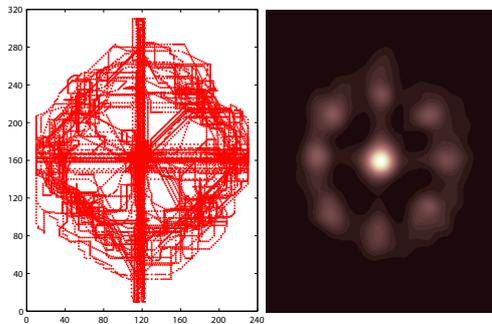
In this experiment audio targets had fixed positions in the state space so the observed search patterns were different than those we found in the pilot study. 24 total patterns were analysed in this experiment. From the training sessions subjects knew the approximate location of the audio sources so in 100% of search patterns in the no-quickening condition the subjects moved to the edge of a circle in the size of the actual radius of the points and started circling to find the active target. In the Doppler condition 87% of subjects could guess in which direction the target was located and after doing a few back and forth movements they landed on the target. Subjects, therefore, followed a sector search pattern. Search patterns of subjects who worked with derivative volume adaptation were mixture of the patterns of the no-quickening and Doppler conditions. Figure 4.14 shows some of subjects' trajectories and density plots in different conditions. Figure 4.15 shows the percentage of the screen covered by participants' movement in 3 conditions. In the derivative condition, the top-left sections (90° - 180°) were explored more than other parts. In the Doppler condition the top-right (0° - 90°) sections were popular to explore and in "no quickening" there was no significant difference in the sections covered by participants' movement and all of the partitions were explored equally. These plots show the Doppler condition had the most covered space with 44.5% and the rest had a similar percentage of coverage, 39%.



(a) Trajectory and density plot of subject 4 in Derivative



(b) Trajectory and density plot of subject 4 in Doppler



(c) Trajectory and density plot of subject 5 in no-quickenig

Figure 4.14: Trajectories of different subjects in three audio conditions.

Discussion

In this experiment it was found that there was an effect of audio condition on the level of accuracy. When the feedback was no quickening, participants were more accurate than when the feedback was Doppler or derivative. This is due to

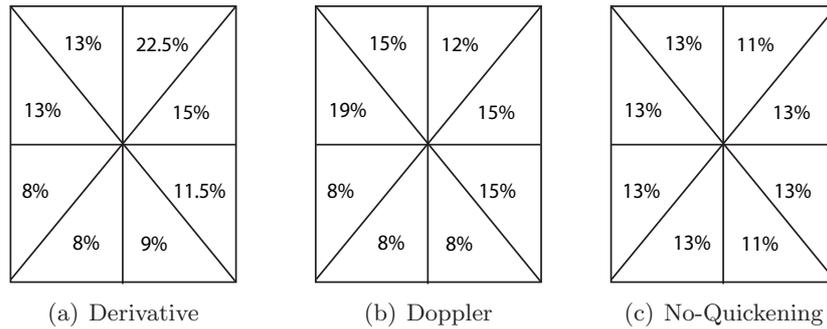
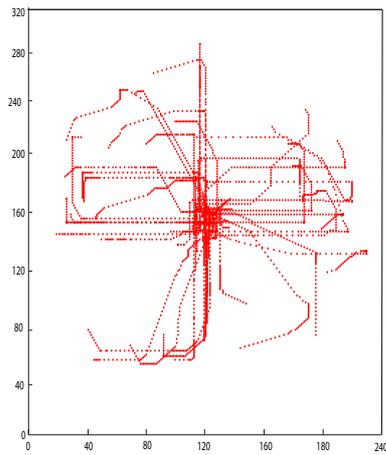


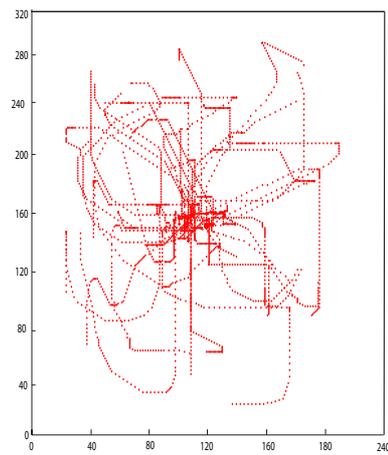
Figure 4.15: Percentage of the screen covered by users’ movement in different conditions. The variance of the coverage in the derivative condition is 0.0023, in the Doppler condition is 0.0017 and in the no-quickenning condition is 8.5714e-005.

the fact that with the no-quickenning condition, the only time that audio feedback is heard is when the cursor is directly over the target, and the difference between hearing and not hearing audio feedback is larger than the difference between hearing different levels of audio feedback. There was also found to be no effect of angle. The level of accuracy was the same, irrespective of the orientation of the target.

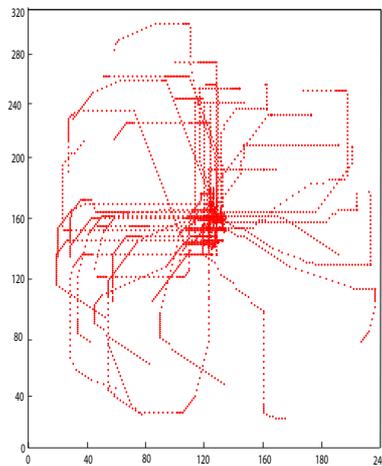
Many participants reported that sometimes they would just “land” on the audio source by chance, and at other times they would search for a long time and still not feel they had located the point accurately. This was an especially common complaint by participants in the Doppler condition. Disorganised search patterns observed in the Doppler condition, for instance in Figure 4.14 (b) may correspond with the claim made by some participants that by the time they had established where the target was through the audio feedback, they had already passed the audio source, and had to go back to it. We plotted users’ trajectories when they had moved from the centre of the screen to any active audio source around the centre. Figure 16 (b) and other users’ trajectories in the Doppler condition highlight that in the first moments after audio source activation, the subjects could guess the direction (left or right side of the space) and approximate position of the target, and consequently moved towards the target correctly, but it was difficult to establish a correct target acquisition and they made some back and forth or up-down movements to land on the target, which is compatible with the observed sector search pattern. This is shown more clearly



(a) Trajectory and density plot of subject 1 in Derivative case



(b) Trajectory of subject 4 in Doppler case



(c) Trajectory of subject 4 in No Qui-ckening case

Figure 4.16: Trajectories of different subjects in three audio conditions when they have moved from the centre to outlying active audio sources.

in Figure 4.17 (a-left) and the user's trajectories as time series in Figure 4.17 (b-left) in an individual target acquisition task when the user has moved from the centre to the target in angle 45° , which has been activated. Figures 4.14(a) and 4.16(a) shows a trajectory that is fairly typical for most participants in the derivative condition. It can be seen that the trajectory is far more ordered, with participants moving in the horizontal and vertical directions (in the directions of 0° , 90° , 180° and 270°), more so than in the Doppler condition. It becomes obvious that participants moved in a circular motion that they learnt during the training session, far more so than those in the Doppler condition. From this,

4.4 Experiment

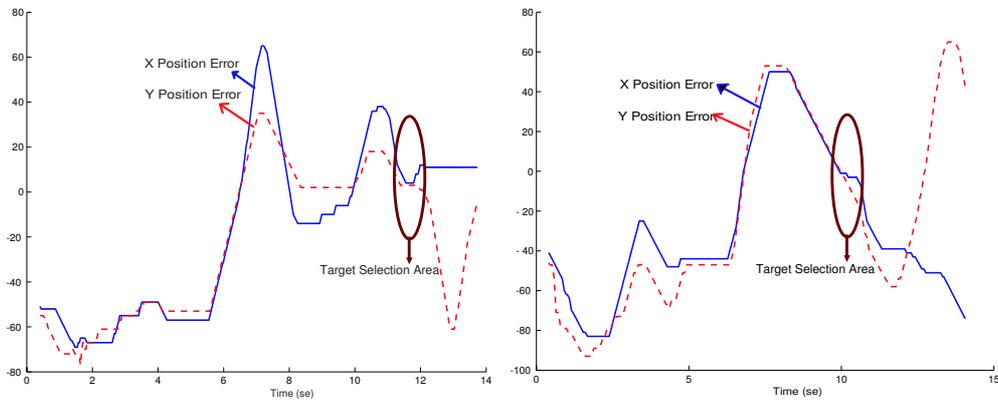
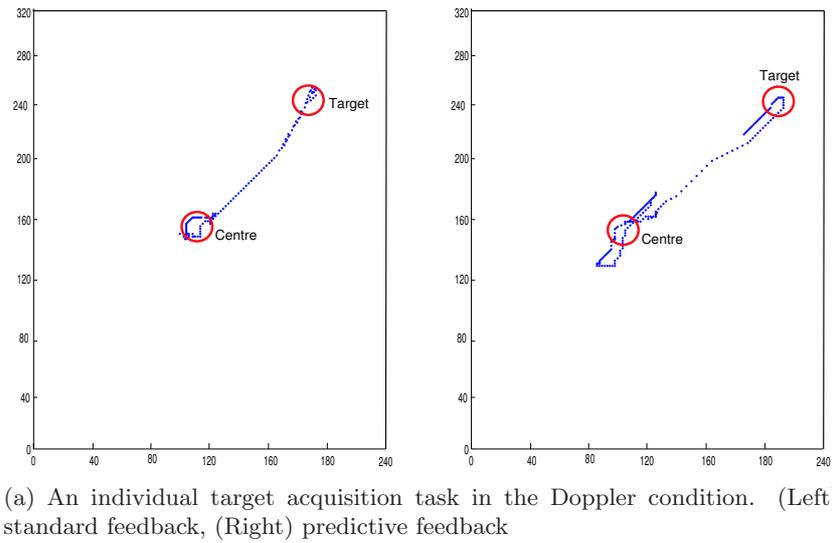
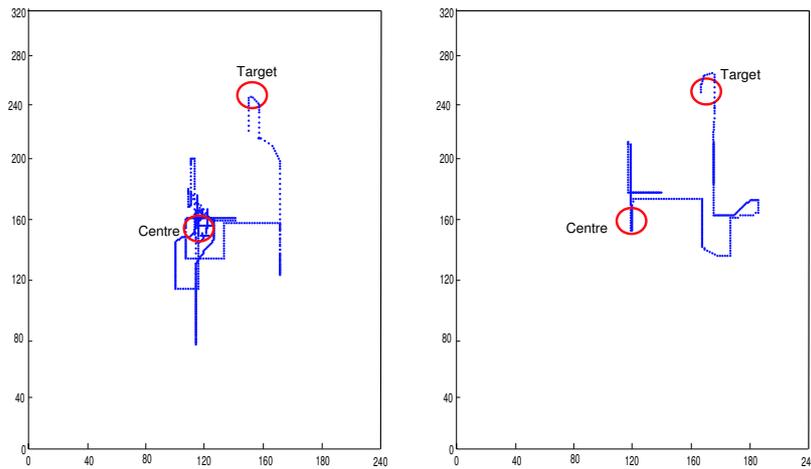
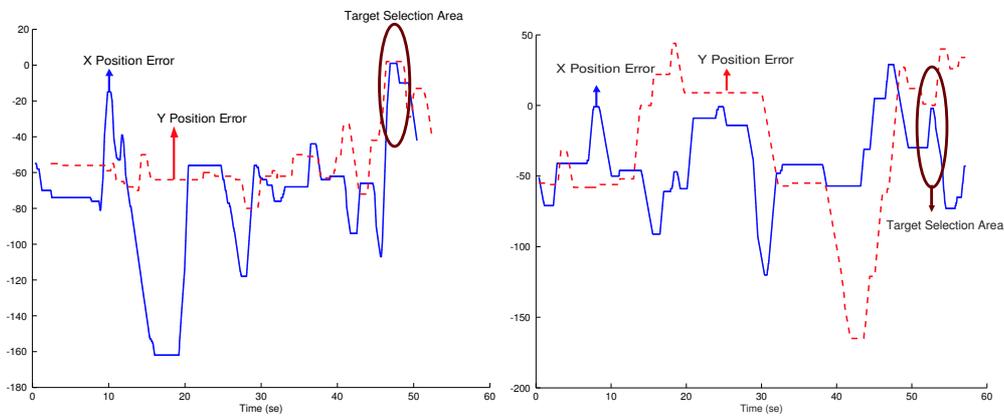


Figure 4.17: (A) One of the participants' trajectories in the Doppler condition with and without predictive feedback in an individual target acquisition task when the user has moved from the centre to an activated target in angle 45° . (B) The time series of the participant's X and Y position error in the same task.

they have established that the audio sources in the experimental session were also arranged in a circle. This suggests that they were not necessarily using only audio feedback, but also prior knowledge about the probable locations of the audio sources. Since this circle is not as clearly defined in the Doppler trajectories, it suggests that participants in the Doppler condition were using predictive information, but were also less able to control their movements efficiently. There is a risk that any significant effects were masked by prior knowledge of the way the audio sources were arranged and visual feedback has affected the users behaviour



(a) An individual target acquisition task in the Derivative condition (Left) standard feedback, (Right) predictive feedback



(b) The time series of one of the participants' position error in X and Y axis in the target acquisition shown above, in the Derivative condition (Left) standard feedback, (Right) predictive feedback

Figure 4.18: (A) One of the participants' trajectories in the derivative condition with and without predictive feedback, in an individual target acquisition task when the user has moved from the centre to an activated target in angle 45° . (B) The time series of the participant's X and Y position error in the same task.

in exploring the audio space. Figures 4.16(a) and 4.18(a-left) provides a clearer picture of the users' browsing behaviour in this condition. As a result of the first impressions that the users have received from the volume of the audio source they have chosen vertical or horizontal directions. Whenever they have not found the target in these directions, for instance in an individual target acquisition in angle 45° presented in Figure 4.18, they have moved around the circle using prior knowledge of the landscape. Moreover, Figure 4.14(c) shows a more pronounced circle and cross-shape for the no-quicken condition. Since the participants in

the no-quicken condition were presented with no aural feedback except when directly over the target, it is, most likely that they were relying on the circular target distribution previously seen in the training. This led to a systematic search strategy, less ‘browsing around’ because of the lack of predictive ability without quickening. All users who participated in this condition claimed that this was not an exciting method of exploring the auditory space.

4.4.5 Human Operator Modeling

Interaction with auditory interfaces is an example of *continuous interaction* which was discussed in Section 3.3.1. In these systems which rely heavily on the tracking of hand in a simulated environment the pretence of reality requires a tight coupling between the user’s view and hearing of the environment and the actions, hand motions, that set the view and hearing. Thus the performance is adversely affected when the feedback is subject to delay or lag (Jagacinski and Flach, 2003; MacKenzie and Ware, 1993).

Using the platform in the previous experiment, we carried out a preliminary investigation to measure and model the accuracy, and bandwidth of human motor-sensory performance in interactive tasks subject to lag. We kept the same format of the second experiment but instead of providing audio feedback to the user’s current position we provided feedback to the user’s predicted position calculated according to equation (3.12) in Section 3.3.1:

$$X_{t+\tau} = X_t + V\tau \tag{4.3}$$

The volume of the audio source, which provides feedback about the target’s position, is a function of the user’s current velocity and position. Here, $X_{t+\tau}$ and X_t are the user’s position at time $t + \tau$ and t or current position and next possible position respectively. τ is the human’s time-delay or reflection time (refer to Section 3.3.1 on page 51), which becomes our ‘prediction horizon’ for the predictive model, and V is the user’s speed of motion in the audio space. This has the effect that, as the user moves toward the target s/he feels him/herself in

the position predicted to be reached at time $t + \tau$.

Design

In the second experimental setup we added a smooth drop-off in the time horizon of the prediction, as the target is approached. The fall off began at radius 15 pixels, and once the user was within 5 pixels of the source the feedback reverted to standard feedback with no predictive element.

In a pilot study we ran the application for three participants familiar with the Pocket PCs and accelerometer. Neither felt any difference in the two derivative conditions, with and without prediction. In Figures 4.18(a) and 4.19(b) we see one of the participant's trajectories when he has moved from the centre to any active target. Providing feedback to the user's future position in the derivative condition has not much changed the user's exploratory behaviour. But users reported a great difference between Doppler with the predictive model-based feedback and Doppler with no predictive feedback. They said it felt they were able to acquire the direction of the audio source more quickly in the predictive case, but that it was a more difficult to land on the source. In the standard model with no predictive element they felt it was slower to find the direction but easier to land. Despite their perceptions, the trajectories in Figures 4.17(a-right) and 4.19(a) suggest the opposite case, that they performed fewer oscillatory movements around the target in the predictive model, compared to the standard case.

Prediction in the Doppler case allowed the users to converge more rapidly and directly to the target, but it seemed less helpful very close to the target. In the derivative condition predictive feedback seems to have smoothed the behaviour, but has not improved the initial target localisation. These preliminary explorations suggest that a more detailed investigation of incorporating the predictive element in the feedback system would be of interest.

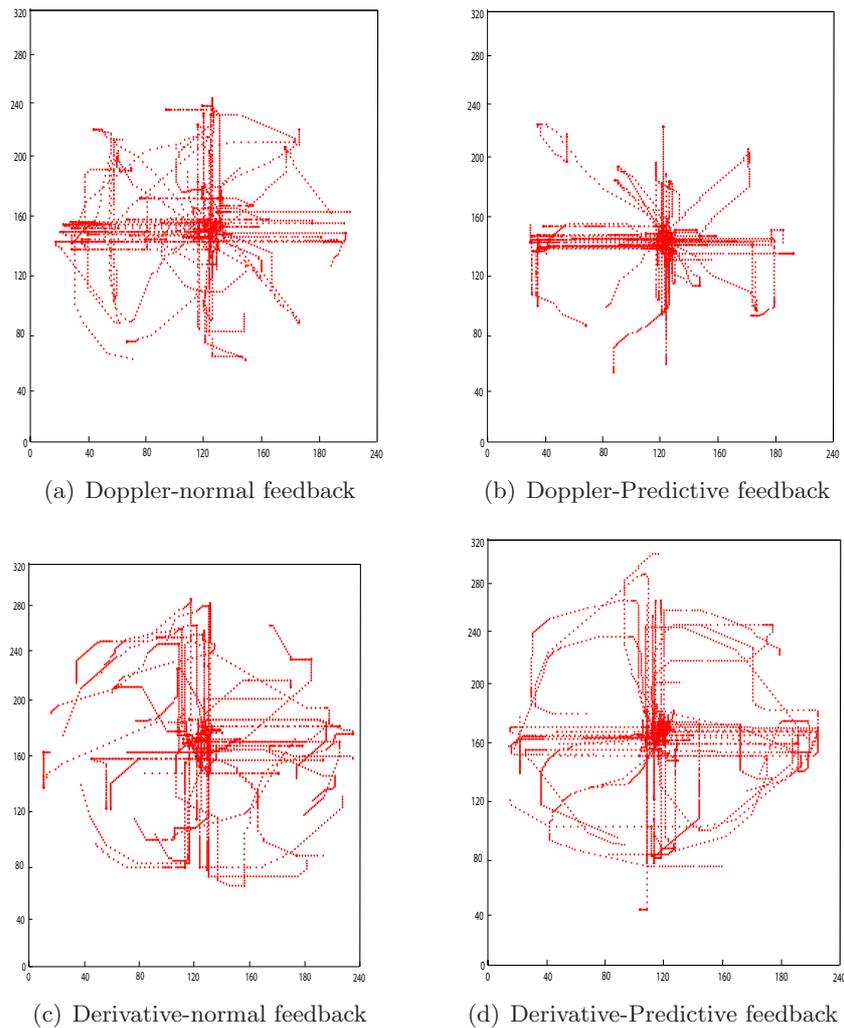


Figure 4.19: The trajectories of two subjects in the Doppler and derivative conditions, without and with predictive feedback.

4.5 Conclusions and Summary

This chapter presented initial experimental results exploring the use of quickened audio displays for localisation and selection based on tilt control of mobile devices. The experiments provided useful exploratory information about how users navigate in such environments, and highlighted some benefits and disadvantages of each of the display options investigated. Users used a search method, which they felt more comfortable with for browsing the space regardless of the sound treatment. Vibration was clearly perceived by users, but led them to spend more time circling around targets.

Average results in the pilot study on the metrics used suggest that partici-

pants were more accurate in target selection in the “no Doppler-no vibration” than other conditions. The results do not suggest that the use of Doppler or vibration brought consistently improved accuracy, but some people did very well with Doppler and most stated that they found the vibration feedback useful. Longer studies might show different use in real-life tasks once users had familiarised themselves with the system.

The main study represented a more focused investigation, with fewer confounding factors. We increased the number of participants, placed all the targets at equal distances from the starting point (centre of the screen), did not include haptic feedback, chose western pop music which was familiar to all users, and specified more time for allowing users to learn how to use the specific interface, which was new to all. We investigated whether quickening was more useful to users searching for targets in state-space than no quickening audio feedback. We also investigated if there was any advantage of using Doppler feedback over derivative, and if there was an effect of orientation in either Doppler, derivative or no quickening, and therefore to find out if the results of the first experiment could have been masked by an interaction with the orientation of the targets. It was also found that there was no effect of the angle at which the audio source was located.

In a preliminary investigation to better understanding the results and to guide future work, we performed an explanatory experiment with predictive model-based feedback. The model is based on human operator modeling in continuous tracking tasks, and it could take human response delays and lags into account (not considered in this Chapter). Using this predictive model, we could improve the users’ performance in the Doppler condition and reduce their overshoots during landing on the target just by providing audio feedback about the user’s predicted position instead of their current position. This suggests that further research to investigate the benefits of explicitly incorporating models of human behaviour in the design of feedback methods. More studies need to be done to find out how much does this method improve the users’ performance in the audio/haptic interfaces? Does this method reduce the user’s overshoots when

they are targeting just by providing the multimodal feedback about the user's predicted position instead of his/her current position?

As discussed earlier in Chapter 2, Fitts' law has not been successful in auditory interfaces but it would be interesting to study Hick's law, or the Hick-Hyman law (Hick, 1952; Hyman, 1953) in auditory/haptic interfaces where targets are located or activated randomly similar to the application described in this chapter. This study may answer questions, for example, how long do users need to familiarise themselves with the system?

The results in this chapter are a useful starting point for further investigation into the types of feedback that are most useful and informative in assisting users of a tilt-controlled Pocket PC and sonified interface. Further development of the techniques and experimental design employed in this study will allow manufacturers of such devices to incorporate the most effective type of feedback into their products.

In the following chapters we focus more on tilt-controlled interfaces, models of human behaviour in the design of audio/visual feedback methods and human response delays.

Chapter 5

Tilt-Controlled Zooming User Interfaces on Mobile Devices

This chapter provides a dynamic system interpretation of the coupling of internal states involved in speed-dependent automatic zooming, and we test our implementation on a text browser on a Pocket PC instrumented with an accelerometer. The dynamic systems approach to the design of such continuous interaction interfaces allows to simulate and use analytical tools to analyse the behaviour and stability of the controlled system alone and when it is coupled with a manual control model of user behaviour and calibrate and tune the parameters of the system before the actual implementation. Furthermore, it is shown that browsing and targeting can be facilitated by using a model-based sonification approach to generate audio/vibrotactile feedback about document structure, in the proposed interface for a text-browser. We show examples of audio/vibrotactile feedback and illustrate that multimodal feedback provides valuable information, supporting intermittent interaction, i.e., allowing movement-based interaction techniques to continue for a blindfolded user.

5.1 Introduction

Navigation techniques such as scrolling (or panning) and zooming are essential components of mobile device applications such as map browsing and reading text documents, allowing the user to access to a larger information space than can be viewed on the small screen. Scrolling allows the user to move to different

locations, while zooming allows the user to view a target at different scales. However, the restrictions in screen space on mobile devices make it difficult to browse a large document efficiently. Using the traditional scroll bar, the user must move back and forth between the document and the scroll bar, which can increase the effort required to use the interface. In addition, in a long document, a small movement of the handle can cause a sudden jump to a distant location, resulting in disorientation and frustration (Brewster et al., 1994).

Speed-dependent automatic zooming is a relatively new navigation technique (Cockburn et al., 2003; Cockburn and Savage, 2003; Igarashi and Hinckely, 2000; Savage, 2004; Wallace, 2003; Wallace et al., 2004) that unifies rate-based scrolling and zooming to overcome these limitations. The user controls the scrolling speed only, and the system automatically adjusts the zoom level so that the speed of visual flow across the screen remains constant. Using this technique, the user can smoothly locate a distant target in a large document without having to manually interweave zooming and scrolling, and without becoming disoriented by extreme visual flow. In this chapter we demonstrate that, as suggested by Igarashi and Hinckely (2000), speed-dependent automatic zooming (SDAZ) is well suited to implementation on mobile devices instrumented with tilt sensors, which can then be comfortably controlled in a single-handed fashion. We also describe an alternative stylus-controlled implementation for the Pocket PC. A further contribution is the use of a state-space formulation of speed dependent zooming, which we believe is a promising reformulation of the technique, which opens the path to the use of analytic tools from optimal and manual control theory.

Next, we show that browsing and targeting can be facilitated by using a model-based sonification approach to generate audio feedback about document structure in the text browser interface. This supports intermittent interaction and allows movement-based interaction to continue while the user is simultaneously involved with other tasks.

5.2 Related Work

5.2.1 Alternative Scrolling Techniques

Several alternations to traditional scroll bars have been proposed. They allow the user to control scrolling speed, enabling fine positioning in large documents. The *AlphaSlider* (Ahlberg and Shneiderman, 1994) and *FineSlider* (Masui et al., 1995) are two alternative scrolling techniques for precise selection in large lists. The essential components of these techniques are the same as those of a drop-down list-box. There is a slider area, a slider thumb and left/right arrow keys. The AlphaSlider functions identically to a drop-down list-box, except for its vertical orientation. This method is very efficient in its screen space use but it allows less use of context in searching. The FineSlider is based upon the AlphaSlider but uses an elastic technique based on a rubber band metaphor. A control object such as a scroll bar is moved by pulling the object with a rubber band between the object and the mouse cursor.

LensBar (Masui, 1998) combines these techniques with interactive filtering and semantic zooming, and also provides explicit control of zooming via horizontal motion of the mouse cursor. A rate-based scrolling interface is described in (Zhai et al., 1997) that maps displacement of the input device to the velocity of scrolling.

Another technique is called Stretch Button Scrollbar (Smith and Henning, 1996). The scroll handle is modified with two extra buttons, one on either side. These buttons allow fine movements similar to that provided by the arrow movement buttons on traditional scroll bars.

5.2.2 Alternative Zooming Techniques

Zoomable user interfaces, such as Pad and Pad++ (Bederson et al., 1994; Perlin and Fox, 1993), use continuous zooming as a central navigation tool. The objects are spatially organised in an infinite two-dimensional information space, and the user accesses a target object using panning and zooming operations. A notable problem with the original zoomable interfaces is that they require explicit

control of both panning and zooming, and it is sometimes difficult for the user to coordinate them. The user can get lost in the infinite information space (Jul and Furnas, 1998). Bimanual approaches also exist, such as that of Guiard et al. (2001) where a joystick in one hand controlled zoom level, and a mouse in the other hand provided navigation. They showed that by using zooming interfaces, bit rates far beyond those possible in physical selection tasks become possible. Van Wijk derived an optimal trajectory for panning and zooming (Wijk and Nuij, 2003), for known start and end points.

5.2.3 Alternative Visualisation Techniques

Information visualisation techniques, such as Fisheye Views (Furnas, 1986; Gutwin, 2002), Perspective Wall (Mackinlay et al., 1991), and the Document Lens (Perlin and Fox, 1993) also address the problem of information overload by distorting the view of documents. The focused area is magnified, while the non-focused areas are squashed but remain in spatial context. The user specifies the next focal point by clicking or panning. These methods can cause several problems for users. One of these is focus-targeting, where a user moves the focus to a new location. Magnification makes focus-targeting difficult because objects appear to move as the focus point approaches them. One solution to this problem is speed-coupled flattening (SCF) (Gutwin, 2002). This technique reduces the distortion level of the focus, based on pointer velocity and acceleration. SCF was proven to significantly reduce both targeting time and targeting errors in fisheye environments. Another technique to solve focus-targeting problem is state-space modeling which will be described in Chapter 6.

5.2.4 Disadvantages of Current Scrolling and Zooming Techniques

Scrolling, panning and zooming techniques have their own limitations. Igarashi and Hinckely (2000) identified the additional overhead involved with the user's attention moving back and forth between the scroll bars and the document. To scroll the user must first acquire the scroll handle, which is sometimes very small (i.e., in long documents) and difficult to target, by moving the mouse

cursor or stylus pointer to the handle and clicking the mouse button or tapping on the screen. Then the user goes back to the updated text in the document. In long documents scroll handle manipulation is more difficult because a small movement can cause a large jump in the information space, which can cause disorientation and confusion (Brewster et al., 1994).

Changing the magnification level affects the user's speed. In zoomed-out document the user moves quickly to avoid frustration but in zoomed-in document s/he moves slowly to avoid disorientation. Furthermore, these non-smooth transitions may cause users to lose context when zooming in and out of a document; because when they are zoomed out to get an overview from the document, there is not enough detail to target and when they are zoomed in to see the detail, the context is lost (Brewster et al., 1994; Cockburn et al., 2005). To improve this problem, multiple windows, each with pan and zoom capability can be provided. But, this method may cause usability problems on small screen devices due to lack of screen space and window overlap. An alternative solution is to have one window containing a small overview, while a second window shows a large more detailed view (Beard and Walker, 1990; Furnas and Bederson, 1995). The small overview contains a rectangle that can be moved and resized, and its contents are shown at a larger scale in the large view. This strategy, however, requires extra space for the overview and the user should mentally integrate the detail and context views. An operational overhead is also required, because the user must regularly move the mouse between the detail and context windows.

The most important problem with panning is that constant mouse movement is required to scroll. One solution is a rate-based scrolling interface (first-order control devices, see Section 3.2.5 on page 38) (Zhai et al., 1993). Rate-based scrolling maps the displacement of the cursor to the scrolling velocity. In a study of different input devices for scrolling and pointing tasks, Zhai et al. (1993) used an isometric joystick which maps the force exerted to velocity in the document. For this study they used the IBM ScrollPoint IITM, which is a mouse with a small joystick in place of the scroll wheel, commonly used for rate-based scrolling. In this study Zhai et al. compared rate-based scrolling with scrollbars. They found

that in rate-based scrolling the users cannot move from one point in the document to another point quickly and their speed is limited to a maximum scrolling speed. If it is set too fast the user will become disorientated by the extreme visual flow, but if it is set too slow the user will become frustrated at the time it takes to scroll to a distant known location (Zhai et al., 1993; Cockburn et al., 2005). Frustration occurs when a user knows the location s/he wants to go to but is forced to wait as the document slowly scrolls there (Zhai et al., 1993).

5.2.5 Role of Input Devices in Scrolling and Zooming Techniques

As mentioned in previous lines the particular input device used can also influence the effectiveness of rate control. An experiment on six degrees of freedom (DOF) input control (Zhai et al., 1997) showed that rate control is more effective with isometric or elastic devices, because of their self-centring nature. It is also reported that an isometric rate-control joystick (Barrett et al., 1995) can surpass a traditional scroll bar and a mouse with a finger wheel (Zhai et al., 1997). Another possibility is to change the rate of scrolling or panning in response to tilt, as demonstrated by Rekimoto (1996) as well as Harrison and Fishkin (1998), suitable for small screen devices like mobiles phones and PDAs.

iPhone (Apple, 2007) allows its users to scroll through songs, artists, albums, and playlists with just a flick of a finger. The scrolling spins gradually to a stop, as though slowed by its own inertia. The effect is both spectacular and practical, because as the scrolling slows, the user can see where s/he is before flicking again.

5.2.6 Speed Dependent Automatic Zooming

Speed-dependent automatic zooming (SDAZ) is a navigation technique first proposed by Igarashi and Hinckely (2000). It couples rate-based scrolling with automatic zooming to overcome the limitations of typical scrolling interfaces and to prevent extreme visual flow. This means that as a user scrolls faster the system automatically zooms out, providing a constant information flow across the screen. This allows users to efficiently scroll a document without having to manually switch between zooming and scrolling or becoming disoriented by fast visual

flow, and results in a smooth curve in the space-scale diagram. In traditional manual zooming interfaces, the user has to interleave zooming and scrolling (or panning); thus the resulting pan-zoom trajectory forms a zigzag line. Cockburn et al. (2003) (Cockburn and Savage, 2003; Cockburn et al., 2005), Savage (2004) and Wallace (2003) (Wallace et al., 2004) presented further developments, with a usability study of performance-improved SDAZ prototypes.

5.2.7 Applications of SDAZ on Small Screen Devices

The need for efficient navigation on small screen displays, such as PDAs and cellphones, have led to a number of studies around the world. Jones et al. (2005) implemented two SDAZ interfaces for small screen displays: a document browser and a map browser. These interfaces were evaluated against interfaces using standard navigation techniques (scroll bars, pan and manual zoom). They found that SDAZ was, on average, 29% slower for browsing text documents on small screen displays. Participants using SDAZ were more accurate and performed significantly fewer actions when completing the tasks. Patel et al. (2004, 2006) also conducted research into the efficiency of SDAZ on small screen displays. The focus of their research was the effective browsing of photograph collections. They evaluated SDAZ against discrete zoom and gesture zoom interfaces. In the discrete zoom interface thumbnails of photographs are presented ordered by creation time. Users can click/tap the desired photo to view an enlarged version, and click/tap again to return to the thumbnail view. In the gesture interface, scroll speed is proportional to vertical mouse displacement (as in rate-based scrolling interfaces) and zooming is proportional to horizontal mouse displacement. A larger horizontal displacement results in a higher zoom level. They found that the SDAZ and gesture zoom interfaces support faster navigation, higher accuracy and have lower subjective task load levels than the standard discrete zoom interface.

5.2.8 Viewing and Navigation

SDAZ provides a smooth navigational path between two views. [Wijk and Nuij \(2003\)](#) introduce the ‘optimal’ animation between two known points of interest based on perceived velocity. They define “optimal” as “smooth and efficient” and use the velocity of the moving image as a basis for measurements, i.e., they aim at a metric for the perceived average optic flow ([Gibson, 1979](#)) in the image window. They use the shortest path in pan-zoom space as the most efficient path when the camera moves from point X to point Y . Without considering the smoothness and the observer’s maximum perceived velocity this path would be a straight line between these two points. The proposed model by Wijk and Nuij only takes into account the perceptual level, not the cognition of the image. For example, they assume that each part of the image is equally interesting (i.e., colour, density, and so forth.) but in real images some parts are more interesting than the other parts.

They suggest that their optimal path could be used to implement a system similar to SDAZ, which uses the scroll handle on scrollbars to determine the target point. Therefore, scrolling to the target location is acquired by the scroll handle and moving to the desired position.

5.3 Tilt-Controlled SDAZ on Small Screen Devices

Implementing the SDAZ technique on a mobile device with inertial sensing allows us to investigate a number of issues: the use of single-handed tilt-controlled navigation, which does not involve obscuring the small display; the usability consequences of tilting the display; the relative strength of stylus-based speed-dependent zooming, compared to mouse and tilt-based control, and combinations of stylus, and tilt-based control. If successful, the user should be able to target a position quickly without becoming annoyed or disoriented by extreme visual flow, and we want the technique to provide smooth transitions between the magnified local view and the global overview, without the user having to manually change the document magnification factor.

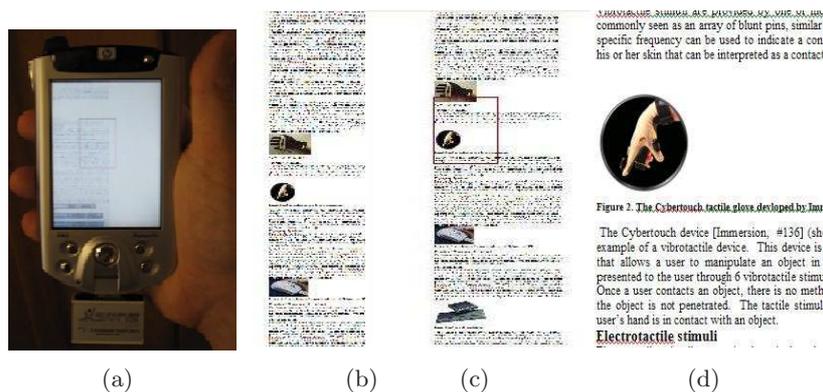


Figure 5.1: A Pocket PC and an accelerometer attached to the serial port. (a) Screen shots of the document browser (b,c and d). (b) shows a red box moving rapidly over the picture, (c) shows the user has found the picture and landing there, and (d) shows the zoomed-in picture.

This method was implemented and executed on an HP 5550 Pocket PC (Figure 5.1).¹ Here, tilting the device moves the zooming-window.² The accelerometer (Xsens P3C, 3 degree-of-freedom linear accelerometer) attached to the serial port of the Pocket PC provides the roll and pitch angles. Before describing the implementation of the system let us have a brief look at the tilt-controlled SDAZ behaviour.

5.3.1 Tilt-Controlled SDAZ Behaviour

All SDAZ methods, discussed in the previous section, are based on static models and in this work we introduce a dynamic model for tilt-controlled SDAZ. But before that, we need to identify the basic components of tilt-controlled SDAZ behaviour, for example, how the user scrolls in the interface, what region the system zooms back, how is the target selection and other low level parameters involved in the development.

¹The author of this dissertation has programmed and coded all the developed applications in Chapter 5 (See Appendix D). This method was implemented using FMOD API (version 3.70CE) (FMOD, 2004), a visual programming environment with object-oriented language (Embedded Visual C++) to manipulate and control sound production and GapiDraw (version 2.04) (GAPI Draw, 2004), a runtime add-in to generate real-time Pocket PC graphics. FMOD API and GapiDraw are available for free under the condition of the GNU General Public License (GPL).

²The term “zooming-window” is used throughout this chapter to indicate a red scrolling rectangular window shown in Figure 5.1. This box is a zoom-in region in the size of the PDA’s screen (240×320 pixels) and the target, which the user wants to land on should be located inside this window. The zooming-window acts as a mouse cursor, which other researchers have used in their SDAZ implementations (Cockburn and Savage, 2003; Savage, 2004).

Low Level Behaviour of Tilt-Controlled SDAZ

Using an accelerometer provides a direct mapping from acceleration in the real world to the acceleration in the interface. Similar to a mouse-controlled SDAZ (Cockburn and Savage, 2003; Savage, 2004) there are three mappings in tilt-controlled SDAZ:

- *Tilt Motion to Zooming-Window Displacement* – A real-time application running on a PDA reads tilt sensor data continuously and maps the physical tilt angles of the device to the corresponding movement of the zooming-window on the screen. Generally, this mapping depends on the speed of tilt sensor data reading from the serial port and it should be left to the Operating System settings.
- *Zooming-Window Displacement to Scroll Speed* – This mapping describes the relationship between tilt angle and the corresponding scroll speed in the document. As described in Section 3.2.8, spring-centred joysticks or force sticks are generally better suited for velocity and higher order control systems and a nonlinear *dead-band* or *dead-zone* in the zero region makes the null position more distinct.
- *Scroll Speed to Magnification Level* – This mapping describes the automatic zooming behaviour: the relationship between the scroll speed and the magnification of the document.

In tilt-controlled SDAZ acceleration data (roll and pitch tilt angles) is translated using the real-time application running on a PDA to vertical and horizontal zooming-window movements, this is mapped to the document scrolling speed and the zoom level is then automatically adjusted to keep visual flow across the screen constant. In this system the scrolling is performed by tilting up/down(pitch) and left/right(roll) the device and moving the zooming-window in the desired direction and returning the device to the equilibrium point.³ Any great lateral

³Equilibrium point is a point from which a controlled variable will not change. Another name for equilibrium point is steady state (Ogata, 1990). An equilibrium point represents a state in which the system can be maintained using the defined action (Ogata, 1995).

acceleration freezes the screen and allows the user to select the desired location on the screen and the system automatically without getting any feedback from the user scrolls the document to that location. In the modeling section (Section 5.3.2) we take into account the second and third mappings in our dynamic model: the relationship between zooming-window displacement and scroll speed, and the relationship between scroll speed and magnification.

Constraints and low level limits of SDAZ, for example, “*maximum ascent rate*”, “*maximum descent rate*”, “*maximum scrolling acceleration*”, and “*maximum fall rate*” have been fully discussed in (Savage, 2004).

Magnification Region

An important issue in ZUIs is the location the system zooms back to, after the user returns the device to the equilibrium point. In (Cockburn and Savage, 2003), Cockburn and Savage used the centre of the screen as the zoom-in location in their SDAZ application when scrolling has finished. They noted that this system is difficult to use for first-time users because users generally concentrate on the cursor and expect the display to zoom to that point and after zooming-in the point disappears from the screen which is confusing for the first-time user. Furthermore, some users felt frustrated with the zoom-to-centre technique because they saw the target area a distance away but had to wait until the area was positioned under the centre of the screen in order to acquire it. Figure 5.2 presents an example of zoom-in to the centre in tilt-controlled SDAZ developed on a PDA.

An alternative solution is zooming to the current zooming-window’s position (Figure 5.3). In an experiment fully demonstrated and analysed in (Savage, 2004) all users stated that they found the zoom-to-cursor (in our application zoom to zooming-window) technique more intuitive. Cockburn and Savage (2003) believe that zooming to the cursor should be used in SDAZ systems for three reasons: First, “*it provides a rapid movement to the position without being overwhelming.*” Second, “*it is the simplest path to implement.*” Finally, “*the method seems natural to use because the system continues scrolling at the same speed and in the same*

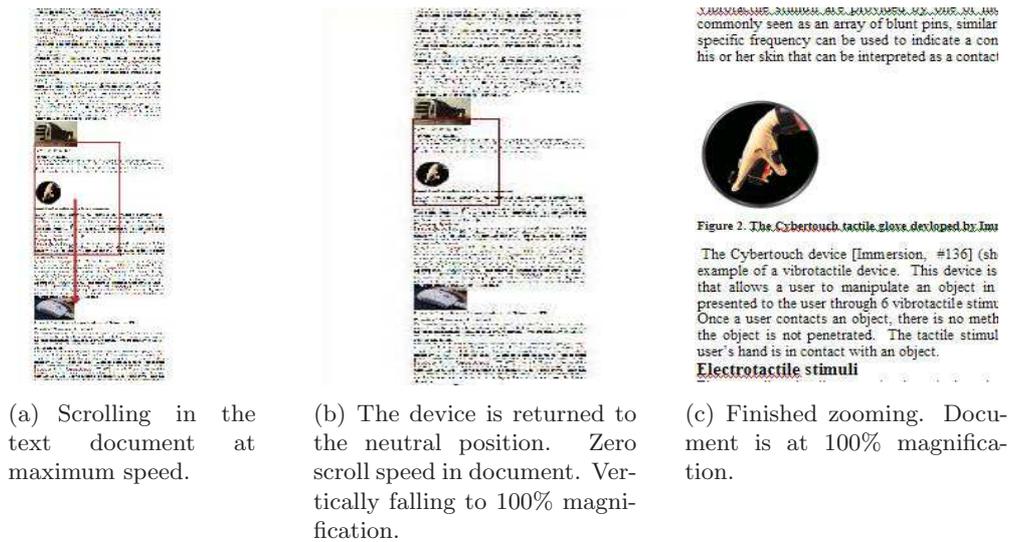
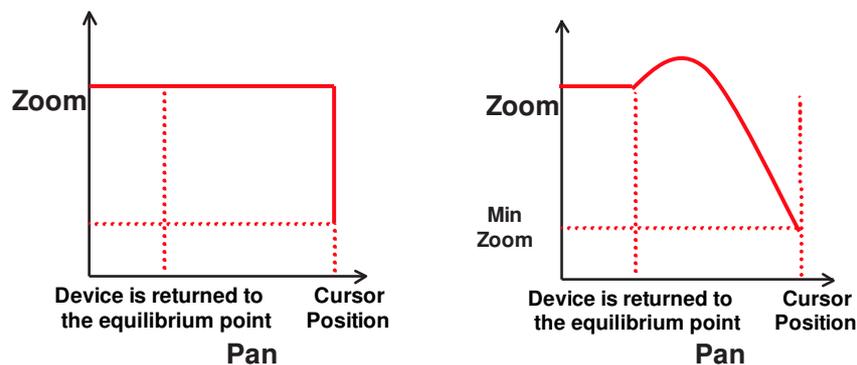


Figure 5.2: Zoom-To-Centre in tilt-controlled SDAZ.



Figure 5.3: Zoom to zooming-window's position in tilt-controlled SDAZ.



(a) Zoom to the zooming-window's position keeping zoom level constant until zooming-window's position is reached. Adapted from Cockburn and Savage (2003).

(b) Zoom to the zooming-window's position using Wijk and Nuij's optimal trajectory. Adapted from Wijk and Nuij (2003).

Figure 5.4: Zoom-Pan space diagrams displaying zoom-in trajectories. The zooming-window's position represents the position the zooming-window was over the document when the device returned to the equilibrium point in tilt-controlled SDAZ.

direction the user was scrolling in before, until it reaches the cursor's point (zoom-in region in our application), then falls to 100% magnification."

For the animation of "zoom to zooming-window position" in tilt-controlled SDAZ we can choose one of these methods:

- keeping the magnification constant, scrolling to the zooming-window's position then falling to full magnification (see Figure 5.4(a)).
- optimal animation path as introduced by Wijk and Nuij (2003) (see Figure 5.4(b)). In this animation, the system zooms out first, then zooms in again to achieve an optimal path.

In the next sections we use zoom to zooming-window position using the method illustrated in Figure 5.4(a) keep magnification constant, scroll to the zooming-window's position then fall to full magnification.

5.3.2 Design

As described in Chapter 3, state-space modeling is a well-established way of presenting differential equations describing a dynamic system as a set of first-order differential equations. State-space modeling allows us to model the internal dynamics of the system like SDAZ, as well as the overall input/output relation-

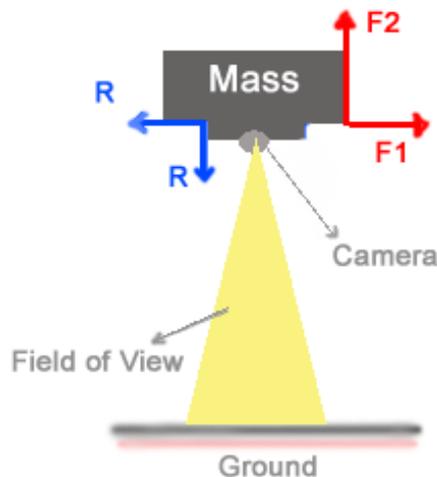


Figure 5.5: Simulating SDAZ as a flying mass. F_1 and F_2 are horizontal and vertical vectors of the external force, F applied to the mass and are coupled together. R is the air Resistance which provides damping effects.

ship as in transfer functions, thus this method is an obvious candidate for the representation of the coupling between the user's speed with zoom level in tilt-based SDAZ. The document viewer to examine the state-space model for the tilt-controlled SDAZ was implemented to browse PDF, PS and DOC files which had been converted to an image (PNG or BMP) file.⁴

The rest of this section will present a state-space model to couple the user's motion with the zoom-level, a method for tuning low level components of SDAZ in the state-space and solutions to some classic problems of SDAZ.

Coupling between velocity and zoom-level

SDAZ can be simulated as a flying object like a bird or an airplane (see Figure 5.5). If the object flies to greater heights it gets a wider view than lower heights (Figure 5.6) and for that it has to fly fast. Thus two variables, velocity

⁴Cockburn and Savage's SDAZ (Cockburn and Savage, 2003) was implemented in *C* and OpenGL exploiting high frame-rates and fluid animation available through hardware acceleration in a desktop PC. Igarashi and Hinckley's system (Igarashi and Hinckley, 2000) was implemented in Java most likely having slower frame-rates. In their document interface, discrete font sizes were used to simulate dynamic font scaling and to improve performance in zoomed-out views, text was depicted as horizontal lines rather than miniaturised fonts. Unfortunately hardware acceleration and high resolution graphics are not available yet on current generation of PDAs. For this reason we had to convert PDF, PS or Microsoft Word Document files to PNG (Portable Network Graphics) or BMP; because these files are more efficient for low graphic resolution systems, and have low rendering time. This increases the speed and smoothness of the browser, the implementation of which was simple but very efficient and smooth (although text tended to flicker during zooming because it was treated as a flat image).

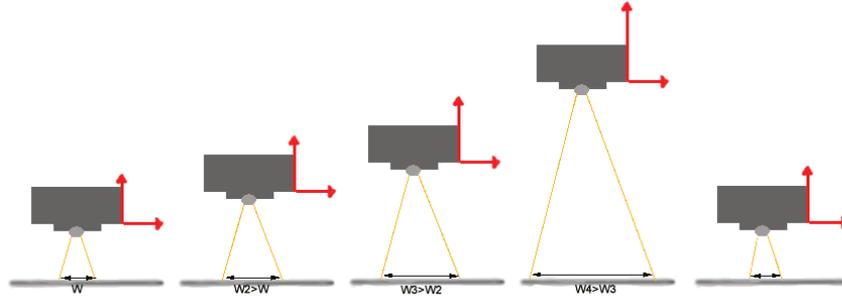


Figure 5.6: View domain of a flying object. If the object flies to greater heights then it gets a global overview of the ground but in lower heights it only gets a local view of the ground.

and field of view, are coupled together.

If we present F_1 and F_2 for horizontal and vertical vectors of the external force applied to the mass, R for air resistance which provides damping effects, m for Mass, v for velocity of the object, a for acceleration, z for zoom and \dot{z} for rate of change of zoom then we can write Newton's second law of motion (refer to Section 3.2.9 on page 46) in the horizontal direction for the object in Figure 5.5:

$$\begin{aligned}
 ma &= F_1 - Rv && \text{or} \\
 a &= \frac{F_1}{m} - R\frac{v}{m} && (5.1)
 \end{aligned}$$

In the vertical direction we can write:

$$\begin{aligned}
 m\dot{z} &= F_2 - Rz && \text{or} \\
 \dot{z} &= \frac{F_2}{m} - R\frac{z}{m} && (5.2)
 \end{aligned}$$

We assume that effects of gravity are negligible. Furthermore we can assume F_2 is a function of F_1 and velocity (this assumption will couple level of zoom to speed of movement as well as tilt input, e.g., in higher speed the field of view, i.e., the area of the triangle increases and vice versa).

$$F_2 = cF_1 - bv \quad (5.3)$$

Where b is a coefficient and c is a scaler. Then we can rewrite equation (5.2) as

below:

$$\dot{z} = c \frac{F_1}{m} - b \frac{v}{m} - R \frac{z}{m} \quad (5.4)$$

Friction in Control

Friction causes delays. Poulton (1974) discusses about the effect of friction in spring-centred control devices, for example, joysticks or tilt sensors. He shows that for tracking in two dimensions, a single spring-centred input device is likely to be an advantage when the task in the two dimensions are similar. Then he argues to prevent accidental operation while the user is tracking in a vehicle, which vibrates we may use different frictions in the vertical and horizontal directions. This idea can be applied to tilt-controlled SDAZ and we can consider two different frictions in different directions; R for horizontal direction and R' for vertical direction. Then the equation (5.4) can be rewritten as below:

$$\dot{z} = c \frac{F_1}{m} - b \frac{v}{m} - R' \frac{z}{m} \quad (5.5)$$

The inputs to the system can be the tilting angles measured using an accelerometer attached to the serial port of PDA, or the stylus position on the PDA's touch screen. The state variables chosen are $x_1(t)$ for position of zooming-window, $x_2(t)$ for speed of scroll and $x_3(t)$ for zoom. u represents input, F_1 (pitch tilting angle), and the state equations are:

$$x_2(t) = v = \dot{x}_1 \quad (5.6)$$

$$x_3(t) = z = f(x_1, x_2, u) \quad (5.7)$$

Thus the zoom-level is a function of position, velocity and pitch tilting angle, u .

An initial suggestion is to reproduce the standard second-order dynamics of a mass-spring-damper system and give the scrolling movement and zoom level some inertia to provide a physically intuitive interface. The first time-derivative of the state equations given in equations (5.1) to (5.4) can be rewritten as below,

as a linearisation of the system at a given velocity and zoom:

$$\dot{x}_1(t) = v = x_2(t) \quad (5.8)$$

$$\dot{x}_2(t) = a = \dot{v} = \frac{-R}{m}x_2(t) + \frac{1}{m}u(t) \quad (5.9)$$

$$\dot{x}_3(t) = \dot{z}(t) = \frac{-b}{m}x_2(t) - \frac{R'}{m}x_3(t) + \frac{c}{m}u(t) \quad (5.10)$$

The standard matrix format of these equations is (refer Section 3.2.9):

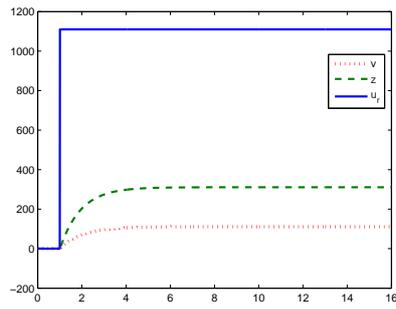
$$\begin{pmatrix} \dot{x}_1 \\ \dot{x}_2 \\ \dot{x}_3 \end{pmatrix} = \begin{pmatrix} 0 & 1 & 0 \\ 0 & \frac{-R}{m} & 0 \\ 0 & \frac{-b}{m} & \frac{-R'}{m} \end{pmatrix} \begin{pmatrix} x_1 \\ x_2 \\ x_3 \end{pmatrix} + \begin{pmatrix} 0 \\ \frac{1}{m} \\ \frac{c}{m} \end{pmatrix} u \quad (5.11)$$

This shows how a single-degree of freedom input can control both velocity and zoom-level. The non-zero off-diagonal elements of the A matrix indicate coupling among states, and the B matrix indicates how the inputs affect each state. This example could be represented as having zoom as an output equation, rather than state, and the coupling between zoom and speed comes only primarily the B matrix, which is not particularly satisfying.

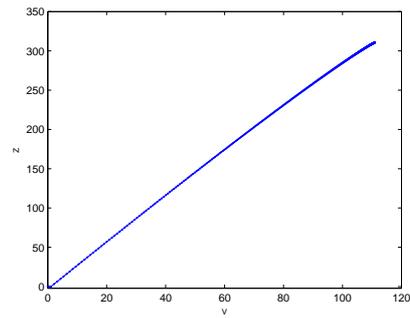
The next step is finding suitable values for R , R' , m , b and c coefficients in the state-space model to make the system controllable (refer to Section 3.2.9 on page 45). We can write the controllability matrix as below:

$$\text{rank}[B|AB|A^2B] = \text{rank} \begin{pmatrix} 0 & \frac{1}{m} & \frac{-R}{m^2} \\ \frac{1}{m} & \frac{-R}{m^2} & \frac{R^2}{m^3} \\ \frac{c}{m} & \frac{-b-R'c}{m^2} & \frac{bR+bR'+cR'^2}{m^3} \end{pmatrix} \quad (5.12)$$

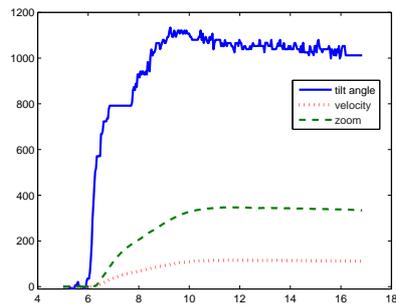
which has a full rank for all R , R' , $m \neq 0$, $b \neq 0$ and c . This suggests a wide range of possible coefficient settings for the model. One way to choose the right settings is observing the simulated system's behaviour.



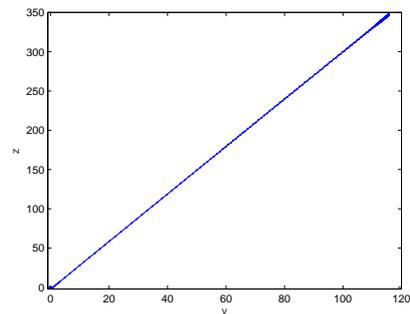
(a) Plots of step input, velocity and zoom of the simulated SDAZ model in MATLAB



(b) Zoom vs. velocity in the simulated SDAZ model in MATLAB



(c) Plots of step input, velocity and zoom of the implemented SDAZ model on a PDA



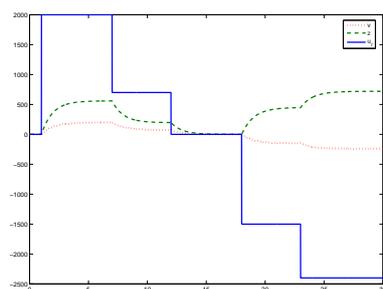
(d) Zoom vs. Velocity in the implemented SDAZ model on a PDA

Figure 5.7: Behaviour of SDAZ model to a step input in simulated model in MATLAB and implemented model on a PDA ($m = 10 \text{ kg}$, $R = 10 \text{ kgs}^{-1}$, $R' = 10 \text{ kgs}^{-1}$, $b = 3 \text{ kgs}^{-1}$ and $c = 3$).

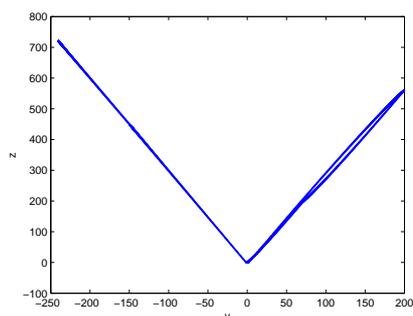
5.3.3 Simulation

A well-designed model should generate similar behaviour on the actual system/device as the simulated system. For this purpose we set the coefficients $m = 10 \text{ kg}$, $R = 10 \text{ kgs}^{-1}$, $R' = 10 \text{ kgs}^{-1}$, $b = 3 \text{ kgs}^{-1}$ and $c = 3$ to check the system behaviour to different input signals in real and simulated environment. Figure 5.7 presents the time domain response of the simulated system in MATLAB and implemented system on a PDA⁵ to a step input, which means scrolling down on a document and staying in a certain speed by tilting the device. In the off-line simulation the input signal is without noise; however in the real experiment, the tilt sensor data is noisy. Figure 5.8(c) shows the sensitivity of the dynamic model in the real experiment to noise. A few milliseconds after tilting the device both velocity and zoom have reached to a steady-state and this is

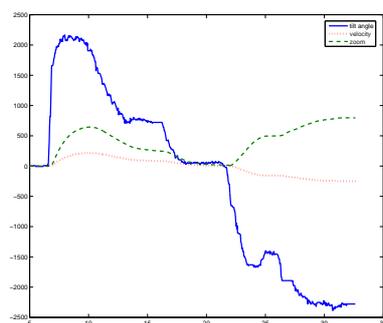
⁵To solve the first-order differential equations in the developed application, Taylor's method was implemented in EVC++ with sampling time 30 ms (Polyanin and Zaitsev, 2003).



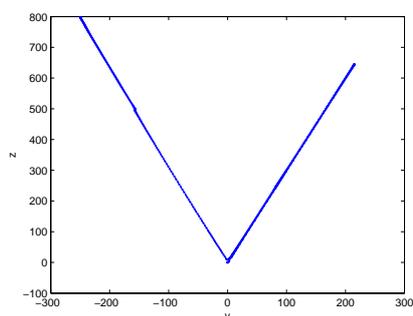
(a) Plots of step input, velocity and zoom of the simulated SDAZ model in MATLAB



(b) Zoom vs. velocity in the simulated SDAZ model in MATLAB



(c) Plots of step input, velocity and zoom of the implemented SDAZ model on a PDA



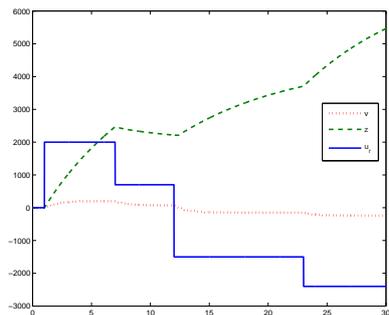
(d) Zoom vs. Velocity in the implemented SDAZ model on a PDA

Figure 5.8: Behaviour of SDAZ model to a step input in simulated model in MATLAB and implemented model on a PDA ($m = 10 \text{ kg}$, $R = 10 \text{ kgs}^{-1}$, $R' = 10 \text{ kgs}^{-1}$, $b = 3 \text{ kgs}^{-1}$ and $c = 3$).

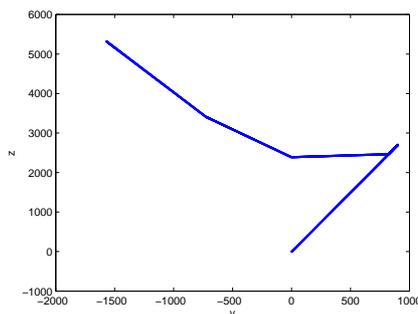
one of main advantages of feedback dynamic systems (refer to Section 3.2.2 on page 34). The relationship between the velocity and zoom in both simulated and actual system are linear indicating the system's behaviour is linear and slope of the line is almost 3.

Figure 5.8 presents the time domain response of the simulated system in MATLAB and implemented system on a PDA to a varying step inputs, which means scrolling down on a document, staying in a certain speed, landing on a figure and scrolling up by tilting the device. Despite changes in the sign of input data the relationship between velocity and zoom remains linear.

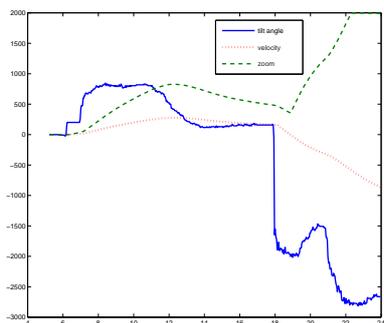
Figure 5.9 presents the time domain response of the simulated system in MATLAB and implemented system on a PDA to a varying step inputs with different settings as mentioned above, $m = 10 \text{ kg}$, $R = 10 \text{ kgs}^{-1}$, $R' = 1 \text{ kgs}^{-1}$, $b = 3 \text{ kgs}^{-1}$ and $c = 3$ (We have only reduced friction in the vertical direction).



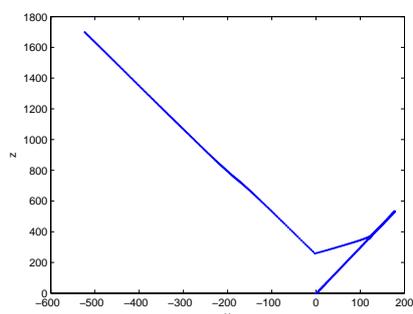
(a) Plots of step input, velocity and zoom of the simulated SDAZ model in MATLAB



(b) Zoom vs. velocity in the simulated SDAZ model in MATLAB



(c) Plots of step input, velocity and zoom of the implemented SDAZ model on a PDA



(d) Zoom vs. Velocity in the implemented SDAZ model on a PDA

Figure 5.9: An example of bad coefficients settings for tilt-controlled SDAZ ($m = 10$ kg, $R = 10$ kgs⁻¹, $R' = 1$ kgs⁻¹, $b = 3$ kgs⁻¹ and $c = 3$). The friction coefficient, R' , has been reduced from 10 to 1 (compare it with Figure 5.8). The system is controllable but level of zoom is not easy to control and small changes in the tilt angle has made the system to zoom out quickly.

The system is controllable but level of zoom is not easy to control (controllability matrix has a full rank, see equation 5.12 but for human is not easy to achieve a good control behaviour) and small changes in tilt has made the system to zoom out quickly, which means that sensitivity to noise in the friction causes less delay and lets the mass zoom out too quickly (see results in Figure 5.8 to compare).

The linear dynamic model presented here can be extended to a general non-linear format (see equation (3.1) on page 43).

Nonlinear State-Space Model

In SDAZ (Igarashi and Hinckely, 2000; Wallace et al., 2004; Wijk and Nuij, 2003), the document velocity as a function of control input (mouse displacement,

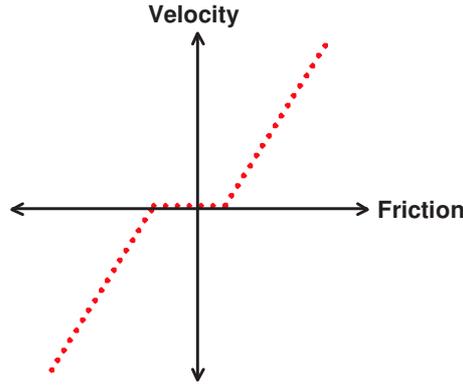


Figure 5.10: An example of non-linear relationship between velocity and friction.

tilt angle, or stylus displacement, depending on platform) tend to be static, linear, or piecewise linear functions (Igarashi and Hinckely, 2000; Wallace et al., 2004). The general state-space equations in (5.7) can be written in a nonlinear form where functions mapping zoom to velocity or vice versa, and functions mapping friction to zoom and velocity can be nonlinear dynamic functions:

$$\dot{x}(t) = v \quad (5.13)$$

$$\dot{v}(t) = a = \frac{-r(v, z)}{m}v(t) + f_{vz}(z) + \frac{1}{m}u(t) \quad (5.14)$$

$$\dot{z}(t) = \frac{-r'(v, z)}{m}z(t) + f_{zv}(v, \dot{v}) + \frac{c}{m}u(t) \quad (5.15)$$

Where $f_{vz}(z)$ and $f_{zv}(v, \dot{v})$ are nonlinear functions which couple speed of scroll to level of zoom. Frictions, $r(v, z)$ and $r'(v, z)$, can also be nonlinear functions of velocity (see Figure 5.10). Using these more interesting behaviour can be obtained, such as those elegantly derived by Wijk and Nuij (2003). Linearising these equations around the equilibrium point can generate equations in (5.9) and (5.10) (Brogan, 1991; Ogata, 1990).

The dynamic model for SDAZ presented in this section provides a few control modes and system behaviours which can facilitate the tilt controlled interaction on portable computing devices.

5.4 Model-Based Interactive Behaviour in SDAZ

The requirements of any good control system are speed, accuracy, and stability. The intelligence is merely the ability of the control system to operate successfully in a wide variety of situations by detecting the specific situation that exists at any instant and servicing it appropriately (Anderson et al., 2001; Morse, 1996; Narendara and Balakrishnan, 1997). External disturbances, changes in subsystem dynamics, parameter variations, and so forth, are examples of different unknown contexts in which the system has to operate (Narendara and Balakrishnan, 1994; Narendara et al., 1995).

Two kinds of switching schemes have been proposed in the literature. In direct switching (Fu and Barmish, 1986; Mårtensson, 1986; Miller and Davison, 1986; Miller, 1994; Middleton et al., 1988; Poolla and Cusumano, 1988), the choice of when to switch to the next controller, in a predetermined sequence, is based directly on the current output of the plant and input to the system. In indirect switching methods multiple models are used to determine both when and to which controller one should switch. This approach was first proposed by Middleton et al. (1988) and later adapted in (Morse, 1996). In the later case, assuming that the models and contexts are parameterised suitably, the model with the smallest error, according to some criterion, is selected rapidly (switching) and then its parameters are adjusted over a slower time scale to improve accuracy (tuning). In switching, the problem is to determine when to switch and what to switch to. In tuning, the problem is to determine the rule by which the parameter value is to be adjusted at each instant (Narendara and Balakrishnan, 1997).

In our application we work with a single controller and here, we introduce a direct switching method and transitions among different control modes which alter the dynamics and the way the user's inputs are interpreted as discussed in earlier chapters (refer to Section 3.2.9 on page 45).

5.4.1 Control Modes in SDAZ

In interaction between user and model-based text browser the user provides raw tilt input data as action via accelerometer and the user's action controls what s/he perceives from the display. The state-space, dynamic system representation couples the user's intention to SDAZ via only one degree of freedom tilt input. In this task the user is either looking for specific piece of information (searching) or targeting something on the display. We define a few different modes of control in this example: no action, free motion, velocity and diving control. Each of these control modes needs special parameter settings in the state-space.

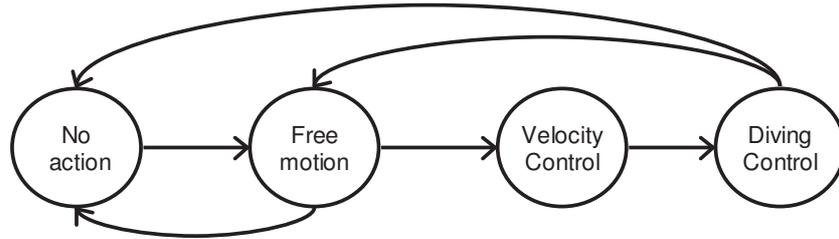
In Figure 5.11(a) we see how the transition between these modes happens. In the beginning the user is in the no-action state because there is no input from the user to the system. By tilting the device, therefore increasing the speed, the user goes to the free motion control mode.

$$\begin{pmatrix} \dot{x}_1 \\ \dot{x}_2 \\ \dot{x}_3 \end{pmatrix} = \begin{pmatrix} 0 & 1 & 0 \\ 0 & \frac{-R}{m} & 0 \\ 0 & \frac{-b}{m} & \frac{-R'}{m} \end{pmatrix} \begin{pmatrix} x_1 \\ x_2 \\ x_3 \end{pmatrix} + \begin{pmatrix} 0 \\ \frac{1}{m} \\ \frac{c}{m} \end{pmatrix} u \quad (5.16)$$

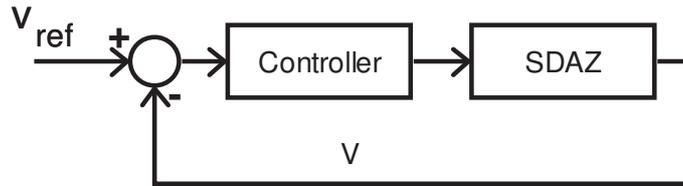
and x_1 , x_2 , x_3 , or $(\dot{x}, \dot{v}, \dot{z})$ are functions of current position, velocity, level of zoom and input or $f(v, z, u)$.

Free motion control is a transient state and the user may go back to no-action or velocity control mode afterward. In the velocity control mode the user is usually looking for some piece of information and s/he may spend a long time browsing at a steady speed in the document searching for a certain data (Figures 5.11(b) and 5.15). In the velocity control mode, the user controls v_{ref} as a desired velocity manually and the controller maintains this velocity automatically and complete the scrolling task with the desired speed for the user.

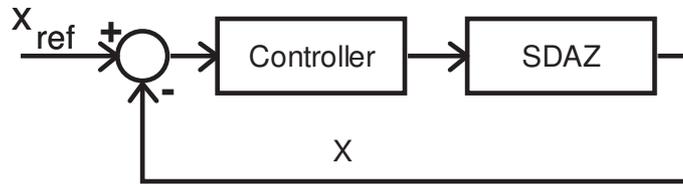
This mode needs state feedback to augment control behaviour, hence the state should move towards the reference value, v_{ref} . From section 3.2.9 (on



(a) Four states of control mode in tilt-controlled SDAZ and transitions among them



(b) Velocity control mode



(c) Diving control mode

Figure 5.11: Control modes and their controllers in tilt-controlled SDAZ.

page 45) we can create a control law such $u = L(r - x)$ (see Figures 5.13 and 5.14).

$$\begin{aligned} \dot{x} &= Ax + Bu = Ax - BLx + BLr \\ &= (A - BL)x + BLr \end{aligned} \quad (5.17)$$

In proportional control, $L(r - x)$ is called control input. In this control law if we introduce $L = [0 \ l \ 0]$ and $r = [0 \ v_{ref} \ 0]^T$ (“T” indicates the matrix transpose) and replace these L and r in equation (5.16) then new state equations will be:

$$\begin{pmatrix} \dot{x}_1 \\ \dot{x}_2 \\ \dot{x}_3 \end{pmatrix} = \begin{pmatrix} 0 & 0 & 0 \\ 0 & \frac{-R}{m} - l\frac{1}{m} & 0 \\ 0 & \frac{-b}{m} - l\frac{c}{m} & \frac{-R'}{m} \end{pmatrix} \begin{pmatrix} x_1 \\ x_2 \\ x_3 \end{pmatrix} + \begin{pmatrix} 0 \\ l\frac{1}{m} \\ l\frac{c}{m} \end{pmatrix} v_{ref} \quad (5.18)$$

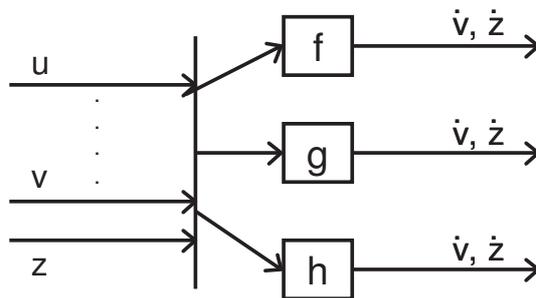


Figure 5.12: Classification in changes in velocity and level of zoom.

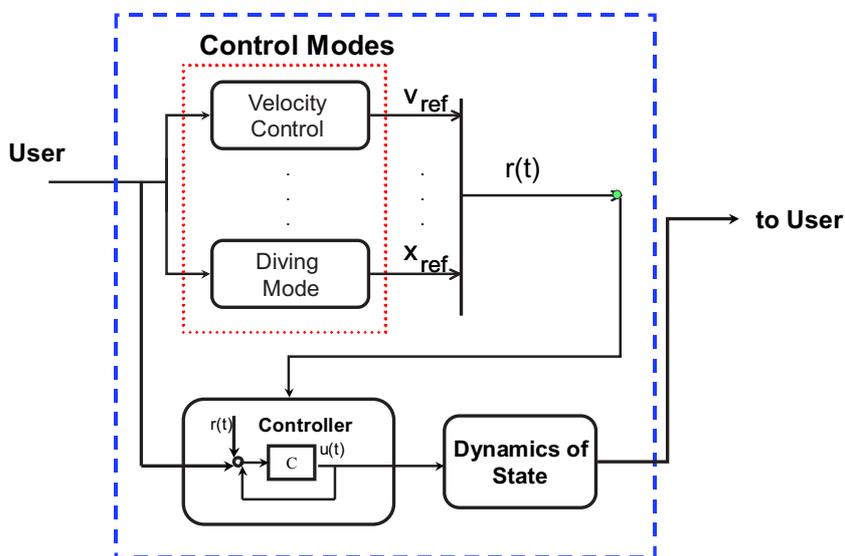


Figure 5.13: Mode switching and reference signals. The user controls v_{ref} or x_{ref} as a desired velocity or position manually and the controller maintains this velocity or position automatically and complete the task for the user.

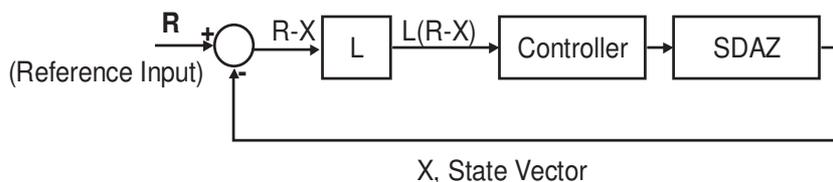


Figure 5.14: An example of proportional control, where the controller uses state feedback to augment control behaviour, by making the state move towards some reference value r , and creating a new control law such $u = L(r - x)$.

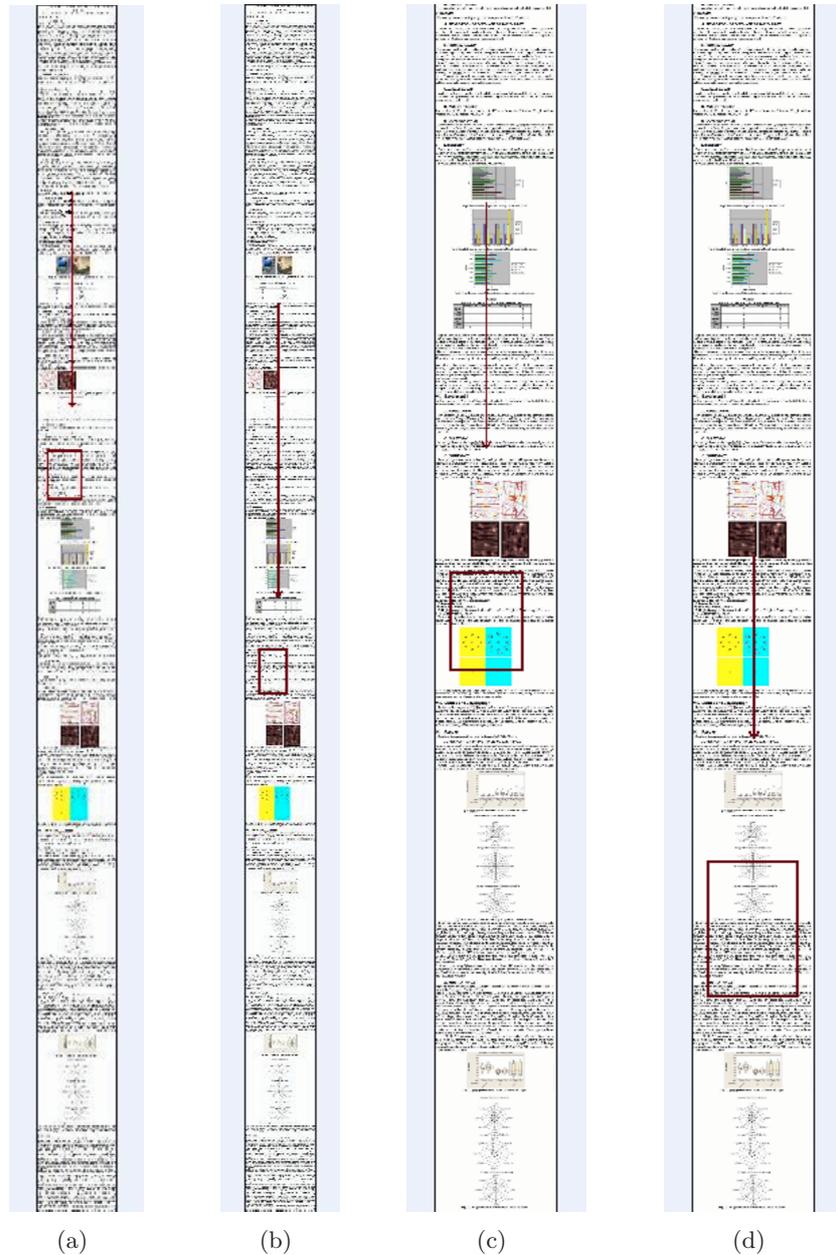


Figure 5.15: An example of velocity control mode. (a) The user has started velocity control mode by tilting the device. The red vertical vector represents the reference velocity (v_{ref}) and length of this vector represents speed of scroll (the higher the speed, the longer the vector appears on the screen.). (b) The user tilts the device faster and increases v_{ref} and moves to a higher height (note length of the vector). Then the controller maintains the desired velocity automatically and complete the scrolling task with that velocity for the user. (c) Where the user is interested in some details in the text he tilts the device slowly and reduces the (v_{ref}), then the controller maintains a new reference value for the velocity automatically. (d) If the user is happy about the speed of scroll he may tilt the device at a constant angle and the controller keeps speed of scroll at the current reference value.

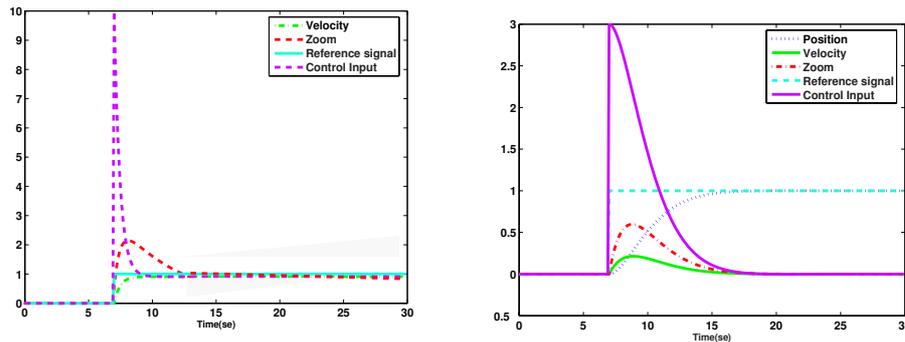
After changing the control law, the system should be both stable and controllable. For stability, $A - BL$ should be full rank and for controllability, the controllability matrix $[BL - (A - BL)BL - (A - BL)^2BL]$ should be full rank, too. Many researches in the past decades in analysis of proportional control of second order systems have been done with special focus on finding optimal value for L , which is beyond the scope of this thesis (for more reading refer to (Cadwallender and Cochin, 1997; Coelingh, 2000)). In this example application with given $m = 10$ kg, $R = 10 \text{ kgs}^{-1}$, $R' = 10 \text{ kgs}^{-1}$, $b = 3 \text{ kgs}^{-1}$ and $c = 3$, we choose $L = 10$, which satisfy stability and controllability conditions discussed earlier. For examples of following a reference signal see figure 5.17 and for the algorithm and simulation code used in MATLAB see Appendix B.

The reference velocity can be either a linear or a nonlinear function of input $v_{ref} = s(u)$ and changes in zoom level will be a function of velocity and v_{ref} , $\dot{z} = h(v, v_{ref})$ (see equations (5.13) to (5.15)).

as those elegantly After finding the target (i.e., the zooming-window is over the target point) the user may slow down or stop tilting thus the system scrolls to the zooming-window with a constant magnification level. When the zooming window is reached, the position of the target the user is interested to land on becomes the reference signal, x_{ref} , and the controller changes the current position value to the reference position, x_{ref} (i.e., moves the state position variable toward the reference value, x_{ref}), and smoothly dives toward it vertically (Figures 5.11(c), 5.14 and 5.16). Similar to the velocity control mode, we create a control law $u = L(r - x)$ and change the standard equation (5.11) to equation (5.19) by introducing $L = [l \ 0 \ 0]$ and $r = [x_{ref} \ 0 \ 0]^T$ then new state-space matrix will be:

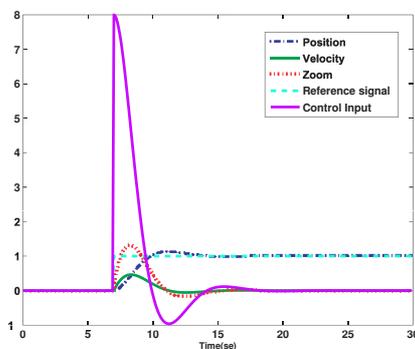
$$\begin{pmatrix} \dot{x}_1 \\ \dot{x}_2 \\ \dot{x}_3 \end{pmatrix} = \begin{pmatrix} 0 & 1 & 0 \\ -l\frac{1}{m} & \frac{-R}{m} & 0 \\ -l\frac{c}{m} & \frac{-b}{m} & \frac{-R'}{m} \end{pmatrix} \begin{pmatrix} x_1 \\ x_2 \\ x_3 \end{pmatrix} + \begin{pmatrix} 0 \\ l\frac{1}{m} \\ l\frac{c}{m} \end{pmatrix} x_{ref} \quad (5.19)$$

The reference signal here indicates the target the user wants to dive to. In this example application with given $m = 10$ kg, $R = 10 \text{ kgs}^{-1}$, $R' = 10 \text{ kgs}^{-1}$, $b =$

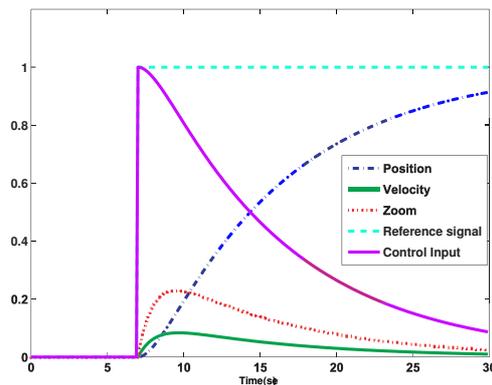


(a) An example of following a reference velocity with settings $m = 10 \text{ kg}$, $R = 10 \text{ kgs}^{-1}$, $R' = 10 \text{ kgs}^{-1}$, $b = 3 \text{ kgs}^{-1}$, $c = 3$, and $L = 10$. After reaching to the desired velocity, v_{ref} , zoom also remains in the desired level. For making more space in the figure position state has not been plotted.

(b) An example of following a desired position and landing there with settings $m = 10 \text{ kg}$, $R = 10 \text{ kgs}^{-1}$, $R' = 10 \text{ kgs}^{-1}$, $b = 3 \text{ kgs}^{-1}$, $c = 3$, and $L = 3$. After reaching to the desired position, both zoom and velocity converge to zero.



(c) An example of following a desired position and landing there with settings $m = 10 \text{ kg}$, $R = 10 \text{ kgs}^{-1}$, $R' = 10 \text{ kgs}^{-1}$, $b = 3 \text{ kgs}^{-1}$, $c = 3$, and $L = 8$. Bad value in L has caused oscillatory behaviour in the system and system after few oscillation has followed the reference signal.



(d) An example of following a desired position and landing there with settings $m = 10 \text{ kg}$, $R = 10 \text{ kgs}^{-1}$, $R' = 10 \text{ kgs}^{-1}$, $b = 3 \text{ kgs}^{-1}$, $c = 3$, and $L = 1$. Bad value in L has caused over-damping behaviour in the system and system in the given time has not reached the desired position.

Figure 5.17: Examples of simulated system behaviour to different reference signals with different coefficients settings.

3 kgs^{-1} and $c = 3$, we choose $L = 3$, which satisfy stability and controllability conditions. For examples of following a reference position see figure 5.17 and different behaviour of the system when L changes.

In the diving control mode, changes in velocity and level of zoom can be a linear or nonlinear function of input, current position, velocity and zoom or in general, $g(u, x, v, z)$. While diving, any tilt angle changes the position of the blue cross and let the user to refine his/her targeting. After diving the user may go back to no-action mode or by any acceleration above a threshold, on route toward a goal, may switch to free motion mode and start browsing again (Figure 5.11(a)).

Figure 5.12 presents a classifier that decides which control mode the system should switch to. According to current values of input, velocity, position and level of zoom (u, x, v and z), functions f, g , and h are calculated but history of tilt input and control states decide which control mode should be active at each time. After selecting the most suitable control mode, coefficients in the state-space model are set to new values.

In the next section, tuning parameters and calibration will be discussed.

5.4.2 Calibration, Performance Measures and State-Space Approach

SDAZ has many parameters that can be tuned, usually treated as a series of interacting, but essentially separate equations. The state-space formulation allows multiple variables, and derivative effects (e.g., position, velocity, acceleration) can be coupled with zoom level, without any further coding, by just changing the entries of the A and B matrices, simulating combinations of springs, masses and damping effects (refer to Section 3.2.9 on page 46).

To enhance the smoothness of the transition between the global overview and the magnified local view after a mouse button is pressed, Cockburn and Savage (2003) use a ‘falling’ speed, and Igarashi and Hinckely (2000) place a limit on the maximum time-derivative of zoom, with similar effect. The falling rate was calculated using trial and error – if the rate was too fast, the user felt

motion sickness and lost their place in the document, whereas it being too small led to a sluggish interface. This can be represented as a straightforward switch to a particular parameterisations of the A matrix, which can be tuned to give an appropriate exponential decay in velocity or zoom. Related problems include rapid zooming in and out when making a rapid change of direction (Igarashi and Hinckely, 2000).

In the state-space representation, our basic assumption is that zoom should lead speed when speed increases, in order to avoid extreme visual flow. Zoom should, however, lag speed when $|v|$ decreases, to allow the user to slow down but still maintain the overview. This also allows, for example, the user to zoom out, without changing position in the document, by repeated positive and negative acceleration.

As mentioned in Section 5.3.1 (on page 107) the zooming-window displacement mapping to speed of scroll is one of low level behaviour of SDAZ. Having an initial dead-zone helps to filter out small tilt angles or small zooming-window displacements, which cause zero or slow responses at small input level and fast responses at large input level (see Figure 3.8). In order to move more rapidly through the document at high levels of zoom, here, we adapted B by making c in equation (5.11) a function of velocity. When speed is above the dead-zone threshold (here set to 0.1), $c = 3$ but below this threshold $c = 0$, where speed of scroll and level of zoom do not change. We wish to avoid rapid drop effects when the user changes direction. To achieve this, we change c to be $-0.5 \times c$, when the sign of velocity and input differ.

Gutwin (2002), Igarashi and Hinckely (2000) and Wallace (2003) report the “hunting effect” problem when users overshoot the target due to the system zooming in as the user slows, the user then rapidly adjusts behaviour to compensate, which causes the system to zoom out again. One approach to this would be to switch to a ‘diving’ control mode if $dz/dt \geq z_{\text{thresh}}$, where $c = 0$, preventing zooming increases, unless a major change in velocity, occurs, which would switch the control mode back to velocity control. Figure 5.18 presents effectiveness of this mode of control in a simulated system in MATLAB. We also developed two

versions of the document browser application on a PDA, one without diving mode and the other one with diving mode. See Appendix D for online C++ source code.

From Section 3.2.10 on page 48, one method that can be used to choose the proper coefficient settings in the state-space model is measuring the user's activity via a cost function. Thus, the function to be minimised in this targeting task would be:

$$uf = filter(u)$$

$$J_t = \|t_f - t_0\| \quad (5.20)$$

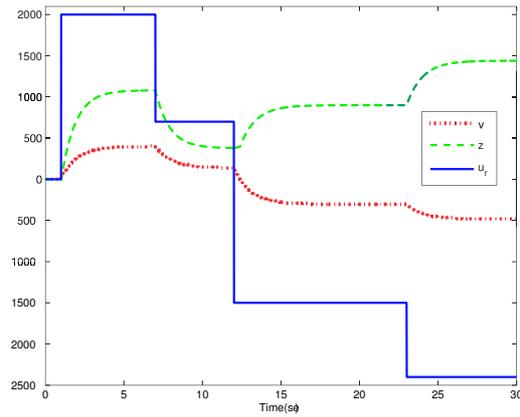
$$J_s = \sum_{t=t_0}^{t_f} \|uf_{t+1} - uf_t\| \quad (5.21)$$

$$J_a = \frac{\sum_{t=t_0}^{t_f} \|uf_{t+1} - uf_t\|}{t_f - t_0} \quad (5.22)$$

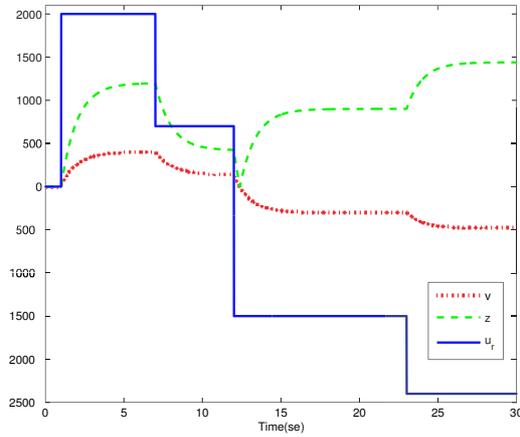
t_0 and t_f are initial and final time and uf_t is the user's tilt input to the system, which has been filtered. Equation (5.20) presents the total time of the completing the task as a performance measure. Thus, when the use is comfortable with the system while interacting s/he should complete the task in the minimum time. Similarly, in equations (5.21) and (5.22) the total sum of changes or mean sum of changes in the tilt input should be minimised if the interaction is smooth.

We used a low-pass filter to smoothen the data⁶ to filter frequencies below 40 Hz in tilt input data. Figures 5.19 and 5.20 show the effect of the diving mode in browsing signals and the cost function. Adding the diving mode reduced the cost function, which also explains the users' low activity in the application having this mode. We include saturation terms for maximum and minimum zoom levels, and there can be specific rules for behaviour at the limits associated with the start and end of the document. For example, if the user is already at the beginning of the document and s/he tilts the device up to scroll up will not be

⁶The "fircls1" command in MATLAB, is used specifically to design low-pass and high-pass linear phase FIR filters using constrained least squares. We used this function as a low-pass filter with cut-off frequency $\omega_c=0.8$ (i.e., 40 Hz) and "filtfilt" function to filter tilt input data (MathWorks, 2005).



(a) An example of ‘hunting effect’ in a simulated system in MATLAB. Hunting happens around time 12 (s) when the ‘diving’ control is not considered.

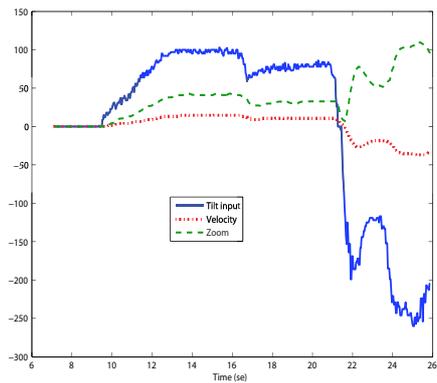


(b) ‘Hunting effect’ disappears in the simulated system in MATLAB after adding ‘diving’ mode.

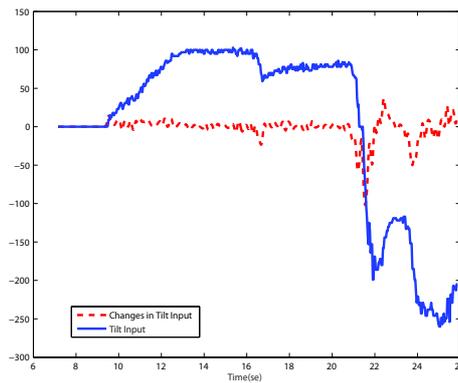
Figure 5.18: Simulated system’s behaviour with settings $m = 10$ kg, $R = 10$ kgs^{-1} , $R' = 10$ kgs^{-1} , $b = 3$ kgs^{-1} and $c = 3$.

taken into account by the controller. Furthermore, in the diving control mode the user cannot dive toward a target beyond the document. Zoom has a maximum level, too which means the user cannot be zoomed out till infinite level.

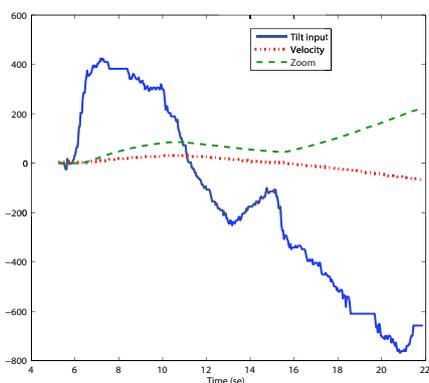
In this section the dynamic tilt-controlled SDAZ behaviour, the performance functions and the system calibration were explored. An important issue in dynamic continuous interactive systems is the system should adapt to user behaviour and complete the task for the user. Achieving this goal requires the system to reinterpret the user’s input as reference signals.



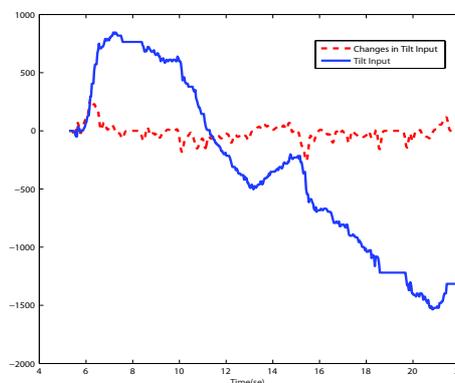
(a) An example of ‘hunting effect’ in a real system developed on a PDA. Hunting effect happens around time 22 (s) when the ‘diving’ control is not considered.



(b) User’s tilt input and changes in the input when the diving mode is disabled. Total sum of changes in input is 615 unit.



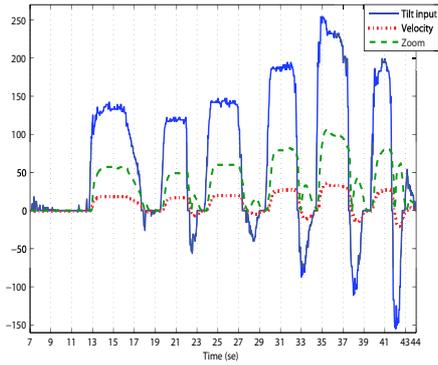
(c) ‘Hunting effect’ disappears in a real system developed on the PDA after adding ‘diving’ mode.



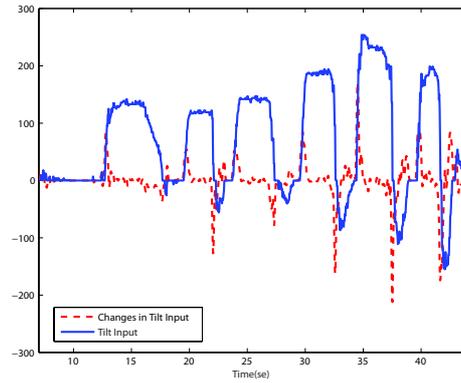
(d) User’s tilt input and changes in the input when the diving mode is active. Total sum of changes in input is 361 unit.

Figure 5.19: Real developed system’s behaviour with settings $m = 10$ kg, $R = 10$ kgs^{-1} , $R' = 10$ kgs^{-1} , $b = 3$ kgs^{-1} and $c = 3$. The user was asked to find and land on the 4th header in the document.

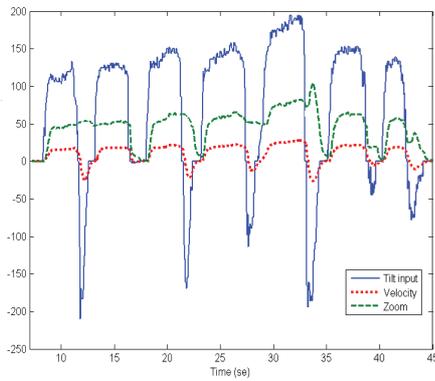
5.4.3 Reference Signals as Inputs



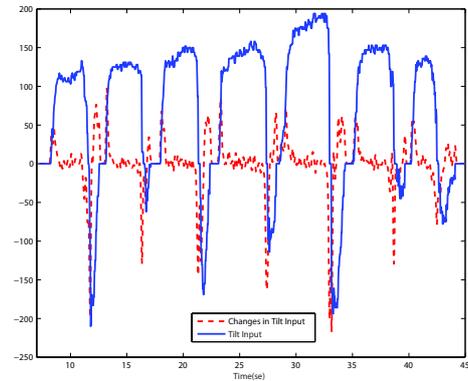
(a) An example of 'hunting effect' in a real system developed on a PDA. This effect happens around time 31 (s) and 42 (s) when the 'diving' control is not considered.



(b) User's tilt input and changes in the input when the diving mode is active. Total sum of changes in input is 18324 unit.



(c) 'Hunting effect' disappears in a real system developed on the PDA after adding 'diving' mode.



(d) User's tilt input and changes in the input when the diving mode is active. Total sum of changes in input is 14809 unit.

Figure 5.20: Real developed system's behaviour with settings $m = 10$ kg, $R = 10$ kgs^{-1} , $R' = 10$ kgs^{-1} , $b = 3$ kgs^{-1} and $c = 3$. The user was asked to find and land on different headers in the document.

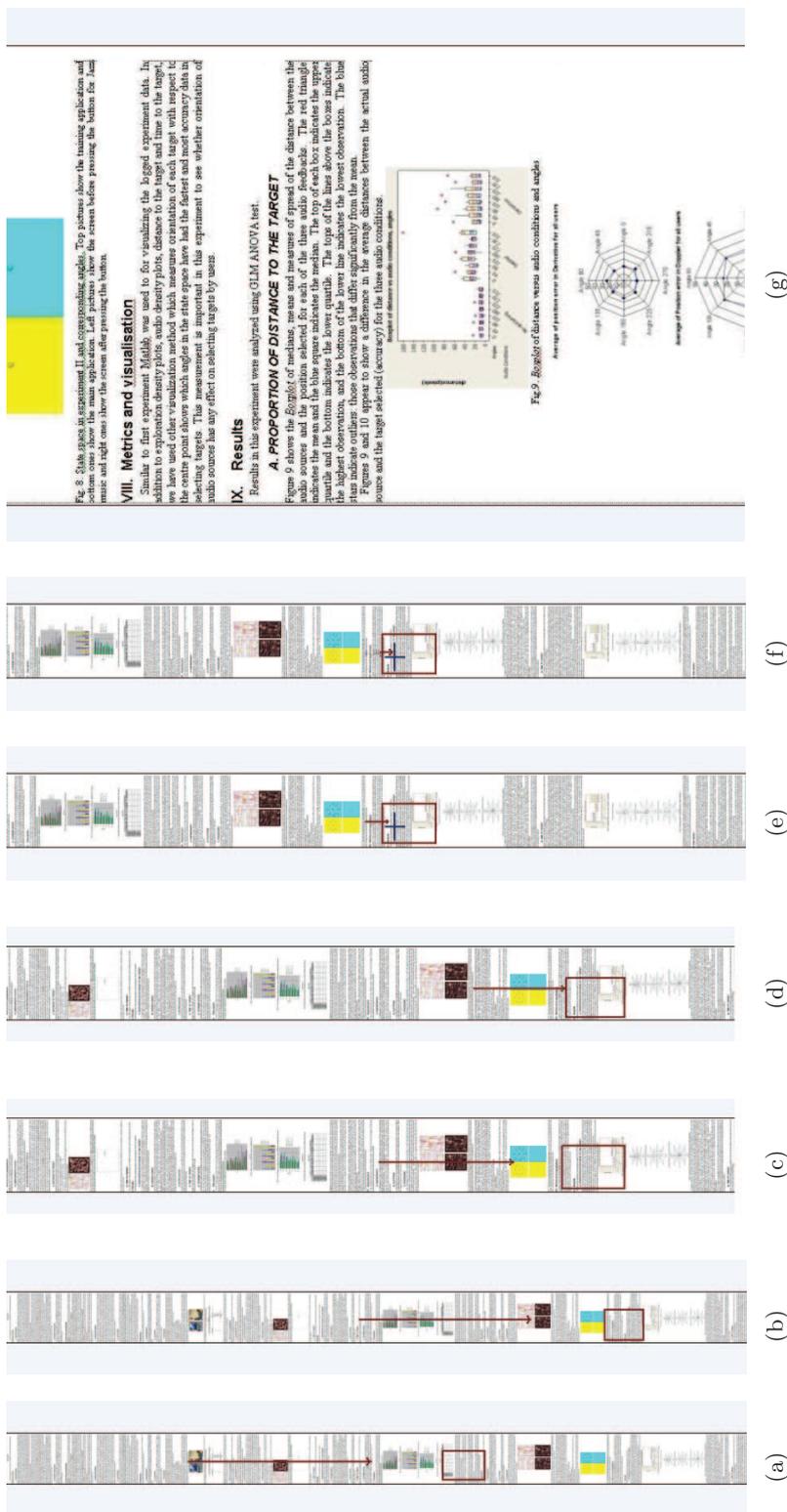


Figure 5.21: An example of reference signal and mode switch. (a) The user is scrolling over the document with a constant velocity v_{ref} . (b) The user has found the target and it is located inside the zooming window. (c),(d) The user returns the PDA back to the equilibrium point thus the controller scrolls to the zooming window with a constant magnification level. (e) When the zooming window is reached the position of the target becomes the reference position (x_{ref} , which is shown as a small blue cross) and the controller changes the current position value to the reference position. (f) The blue cross, x_{ref} is over the target and the controller dives toward the target position vertically. (g) The user has landed on the target and gets a magnified local view from the picture.

From Section 2.3 and Figure 2.1 we know the reference signal is a goal or a target the user is aiming to reach. The attempt to design systems that could keep variables in reference states led to development of control theory in the first place (Jagacinski et al., 1980). In control engineering, engineers design systems to control variables with respect to reference signals, and they plan to be able to manipulate the references (inputs) when they want to get the system to control a variable at a different level (as when we change the setting on the thermostat) (Brogan, 1991; Ogata, 1990).

Control systems and Reference Signals

In control systems the controller may support the user to complete the task with less effort by changing the interpretation of the inputs to being reference values, rather than control commands. In modern aircraft controllers there are different interpretations of aircraft controls depending on flight mode (e.g., take off, altitude-hold and so forth.) and blend seamlessly between modes (See (Tischler, 1994) for examples). For example, in tilt-controlled SDAZ we have two variables the user is aiming to reach: a desirable speed of scroll for browsing, which is also coupled to the level of zoom, and a target that the user is trying to land on. For these two variables we have two individual reference signals, v_{ref} and x_{ref} and these signals give an example of an intuitive mode transitions.

To show the effect of the reference signal in mode transition we ran a few examples. We asked the user to track a position in the document in cruising mode by holding the cross-hair over the target. Tracking has been started from top of the document. We logged the time series of the zooming-window position, velocity and level of zoom. As an example of tracking, 10th header in the document and its time series of data and phase plot is shown in Figures 5.21 and 5.22. In this example, while the user tilts the sensor at a constant angle, the controller maintains the desired velocity automatically, e.g., v_{ref} and completes the scrolling task with the velocity the user wants to achieve, rather than the user having to do this. Any change in the tilt angle for the controller means the user wants to change the v_{ref} (see Figure 5.15).

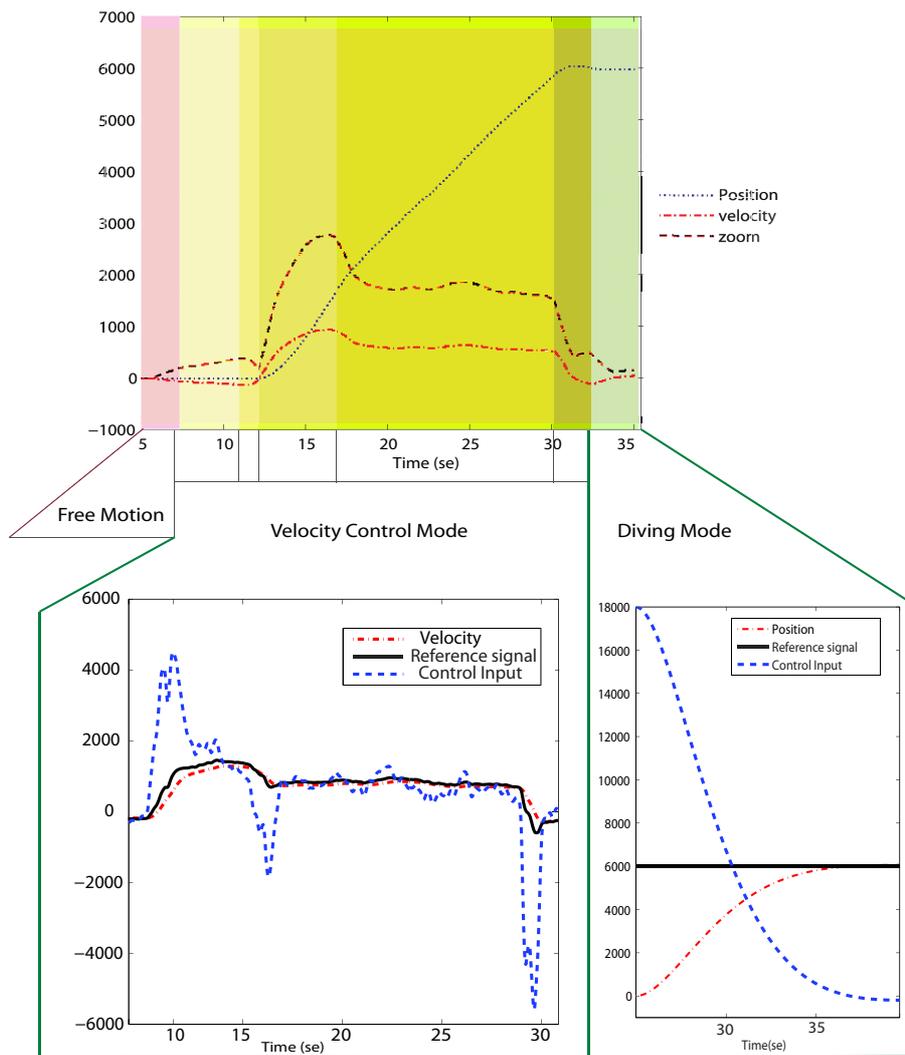
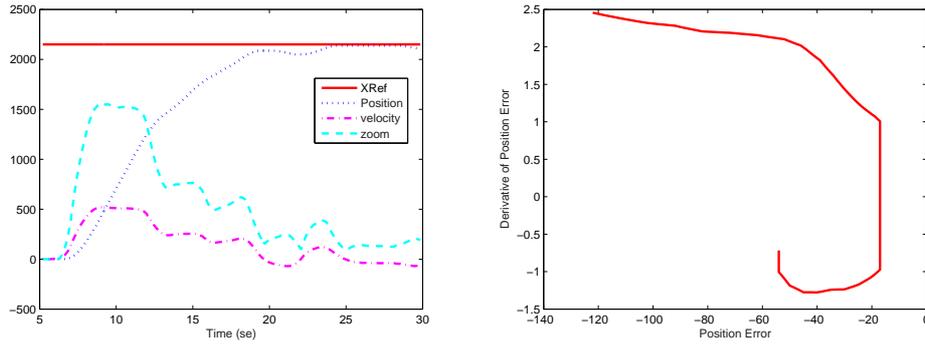


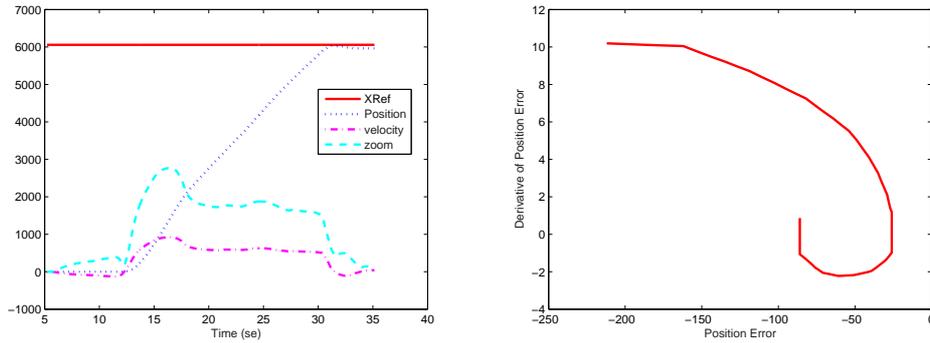
Figure 5.22: (a) A user's trajectory and position, velocity, and zoom-level data when he is looking for 10th header in the document (see Figure 5.21). Different colours highlight different modes of control or changes in the reference signal as explained in Figure 5.21. Bottom figures highlight the changes in v_{ref} and x_{ref} . In the velocity control mode, the system is moving velocity state variable toward the reference input, using control law $L(r - x)$. Here, L is set to 10 and in diving control mode, L is set to 3.

Similarly, in the diving mode, the system can reinterpret tilt input to change the desired position while zooming in to a point of interest after browsing (see Figures 5.16 and 5.21). During these mode transitions, in order not to have a sharp transition at the changeover, the offset variables⁷ have to be such that they are enough to cancel out the input provided by the user at the point they enter diving control mode. After transition, the offset values gradually reset to a

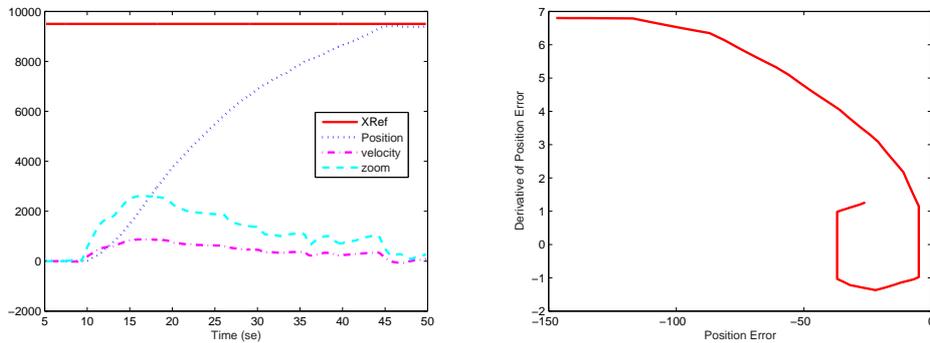
⁷The offset is the equilibrium point, or bias that is needed to bring a system to rest. Trim variables are another name for offset variable more often used in the aerospace field (the settings of flaps so forth that keeps an aircraft in a stable, or trim state) (Aponso et al., 1990; Bradley, 1996; Hess and Chan, 1988; Padfield, 1996).



(a) The user is targeting 5th header in the document.



(b) The user is targeting 10th header in the document.



(c) The user is targeting 12th header in the document.

Figure 5.23: Tracking a few targets in the document. (Left) Time series of the zooming-window position, velocity and level of zoom, (Right) Position error vs. derivative of position error (phase plots) in the last 1.25 seconds.

more sustainable position, but in such a way that the user gradually returns the device back to the equilibrium position. This means that as the user performs the various tasks they switch between control modes automatically, and their inputs have different meanings, but that the transitions are always smooth and natural, and the user is often not even aware that their movements are having a different effect in the different modes. Figure 5.22 presents an example of mode switching and transitions where the user is tracking 10th header in the document.

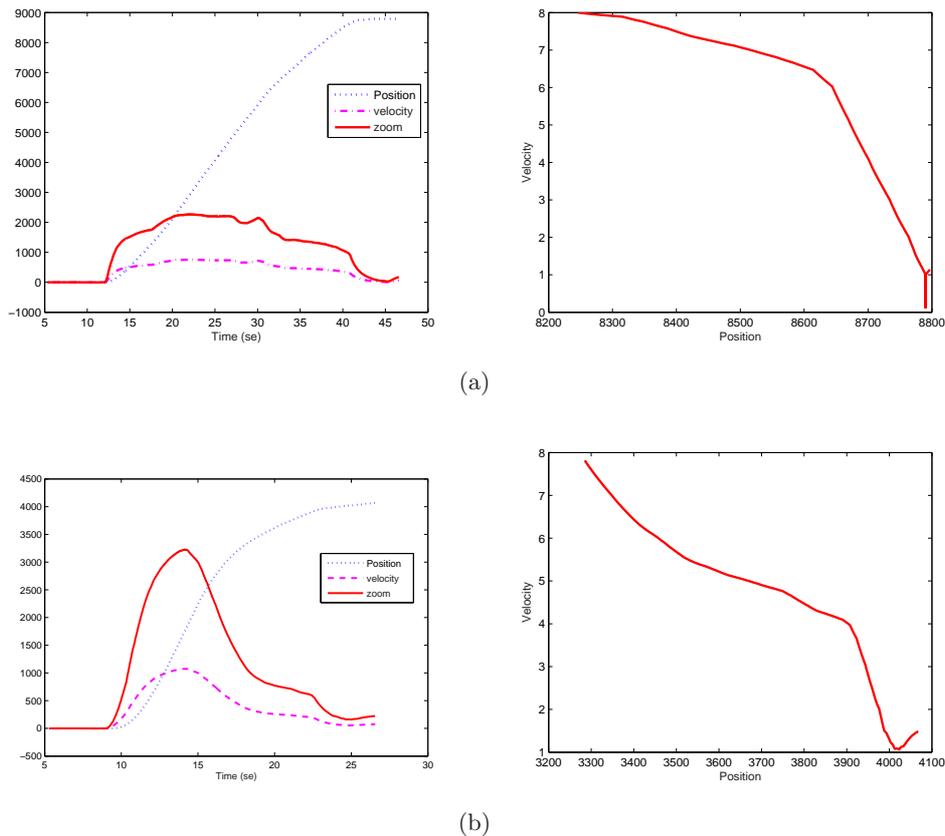


Figure 5.24: Examples of slowing down in the document when the eyes are closed. (Left) Time series of the zooming-window position, velocity and level of zoom, (Right) Position vs. Velocity (phase plots) in the last two seconds.

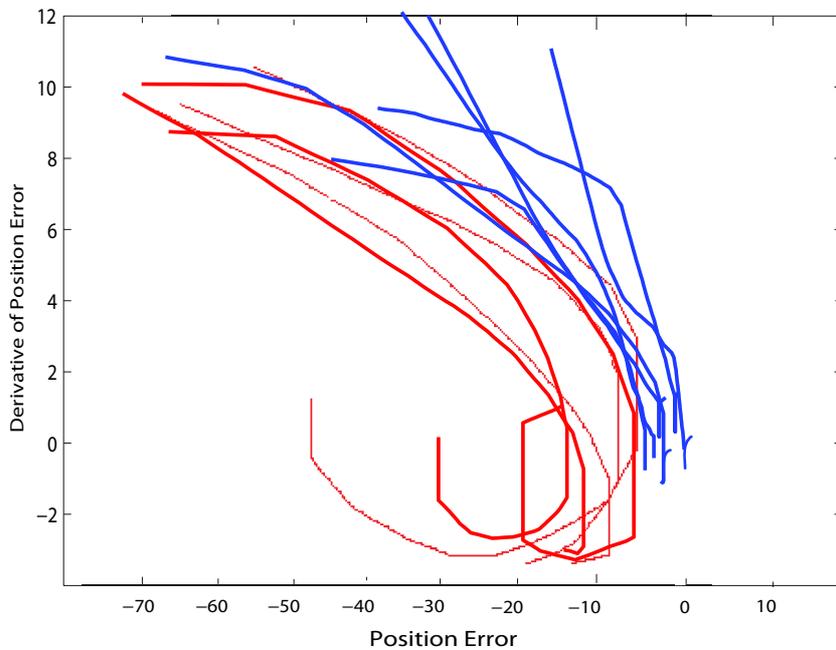


Figure 5.25: Phase plots of tracking task in the document in the last one second when the user is blindfolded (blue patterns) and when the user is tracking a few sub-headers and figure captions in the document (red patterns). Blue patterns have been scaled to zero because the error signal diversity is large in the blindfolded task.

Figure 5.23 presents more examples of the targeting in different positions in the document. We chose narrow targets, for example, headers in the document where the user does not need any horizontal scroll. In these examples, while the reference signal is available (targets), we see the user's targeting behaviour is quite similar (converging spiral in the phase plots) and the error signal is very small. In a similar experiment we asked the users to track sub-headers and figure captions in the document. We found that there was no significant difference between the targeting behaviour in headers and sub-headers or figure captions. We have collected them all in one figure to compare (see Figure 5.25). It proves that varying the reference signal (target position) does not change the targeting behaviour.

The user has adjusted his browsing and targeting behaviour depending on the position of the target in the document. In targets close to the top of the document (Figure 5.23(a)) for very short time the reference velocity is high and it smoothly decreases until the user finds and stops over the target. In targets far from the top (Figures 5.23(b) and 5.23(c)) the user spends more time scrolling with high speed.

In a different experiment we asked the user to close his eyes and explore the document and do some slowing down but there is no specific target to stop over. The results are shown in Figures 5.24 and 5.25. Here the stopping trajectories are different from those in the examples with chosen targets to stop over. It suggests that we can recognise and classify the user behaviour when s/he is aiming for a target from other patterns by a classifier, for example a multi-layer Perceptron (Ripley, 1996) or a Bayesian classifier (MacKay, 2003). This classification is useful in mobile situations and during the moments the user is not looking at the screen and is involved in other tasks, i.e., answering a phone call. In these situations any hand motion causes unwanted tilt input and it affects controlled variables in the application. Thus recognising unwanted targeting patterns helps in toggling off the input automatically. Hence, the classification supports intermittent interaction and prevents unwanted actions made by the user.

The focus of previous sections in this chapter have been on modeling a dynamic continuous system for tilt-controlled SDAZ. However, interactive systems are designed to be used by the user and building a quantitative model for the human operator facilitates the ability to predict the performance of human-machine systems.

5.4.4 Human Operator Modeling in Tilt-Controlled SDAZ

An important fact in all controlled systems is, the system itself might be stable, but when coupled with the time delay and lead-lag-dynamics of typical human control behaviour, the combined closed loop system might be unstable, as in pilot-induced oscillations in aircraft control (Jagacinski and Flach, 2003; Sheridan and Ferrell, 1974).

From Section 3.3 we know the frequency response of the human element changes with changes in the plant dynamics. The tilt-controlled SDAZ is a velocity control system, thus in this case the human looks like more like a gain and time delay (Figure 3.16 on page 52). In the velocity control mode we can introduce $a_1 = \frac{R}{m}$ and $b_1 = \frac{1}{m}$ and rewrite equation (5.9) as below:

$$\dot{x}_2(t) = -a_1 x_2(t) + b_1 u(t) \quad (5.23)$$

From equation (3.14) we can write the open-loop transfer function for the human, controller and the device, considering the device (PDA) is light and no delay is caused by that, as below:

$$Y_h(j\omega)C(j\omega)Y_p(j\omega) = [Ke^{-j\omega\tau}] \cdot \left[\frac{b_1}{j\omega + a_1} \right] \cdot 1 \quad (5.24)$$

The left bracket is a transfer function for human operator, which is a simple gain and time delay, the middle bracket is the transfer function of the SDAZ in the velocity control mode and the last one indicates a simple gain for the device.

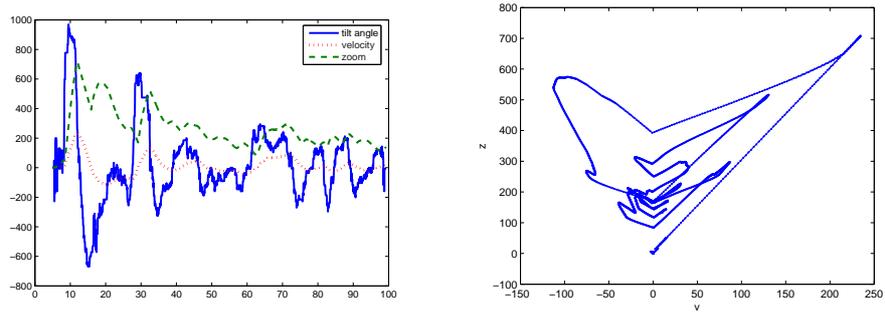
In (Jagacinski and Flach, 2003) it has been shown that time delay, τ , is between 0.1 (s) and 0.25 (s) and crossover frequency, K is between $4 s^{-1}$ and $6 s^{-1}$ for velocity control systems. As an example to show how the changes in

coefficients a_1 and b_1 affects both human and controller we chose gain, $k = 5 s^{-1}$, and time delay, $\tau = 0.2$ (s). We set coefficients $m = 10$ kg, R and $R' = 1$ kgs^{-1} , $b = 3$ kgs^{-1} and $c = 3$ or $a_1 = 0.1 s^{-1}$ and $b_1 = 0.1$ kg^{-1} and asked a user to scroll down a document browser developed on a PDA with tilt sensor and find two figures there. Figure 5.26(a) presents the user behaviour in this task. It is obvious the user has not been comfortable with this task and he complained it was almost impossible to land on the figure because any slight tilt was causing sluggish behaviour in zoom (slope of zoom vs. velocity has been very variable Figure 5.26(b)). This also supports the comments made by Gaines (1969) (refer to Section 3.3.2 on page 54) about the variability of the human operator's switching boundary in controlling an unstable second-order system. In this unstable system the user had to change his switching lines (one between acceleration to coast and the other between coast to deceleration) to control the targeting.

Figure 5.26(c) presents the user's input and sum of changes in the tilt input. The total sum of input changes, J_s in equation (5.21) on page 129, for this user in this task was 15304 unit. Figure 5.26(d) presents Bode plots of the open-loop transfer function for the human and controller with the setting mentioned earlier. All Bode plots presented in this section have been produced in MATLAB in the simulated setting presented in equation (5.24). For the MATLAB code see Appendix C.

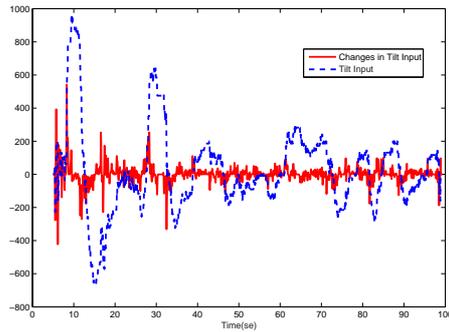
We changed the coefficients $m = 10$ kg, R and $R' = 5$ kgs^{-1} , $b = 3$ kgs^{-1} and $c = 3$ or $a_1 = 0.2 s^{-1}$ and $b_1 = 0.1$ kg^{-1} and asked another user to repeat the task. Figure 5.27(a) presents the user behaviour in this task and there is a slight improvement in controlling the task. Figure 5.27(c) presents the user's input and changes in the tilt input. J_s for this user in this task was 8118 unit, which is much lower than previous user's activity and J_t , the time taken to complete the task is considerably shorter than previous example. Furthermore, this user's phase margin, Figure 5.27(d), is higher than previous one.

In another setting $m = 10$ kg, R and $R' = 10$ kgs^{-1} , $b = 3$ kgs^{-1} and $c = 3$ or $a_1 = 1 s^{-1}$ and $b_1 = 1$ kg^{-1} with different user for the same task we

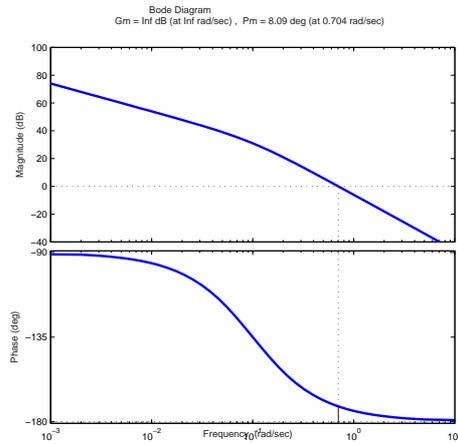


(a) User's tilt behaviour and changes in velocity and zoom

(b) Zoom vs. velocity



(c) Total sum of changes in input is 15304 unit.



(d) Phase margin = 8.09 degree and amplitude ratio = Infinite db

Figure 5.26: Controller with settings $m = 10$ kg, R and $R' = 1$ kgs⁻¹, $b = 3$ kgs⁻¹ and $c = 3$ or $a_1 = 0.1$ s⁻¹ and $b_1 = 0.1$ kg⁻¹.

could get the behaviour presented in Figure 5.28(a). This user's performance was much higher than two previous ones with only 5265 unit in his total sum of input changes and it has taken shorter time than two previous subjects to complete the task (Figure 5.28(c)). Moreover, his phase margin's plot highlights this fact, too (Figure 5.28(d)).

Other settings for this system could not bring the cost down or maximise the phase margin more than settings, $a_1 = 1$ and $b_1 = 0.1$ (Figure 5.29). Thus this simple example shows, first, the controller with settings $m = 1$ kg, R and $R' = 10$ kgs⁻¹, $b = 3$ kgs⁻¹ and $c = 3$ is stable; second, a quasi-linear model of human operator (first-order system, equation (5.24)) is a suitable model for our task; third, phase margin and amplitude ratio of the open-loop transfer function for the human and controller is maximised for this setting; fourth, the cost function (either the time required to complete the task, equation (5.20) or total sum of changes in the input, equation (5.21)) is minimised for this setting. For these reasons and for later research we kept these setting for the controller to compare its efficiency with other input methods, which will be discussed in later sections in this chapter.

The next section presents an example application for browsing a document developed on a PDA to highlight a few effects of calibration by taking into account the results in the previous sections.

5.5 Example Application – Document Browser for a PDA

We implemented a touch-screen version of the tilt-controlled SDAZ for browsing the same document used in previous examples to compare with the tilt-controlled version. The state-space settings for the touch-screen one was the most stable setting in previous section, $m = 1$ kg, R and $R' = 10$ kgs⁻¹, $b = 3$ kgs⁻¹ and $c = 3$.

Users found the touch-screen-based mechanism intuitive and easy to use for browsing. Figure 5.30 presents the system's inputs in three SDAZ applications to find the same paragraph used in scroll bar browser for tilt-based and touch-screen-controlled SDAZ. Additionally this figure presents an example run with tilt-based SDAZ, with augmented velocity control, as described in Section 3.2.9, to browse the document to find 7 main headings. For comparison, the central plots in Figure 5.30 show tilt-based SDAZ without augmented velocity control

on the same task, where fluctuations indicate that controlling the zoom level was difficult, and hunting behaviour appears when users tried to land on the targets (e.g., $t=20, 40, 85$ seconds in Figure 5.30(b)).

5.5.1 Discussion

We asked five users from our research lab to work with the document browser using tilt-based SDAZ and touch-screen-controlled SDAZ with and without augmented velocity control. Users who did the experiment without augmented velocity control suggested that adding a control option or a switch to control the zoom-level with velocity and tilting angles will make the system more comfortable to use. Most of them proposed if they could control level of zoom by tapping on the screen or pressing a key on the PDA, the application would be easier to use.

In contrast, the users who did their experiments with augmented velocity control were satisfied with the application in both tilt-based and touch-screen-controlled modes; because they commented they could easily land in on the goal without tilting back and forth to adjust their targeting. Some users complained that with tilt input, they had to tilt the device to angles which caused irritating reflections from the Pocket PC screen. We could improve this by calibrating the interface to the starting tilt-angle in the user's palm.

Users in both groups, with and without augmented control, commented that if they were involved with other tasks, (answering the phone, showing a figure on the PDA to someone, and so forth) they would prefer the touch-screen-controlled SDAZ because they imagined it would be difficult to stay in the desired position in the document with a tilt-based SDAZ. This is one of the significant disadvantages of using motion as an input in a handheld device. Motion as an input in a handheld scenario limits the usefulness of the visual display for the duration of the input; as the user is moving the device, s/he is unable to clearly see its screen (Oakley et al., 2004). Using a classifier suggested in Section 5.4.3 would be one solution to filter out unwanted movements. A more complex controller that responds to only intended angles of tilt and filters unintended angles or a

controller that senses different contexts and locations the user is in and toggles on suitable inputs are other solutions for this problem.

Furthermore the real physical model of the system (e.g., a flying object) provided a clearer understanding about the tilt-controlled SDAZ. Users who were told about this model could improve their actions quickly and commented that after explaining the actual physical model the interaction made more sense.

In the next section we use multimodality as a possible solution for this problem in tilt-controller SDAZ and its application in browsing a document.

5.6 Multimodal Feedback in a Tilt-Controlled SDAZ

Earlier in this chapter it was shown how interaction models and state-space design can help create interactive systems. This design focuses on the lower level of sensory-motor phenomenon and here we show how this method may help in higher level of context of use.

Using motion as an input in a handheld device reduces the quality of the visual display for the duration of the input, due to reflections from the screen and difficulty in concentrating on a rapidly moving screen (Oakley et al., 2004). Consequently, we believe that non-visual feedback will be an essential component of movement-based interaction techniques. Audio/vibrotactile feedback in particular seems suitable for this role as it can be discretely presented directly to a user's ears/hand, and is already prevalent in mobile devices. Audio or vibrotactile feedback may be crucial to support tasks or functionality on mobile devices that must continue even while the user is not looking at the display (Hinckley et al., 2000).

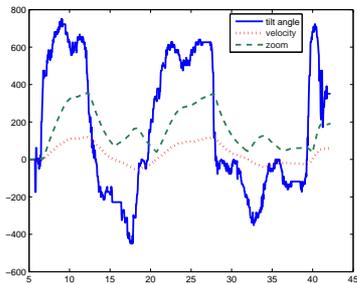
There are several stages in the process that produces audio/haptic representations out of raw, abstract data. A general method which has been used in our application is presented in Figure 5.31. The starting point in adding multimodality is the raw data. This data, for example, Microsoft document, is in "Data Tables" format. Data tables can describe many types of data, header, sub-header, paragraph, table, figure, variables, and so forth in multiple dimensions.

Data tables are transformed into visual/audio/haptic structures by applying visual/audio/haptic mappings. In our application visual structures are transferred to an image format, BMP or PNG. Audio/Haptic mappings will be discussed in more details in the next section.

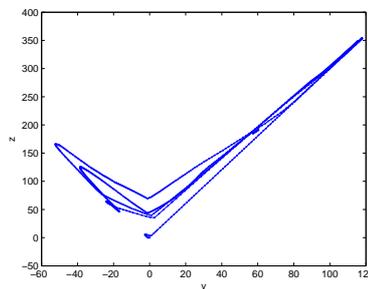
5.6.1 Design

We have used two mechanisms by which we can support tilt-controlled SDAZ with audio feedback for rate of scrolling and structural information, to highlight specific information that is currently on the screen.

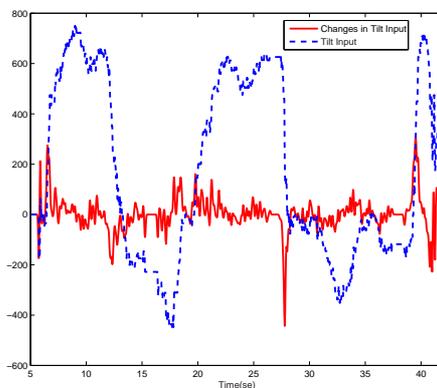
As an intuitive model of the sonification process, we can imagine the text on the screen to be embossed on the surface. This embossed type excites some resonating object (elastic band or guitar string, for example) as it is dragged over the text. This physically motivated model is similar in nature to the model-based sonifications described by [Hermann and Ritter \(1999\)](#).



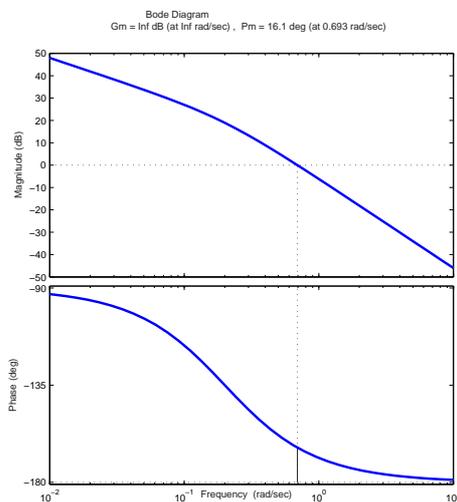
(a) User's tilt behaviour and changes in velocity and zoom



(b) Zoom vs. velocity

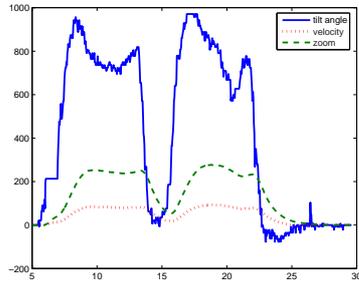


(c) Total sum of changes in input is 8118 unit.

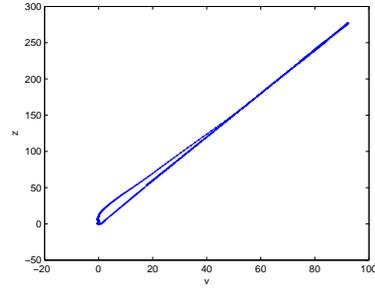


(d) Phase margin = 16.1 degree and amplitude ratio = Infinite db

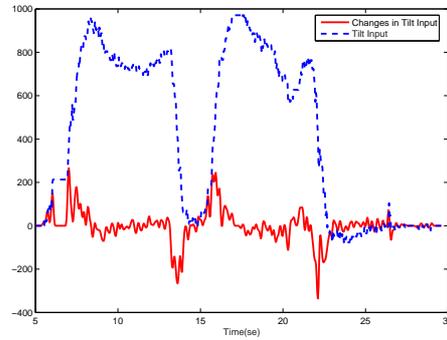
Figure 5.27: Controller with settings $m = 10 \text{ kg}$, R and $R' = 5 \text{ kgs}^{-1}$, $b = 3 \text{ kgs}^{-1}$ and $c = 3$ or $a_1 = 0.2 \text{ s}^{-1}$ and $b_1 = 0.1 \text{ kg}^{-1}$.



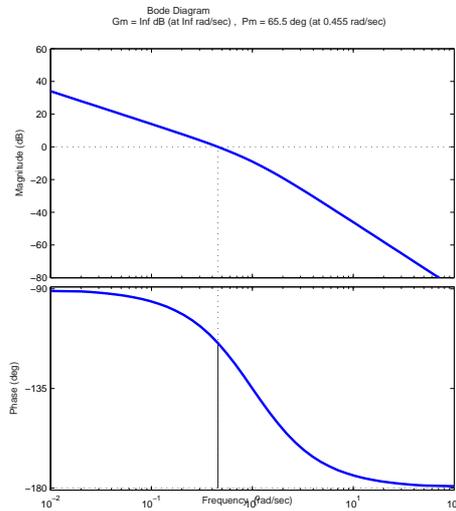
(a) User's tilt behaviour and changes in velocity and zoom



(b) Zoom vs. velocity

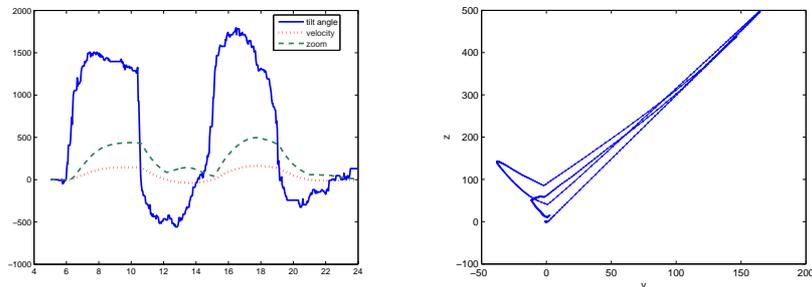


(c) Total sum of changes in input is 5265 unit.



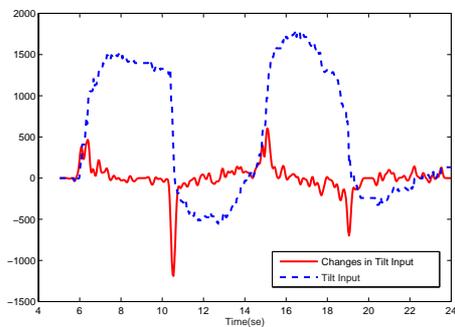
(d) Phase margin = 65.5 degree and amplitude ratio = Infinite db

Figure 5.28: Controller with settings $m = 10$ kg, R and $R' = 10$ kgs⁻¹, $b = 3$ kgs⁻¹ and $c = 3$ or $a_1 = 1$ s⁻¹ and $b_1 = 0.1$ kg⁻¹.

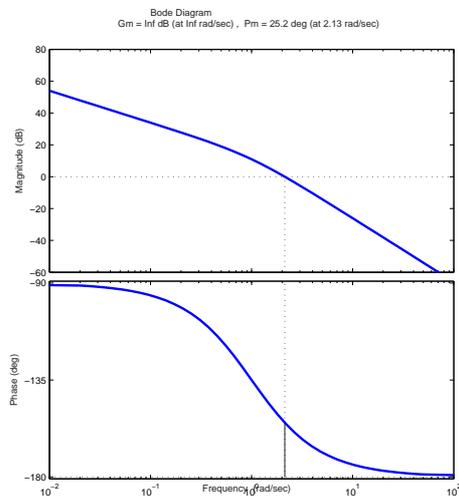


(a) User's tilt behaviour and changes in velocity and zoom

(b) Zoom vs. velocity



(c) Total sum of changes in input is 9428 unit.



(d) Phase margin = 25.2 degree and amplitude ratio = Infinite db

Figure 5.29: Controller with settings $m = 1$ kg, R and $R' = 1$ $kg s^{-1}$, $b = 3$ $kg s^{-1}$ and $c = 0.5$ or $a_1 = 1$ s^{-1} and $b_1 = 1$ kg^{-1} .

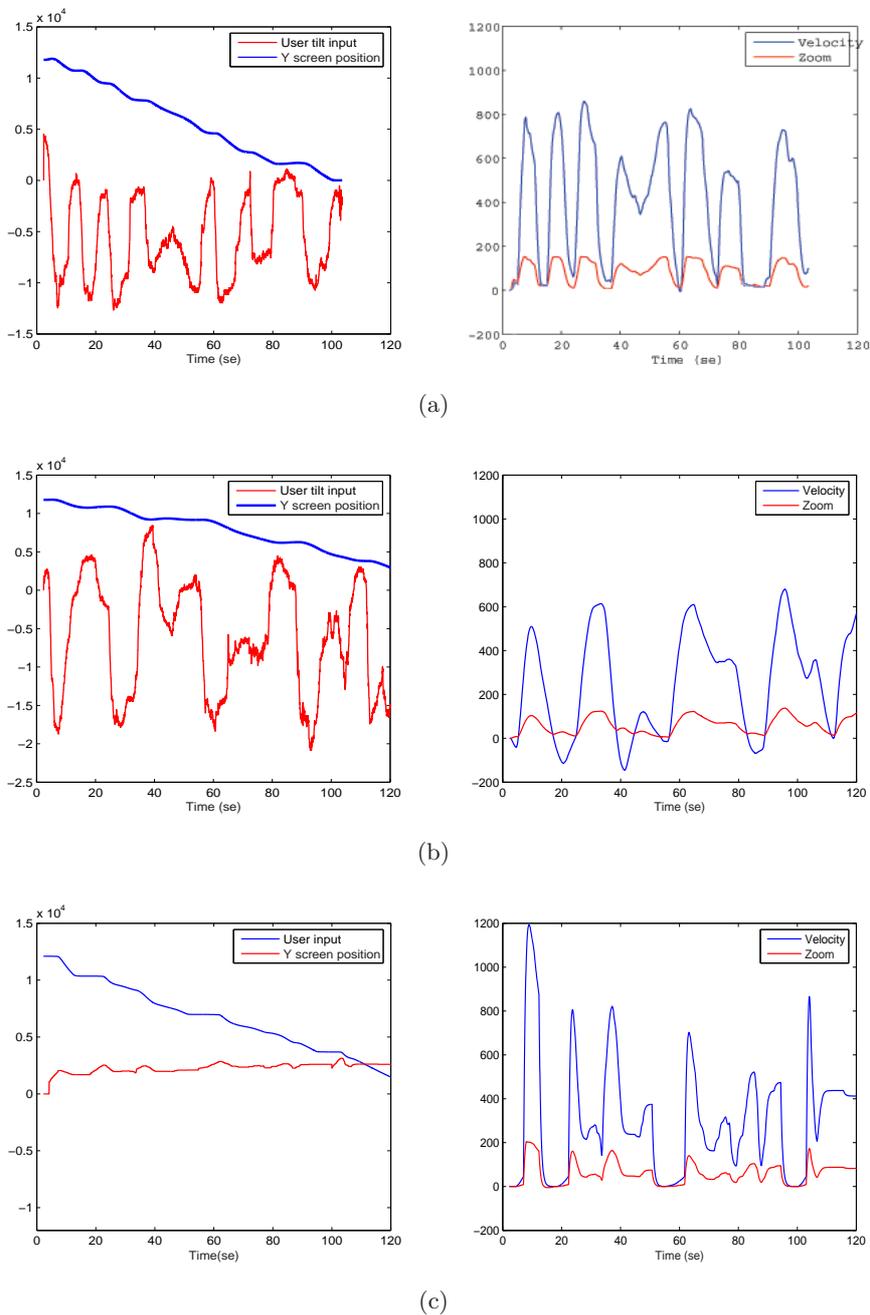


Figure 5.30: (a) Tilt-controlled SDAZ with augmented velocity control, (b) Tilt-based SDAZ without augmented control. Hunting behaviour appears in tilt-controlled SDAZ without augmented control mode around time 20(s), 40(s), and 85(s), (c) Touch-screen-controlled SDAZ.

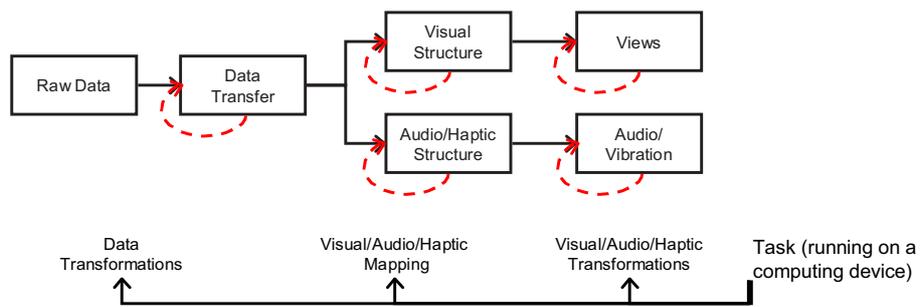


Figure 5.31: The reference model for multimodality in designing interfaces. Adapted from [Card et al. \(1999\)](#).

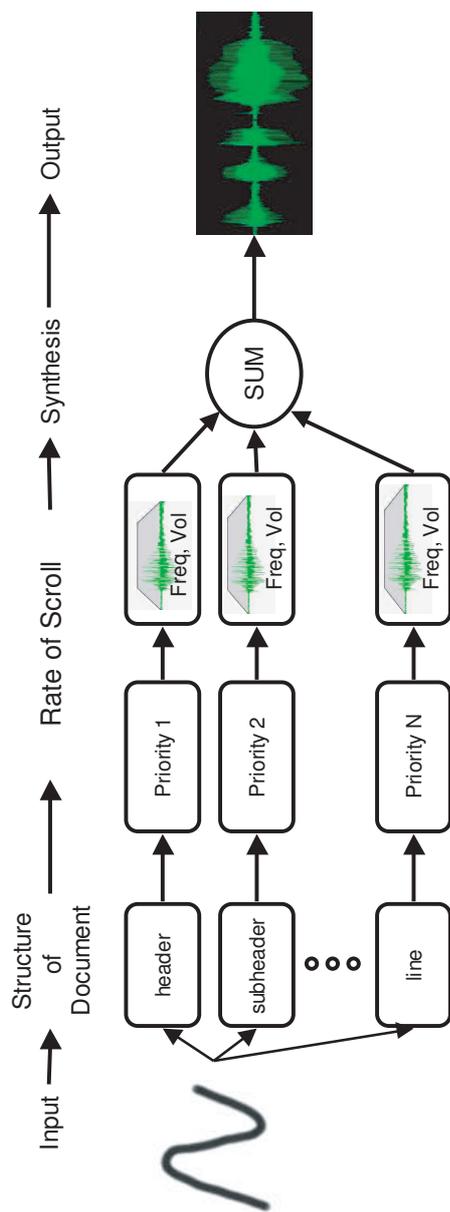
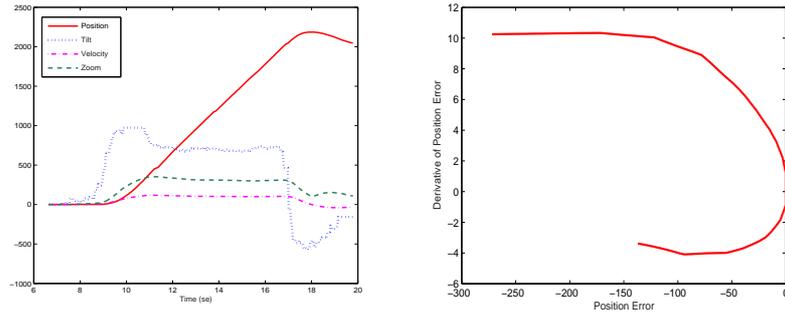


Figure 5.32: A general framework of the model-based sonification system for the document browser. The audio textures as the user passes over the document gives the both the impression of the structure of the text as well as the speed and zoom level at which s/he is passing it.

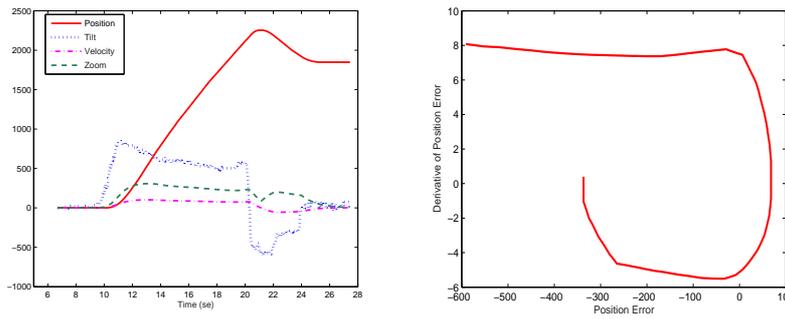
5.6.2 Sound Synthesising

We simulate this model in our implementation by drawing an audio sample and placing that in an audio buffer, as each line in the document “hits” the zooming-window. This technique is a form of granular synthesis; (Williamson and Murray-Smith, 2004a) gives other examples of granular synthesis in interaction contexts. A real world example would be the perception of continuous radiation values via discrete pulses from a Geiger counter; in this paper the continuous variable is the text flow rate (Figure 5.32). The strength of excitation associated with higher rate-of-scroll changes the acoustic response of the system, e.g., sampling frequency and volume of the audio sample decreases and provides the sense of distance to the text. As the speed increases, headings, sub-headings, figures and tables become relatively more prominent, to give a better overview of the document structure (an audio equivalent of semantic zooming), because these structures have a higher priority than the standard lines of text. The rate of scroll controls the play rate of audio samples inside the audio buffer, i.e., the sound samples with higher priority are played sooner than sound samples for each line passing. Furthermore, volume and frequency have inverse relation to rate of scroll. At greater ‘heights’ the features are blurred and damped suitably. As frequency and volume of the audio samples decreases when the user zooms out, scrolling slowly gives distinct audio feedback for individual lines of text. In this fashion, the audio texture as we pass over the document gives both an impression of the structure of the text, as well as the speed and zoom level at which we are passing it.

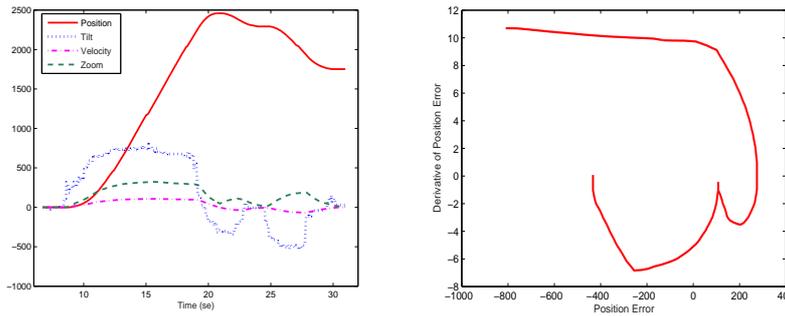
The particular audio cues chosen in our implementation of the text browsing are: scrolling over lines gives the impression of the sound of typing with a teletype keyboard. Passing over headers produces the sound of knocking a heavy object; sub-headers have a less important role than headers thus the sound is the same as header but with lower pitch, and the sound for figures gives the sense of dragging a large object. The sound for tables highlights the tabular structure like a “bing”. A change in zoom level, as e.g., in target acquisition in the diving control mode, is accompanied by the sound of rushing air. This gives the user



(a) Visual only task.



(b) Audio only task.



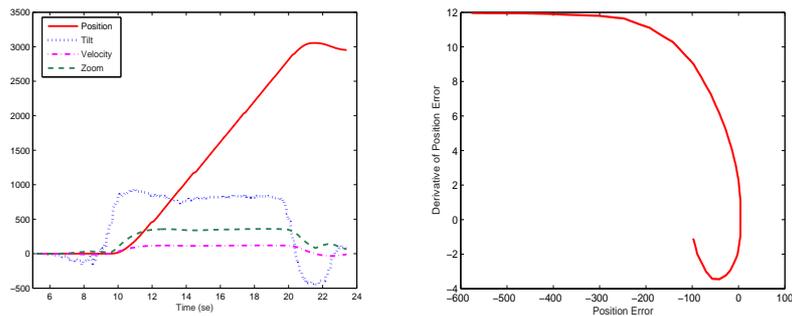
(c) Vibrotactile only task.

Figure 5.33: Searching for 4th header in the document. (Left) Time series of the zooming window position, velocity, zoom and tilt input. (Right) Position vs. velocity (phase plots).

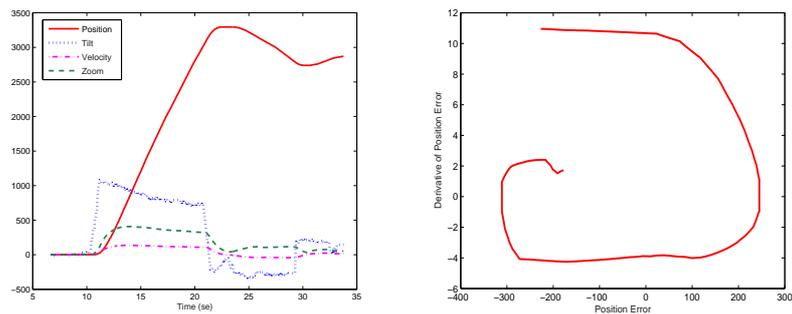
an impression of transition which is especially useful when there is no change in document position.

5.6.3 Experiment

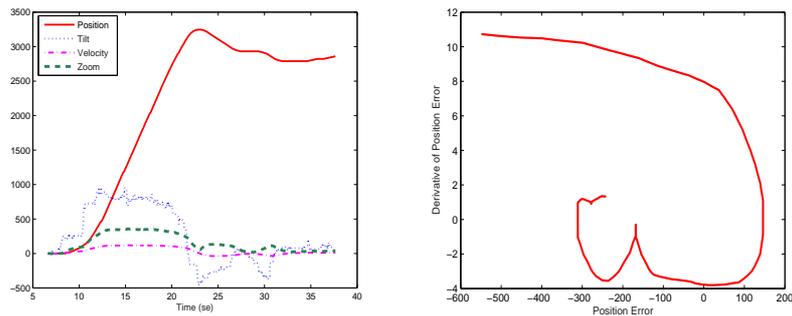
This study is carried out with an HP 5500 PDA with the Xsens P3C accelerometer and a headset (shown in Figure 5.1). In this study we map the zooming-window's position and its speed to the audio space. In three tasks, i.e., audio only, visual only and vibrotactile only, we asked users to find three different



(a) Visual only task.



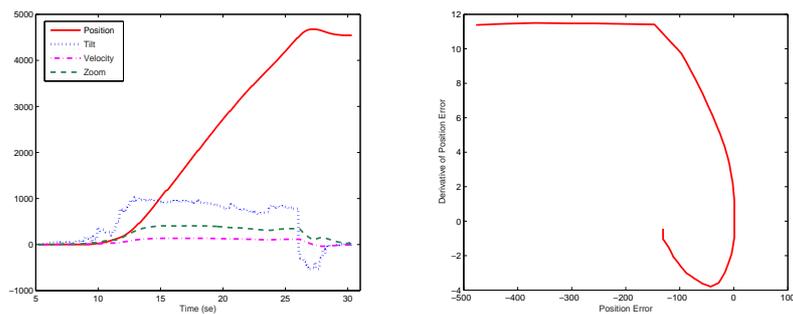
(b) Audio only task.



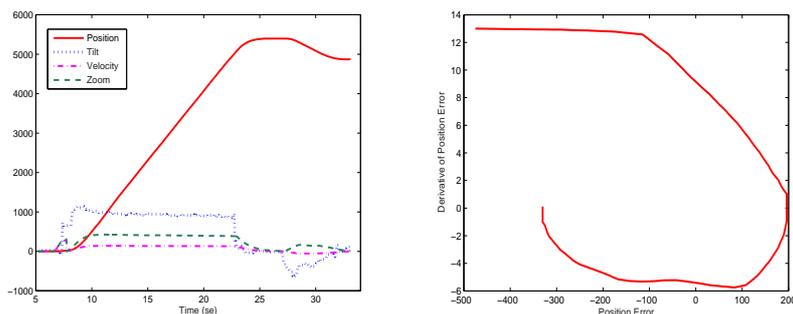
(c) Vibrotactile only task.

Figure 5.34: Searching for 5th header in the document. (Left) Time series of the zooming window position, velocity, zoom and tilt input. (Right) Position vs. velocity (phase plots).

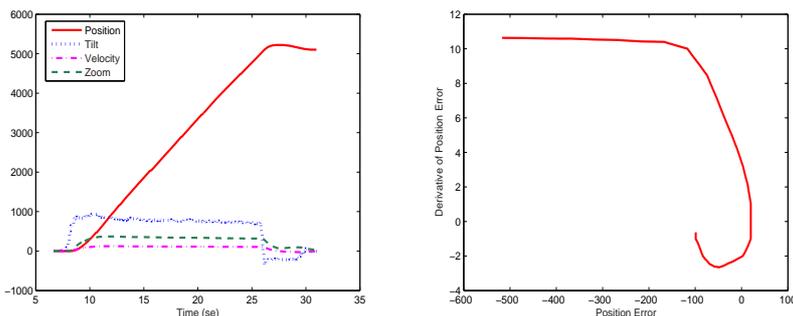
targets, 4th and 5th headers and 7th figure in the document. Figures 5.33, 5.34 and 5.35 present the users' trajectories, time series of the zooming window position, velocity, zoom, tilt input and phase plots. The users were given time to familiarise themselves with the system, and the specific document. They browsed the document in three versions of the application: (a) tilt-based SDAZ with visual display only, no audio or vibrotactile feedback, (b) with audio feedback only, no visual/haptic display (the user did the experiment blindfold), and (c) with vibrotactile feedback, no audio/visual feedback. The results show that the



(a) Visual only task.



(b) Audio only task.



(c) Vibrotactile only task.

Figure 5.35: Searching for 7th figure in the document. (Left) Time series of the zooming window position, velocity, zoom and tilt input. (Right) Position vs. velocity (phase plots).

audio/haptic cues were sufficient for the users to distinguish when they passed the target, slowed down and returned to the target. The phase plots, trajectory and tilt angles are as smooth as the visual-only SDAZ. The difference here is the users worked with visual display only was faster in locating the target and landing on that and in both audio and vibrotactile feedback we see overshoots on the trajectories, while the visual one allowed an over-damped target acquisition because of the extra predictive power of the visual display. Phase plots of velocity vs. position close to landing (See Figures 5.33 to 5.35) show that the

narrower the target, more the overshoot happens. Additionally, we calculated the users' performance (sum of changes in filtered tilt input, see equation 5.21 on page 129) in these tasks, shown in Table 5.1. This provides strong evidence that audio and haptic feedback needed more effort from the user for targeting and landing and as the target gets bigger, performance difference between visual task and audio/haptic task grows smaller (compare targeting the figure with the header in Table 5.1).

The system was also informally evaluated by a blind user. The user commented that

... [the system] has potential as a scrolling interaction for non-visual interfaces such as speech, but it has yet to be integrated with speech-based content. The sounds used are well-chosen from the point of view of controlling the speed of scrolling and drawing attention to key features in the document.

Table 5.1: Users performance in different targeting tasks using vision only, audio only and haptic only

Task	sum of changes (unit)
Visual- 4th header	36113
Audio- 4th header	41712
Haptic- 4th header	47293
Visual- 5th header	38501
Audio- 5th header	47118
Haptic- 5th header	55063
Visual- 7th Figure	51969
Audio- 7th Figure	55826
Haptic- 7th Figure	56577

An interesting observation relating to the vibrotactile work in (Oakley et al., 2004) was that most users thought that the purely vibrotactile system also had audio feedback, and similarly in our work, although it was only audio feedback, users had a strong sense of vibrotactile feedback. A combination of the approaches seems a promising research direction.

5.7 Conclusions and Summary

This chapter provided broader view toward dynamic simulation, continuous control and human modeling.

5.7.1 Dynamics and Modeling in Tilt-Controlled SDAZ

This chapter gave an example of state-space modeling for tilt-controlled SDAZ based on a flying object. The applicability of the approach was demonstrated by implementing the SDAZ interface for a text browsing system on a PDA instrumented with an accelerometer, and a stylus. The real physical model (e.g., a flying object) of the dynamic system provided a better understanding about the tilt-controlled SDAZ and helped the users to improve their actions. The standard matrix format provided for state-space equations showed that a single degree of freedom input could control velocity and level of zoom (controlled variables). The flying object model of SDAZ (combinations of springs, masses and damping effects) allowed multiple variables, and derivative effects (e.g., position, velocity, and acceleration) to be coupled with zoom level, without any further coding, by just changing the entries of the A and B matrices. It was shown that in general (i.e., interaction with higher degrees of freedom input), this approach makes tuning and calibration easier because proper settings can only be found by observing the behaviour of the simulated system before the actual implementation. Furthermore, this model can be generalised to a nonlinear model, so the state-space modeling has a potential in providing a general framework for development, analysis, calibration, and optimisation.

5.7.2 Augmented Control and Reference Signal

We showed that in control systems the controller can change the interpretation of the inputs to being different reference values. In a dynamic, continuous control model for the tilt-controlled SDAZ, the user controls v_{ref} or x_{ref} as a desired velocity or position manually and the controller maintains this velocity or position automatically and completes the task for the user. According to refe-

rence variables x_{ref} and v_{ref} , the controller switches among four discrete states, no action, free motion (i.e., basic acceleration mode), velocity and diving control modes. During mode transitions, in order not to have a sharp transition at the changeover, the offset variables change such that to cancel out the input provided by the user at the point they enter a new control mode. After transition the offset values gradually reset to a more sustainable position, but in such a way that the user gradually returns the device back to the equilibrium position, so the transition is smooth and natural, and the user is often not even aware that their movements are having a different effect in different modes. Moreover, users commented that with augmented velocity control the application was easier to control during landing; because the controller's setting is adapted to the task the user tends to do and makes that task easier to control for the user and it improves hunting behaviour.

5.7.3 Modeling the User Behaviour

A number of examples were presented to show that, the controlled system itself might be stable, but when coupled with the time delay and lead-lag-dynamics of typical human control behaviour, the combined closed loop system might be unstable. It proves control theory can support design of closed-loop interaction between human and system. We modeled human operator like a gain and time delay, plotted the Bode plots of the open-loop transfer function for the human and controller and calculated the activity of the user using a performance function with different settings for the controller and human. It helped us to choose settings that suit both the system and the user and made the controlled system stable when coupled with user model.

5.7.4 Tilt Control Interaction

The tilt-controlled version has its own pros and cons. The tilt input application can be controlled in a single-handed manner, without obscuring the screen. Users preferred the stylus, as there were no reflections from the screen and they could stop interacting by taking the stylus off the screen. In the tilt-controlled

version users have to tilt the device to angles, which caused irritating reflections from the Pocket PC screen. We improved this by calibrating the interface to the starting tilt-angle in the user's palm as an equilibrium point. Furthermore, users commented that if they were involved with other tasks, i.e., answering the phone, and so forth they would prefer the touch-screen-controlled SDAZ because it would be difficult to stay in the desired position in the document, with a tilt-based SDAZ. Recognising targeting patterns as discussed before may help in toggling on/off the input automatically.

5.7.5 Multimodal Tilt-Controlled SDAZ

Next, we presented an audio/haptic feedback representation of the speed-zoom coupling involved in speed-dependent automatic zooming. The applicability of the approach was demonstrated by implementing the SDAZ interface for a text browser system on the PDA instrumented with the tilt sensor. Sonifying each piece of structural information in the document was easy to understand by users and they could feel different textures in the document even blind people. The results showed that the audio/haptic cue is sufficient for the blindfolded users to distinguish where the target is but when they start to land they have already passed the target, so they have to adjust the tilt and go back to the target. Additionally, the users' activities in the audio and haptic only interface were higher than the visual only, most likely because the vision is leading sense (this will be discussed in the next chapter). Providing audio feedback about the user's predicted position instead of their current position may solve this problem (see Chapter 4). Multimodal SDAZ can also support intermittent interaction.

In the next chapter we introduce a similar approach in designing interfaces to multimodal SDAZ, for a focus-in-context method and extend that to support human behaviour in browsing a document, and feedback its contents visually and in non-speech audio based on a language model and prediction.

Chapter 6

Multimodal Motion Controlled Focus-in-Context Method: Sensing Complex Information

This chapter introduces a dynamic system approach to the coupling of internal states involved in a focus-in-context visualisation. We use an example, where we support human behaviour in browsing a document, and feedback its contents visually using the focus-in-context method and in non-speech audio based on a language model. We alter the dynamics of movement in the document as a function of the interpreted behaviour. It is argued that to design interaction we need models of key aspects of the process. Here for example, we need models for the dynamic system, a probabilistic language model and a probabilistic audio feedback as an example of a multimodal approach to sensing different languages in a multilingual text. We demonstrate that how the user's intention is coupled to the visualisation technique via the dynamic model, and how the focus-in-context method couples details in context to audio samples via the language identification system.

6.1 Introduction

As mentioned in the preceding chapters the unique challenge in the computer-as-tool paradigm (see Section 2.4.2 on page 21) is to create new tools that both augment and complement human capabilities. One important area of research in

this chapter is presenting multimodal information on the display. Thus, we utilise focus in context techniques, which apply complex algorithms to data and human perceptual abilities to extract patterns, to facilitate the visual presentation issue.

Psychology's gestalt theory deals with issues regarding details and context, stating that details have more meaning when presented within their context. Specifically, [Wertheimer \(1938\)](#) states that, "*there are wholes, the behaviour of which is not determined by that of their individual elements, but where the part-processes are themselves determined by the intrinsic nature of the whole.*" [Furnas \(1986\)](#) illustrates an efficient way of embedding a specific piece of information within its larger context. He represents those portions of the context that are closer to the immediate area of interest in greater detail while including only some major landmarks of the context further away. His method suggests that such views (he called them 'fisheye views') might be useful for the computer display of large information structures like programs, data bases, online text, and so forth ([Furnas, 1986](#)) and for large steering tasks ([Gutwin and Skopik, 2003](#)).

In this chapter, we extend this issue to the multimodality and the human interaction with multimodal interfaces. We introduce browsing and sensing multilingual texts as an example of a continuous interactive system and present a model-based interactive method for searching a particular language based on a language model, sonification, a focus-in-context method and continuous interaction interface, which can be linked to a wide range of inputs and feedback/display mechanisms.

6.2 Related Work and Background

In this section we explore the presentation problems and its possible solutions.

6.2.1 The Presentation Problem

Providing both detailed and contextual information in the same view is a crucial issue, especially on displays with constrained view, for instance, mobile phones. In the past 20 years many researches on the information visualisation have been done in solving this problem. [Spence \(2001\)](#) categorises these solutions into: (1) *focus + context*, (2) *suppression of information*, (3) *magic lenses*, (4) *browsing*, (5) *effective views*, and (6) *zoom and pan*. Focus-in-context and suppression of information will be focus of the research in this chapter, thus we explore their principles in brief in this section.

Focus+Context Techniques

[Card et al. \(1999\)](#) and [Carpendale and Montagnese \(2001\)](#) suggest three premises for focus + context techniques: “*First of all, both the context and the detailed information must be available simultaneously. Second, the type of information shown in the detailed view and context may be different from one another. Third, these two types of information should be combined into one display.*”

Generally distortion in focus + context techniques is controlled by a visual transformation function, which distorts the visualisations through stretching and compression, in order to give the focal portion of the visualisation more visual detail. The shape of the transformation, that is how the magnification factor changes across the visualisation, is expressed by a magnification function that is a derivative of the visual transformation function ([Carpendale and Montagnese, 2001](#)).

[Leung and Apperley \(1994\)](#) presented a thorough review of focus + context techniques. In this review they divided transformation functions into two categories: *step functions* and *continuous transformation functions*. They define step functions as functions, which change the values discontinuously from one constant to the next, causing discrete levels of magnification and continuous transformation functions as functions, which scale the values in a continuous manner, causing smooth magnification. Continuous transformation functions will be discussed in suppression techniques. The step magnification function can be constant (as in

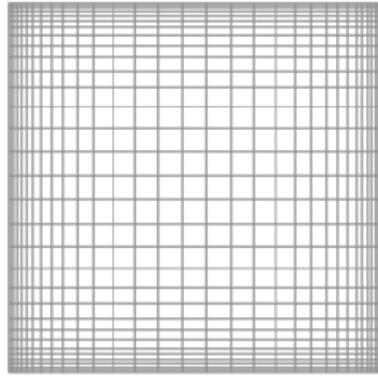
the one-dimensional bifocal view (Spence and Apperley, 1982)) or varying (such as the perspective wall (Mackinlay et al., 1991)). The bifocal lenses have only magnified or unmagnified areas; the perspective wall creates the illusion of three-dimensional perspective by applying varying degrees of magnification to the data not in focus. These distortion principles have been extended in the Document Lens (Robertson and Mackinlay, 1993) and the Table Lens (Rao and Card, 1994).

Suppression Techniques

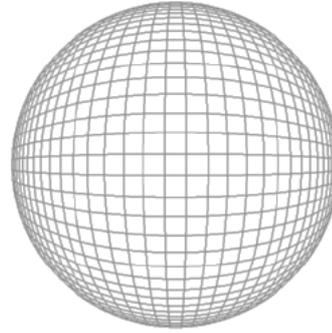
Suppression techniques are built on the idea that not all the information in the information space is interesting for the user and can thus be suppressed from the view (Furnas, 1986; Leung and Apperley, 1994). The most famous technique in this category is the fisheye technique suggested by Furnas (1986). According to Furnas (1986) it is often practical to show data only if its perceived value exceeds some threshold set by the user. He introduces the *degree of interest* (DOI) function which calculates the perceived value. For example, the perceived value could be calculated as a factor of the distance of the item from the current viewpoint. As a consequence of applying the DOI function, items that have perceived values above the threshold are shown in the view while items with values below the threshold are suppressed from the view. In complex situations the DOI function would be composed of a presupposed (*a priori*) component, the general interest of the object, and an observed (*a posteriori*) component, the distance of the object from the current viewpoint. For example, in map applications this would mean that larger cities with high general interest that are far away from the current viewpoint would more likely be shown than small cities with low general interest.

Card et al. (1999) and Skopik (2004) suggest that by highlighting or distortion they can perform a selective reduction of information for the contextual area. Instead of removing the objects from the view, only the objects of interest could be highlighted or the view could be distorted so that only the objects near the points of interest are visible in detail.

Sarkar and Brown (1992) first developed the mathematics to apply the in-



(a) Fisheye transformation function applied to x and y coordinates independently. Adapted from [Sarkar and Brown \(1992\)](#) and produced by the InfoVis CyberInfrastructure ([InfoVis, 2004](#)).



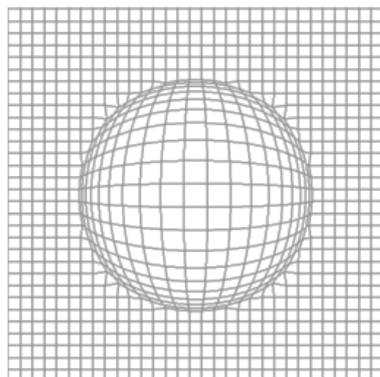
(b) Fisheye transformation function applied radially to polar coordinates. Adapted from [Keahey \(1998\)](#) and produced by the InfoVis CyberInfrastructure ([InfoVis, 2004](#)).

Figure 6.1: The magnification function in different coordinate systems.

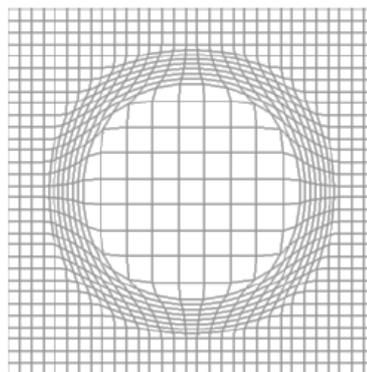
place magnification concept to 2D spatial coordinates. They added Furnas' ideas of DOI to provide both a method for information suppression and enhancement. Most of these graphical fisheyes are interactive, with the focus typically following the cursor to provide the maximum magnification at the point of user interaction.

The magnification function has different presentations on different coordinate systems. For example, the magnification function can be applied to the Euclidian x and y coordinates independently ([Sarkar and Brown, 1992](#)) (Figure 6.1(a)), or to the Euclidian polar coordinates ([Keahey, 1998](#)) (Figure 6.1(b)). Furthermore, the magnification function can be applied to a two-dimensional 2D space or a three-dimensional one ([Carpendale et al., 1997](#)) or the calculations may be done in three dimensions and then mapped back to a two-dimensional representation ([Carpendale, 1999](#)).

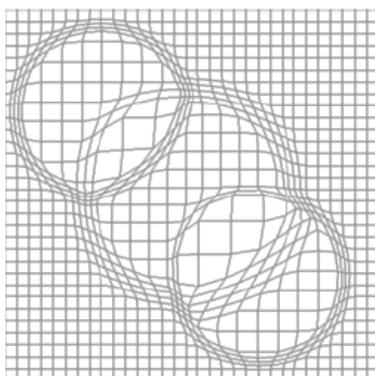
In most suppression techniques (for examples see [Furnas \(1986\)](#), [Lamping et al. \(1995\)](#), [Robertson and Mackinlay \(1993\)](#), [Rao and Card \(1994\)](#)), the technique is applied to the entire data space, but [Keahey \(1998\)](#) presented the magnification functions that can be constrained to part of the space (Figure 6.2(a)). The magnification functions can be either linear or non-linear and sometimes both can be combined, thus that the area in focus is shown at a constant magnification, while the surroundings are shown with a non-linear magnification (Figure 6.2(b)).



(a) Constrained fisheye transformation. Adapted from [Keahey \(1998\)](#).



(b) A truncated fisheye lens. Adapted from [Keahey \(1998\)](#).



(c) Multiple foci. Adapted from [Greenberg et al. \(1996\)](#).

Figure 6.2: A few fisheye transformations produced by EPF toolkit ([Carpendale, 2004](#)).

This truncated fisheye has the advantage of not distorting the area of focus, while preserving the non-occluding view of the context. The fisheye transformation can also be applied to multiple foci, with the magnification transformations interacting in a predetermined way. This can be especially useful in groupware applications, where each participant has their own fisheye lens ([Greenberg et al., 1996](#)) (see [Figure 6.2\(c\)](#)).

Existing presentation methods create displays that vary considerably visually and algorithmically. [Carpendale \(1999\)](#) presented a framework, “Elastic Presentation Space” or EPS library that encompasses the presentation distortion dimension as defined earlier in this section and the other presentations introduced in the literature of the detail in context. It facilitates the inclusion of more than one presentation method in a single interface, and supports extrapolation

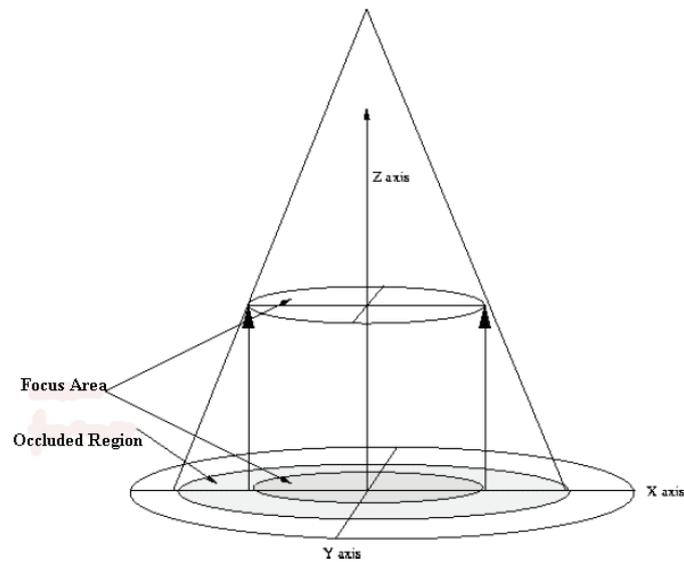


Figure 6.3: Carpendale’s EPS library uses a three-dimensional projection of a two-dimensional image. From [Carpendale \(1999\)](#).

between the presentation methods it describes.

Carpendale’s display surface distortion technique visualises the display space as a three dimensional space in which a two dimensional display can be flexibly projected. As shown in Figure 6.3, the focus area of the display is raised along the z -axis to magnify it. The context remains on the plane at the origin of the z -axis. To avoid occluding the shaded region of the context, the context can be distorted in various ways using a “drop-off” function. Drop-off functions are polynomial curves that are used to raise points on a base image to various heights depending on their distance from the focus location. Basically, they take the context and gradually distort it into the focus, allowing smooth embedding of the focus into the context ([Carpendale, 1999](#)).

Despite fisheye views being a long-established visualisation technique, they have not been widely used. The Macintosh OS X “dock” ([Apple, 2002](#)) is one of main examples of fisheye use in business applications.

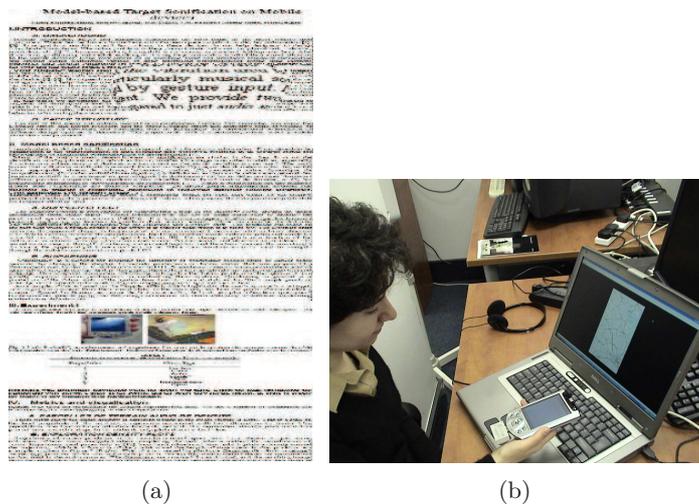


Figure 6.4: (a) A document representation in Elastic Presentation Framework, (b) Communication between the PDA and the laptop via BlueTooth

6.2.2 Why have Focus in Context methods not been widely accepted?

Distortion-oriented techniques are inherently complicated in their implementation, and some require a significant amount of system time to generate a new image (known as rendering time). While an excessively long system response time would render an interface “unusable,” this problem may be overcome by using dedicated computer hardware and memory management systems to support the implementation of such techniques (Card et al., 1999). Further, as general-purpose graphics hardware becomes increasingly sophisticated and powerful, effective software solutions have become practicable (Robertson and Mackinlay, 1993).

Leung and Apperley (1994) argue that the basic law governing distortion-oriented techniques is a corollary of Newton’s third law of motion, stating that “where there is a magnification, there will be an equal amount of demagnification to compensate for the loss of display area in a confined space; otherwise the area of that confined space will change.” and a general discomfort with the use of distortion and/or to the perception that the use of distortion and non-distortion based presentation methods are raised by this issue (Carpendale, 1999). For instance, comments have been made:

It is all very well to use a fisheye distortion to locate the details I am interested in, but when I find them I don't want all the space wasted for context.

or

I'm happy with insets but sometimes they get in the way of seeing connections.

The outcome of different presentation methods depends on the type of task, the nature of the information, and the preferences, skills of the person using it and tasks. Thus it is not easy having a general purpose focus-in-context method unless we bring some *intelligence* to it.

Some specific usability problems with fisheyes, such as targeting (Gutwin, 2002), have been identified. In particular moving and positioning the pointer relative to the global context can be difficult, because the magnified data appear to move in the opposite direction of the moving focus point (Gutwin, 2002; Gutwin and Skopik, 2003). For example, with a $2\times$ magnifying lens, moving the lens by one centimeter will cause the image in the magnifier to move two centimeters, in the opposite direction to the lens's movement (Figure 6.5). This happens because of magnification. However, due to the non-linear transformation function of the fisheye lens the magnification and the movement increase as the focus gets closer to the target. As a result, targets move towards the focus more and more rapidly as the focus approaches them (Gutwin, 2002). Even though an object also appears to become larger the closer it gets to the lens's focus, its motion makes acquisition of the target more difficult. A solution for this problem has been suggested in (Gutwin, 2002) but little research has been done on the effectiveness of the fisheye views in real applications.

6.2.3 Applications of Focus in Context Methods on Small Screen Devices

Small memory space and poor graphics cards cause long rendering time on handheld devices and as discussed earlier, a long system response time would



Figure 6.5: Motion effect of magnification: as the magnifier moves upwards, the magnified image moves down. From [Gutwin \(2002\)](#).

make the interface “unusable,” thus not many focus-in-context applications have been implemented and tested on these devices.

[Holmquist et al. \(1999\)](#) demonstrated the “flip zoom” technique embodied in a palmtop display, to function as a Web browser (The Zoom Browser). Users navigated through a data set by flipping between the individual pieces, just like flipping among pages in a book. When an entry is to be examined in detail, it is selected by clicking on the representation of the item. This zoomed the image of the item to a readable size, and the surrounding items are reduced in size and rearranged to accommodate the expanded focus image. The main advantage with this technique was that the computational demand of the graphics was quite low which, at the time, was very important. The main problem was the scalability. When viewing a large number of pages, the thumbnails got very small they could not show any useful information.

[Rauschenbach \(2002\)](#) presented the “Rectangular FishEye View” as a solution for the problem of screen space on mobile devices. He rendered the user’s point of view (the focus) at high detail, and downscaled the surrounding context to save display space. He implemented this idea on a Siemens tablet computer.

In 2003, [Bederson et al. \(2003\)](#) published an article on a ZUI for calendars in PDAs. They implemented a zoomable calendar for the Pocket PC called the DateLens. Their studies showed that a ZUI can be very useful when trying to access a large amount of information, and accessing data deeper in the dataset at the same time as keeping an overview. Later, in 2003, [Karstens et al. \(2003\)](#) proposed a technique to visualise hierarchical structures on mobile devices. They adapted the “magic eye view,” and integrated the interaction paradigm “event

horizon” and discussed concepts for browsing the Web via handhelds.

Baudisch et al. (2004) introduced “Fishnet,” a web browser that always displays web pages in their entirety, independent of their size on small screen devices. Fishnet accomplishes this by using a fisheye views, i.e., by showing a focus region at readable scale while spatially compressing page content above and below that region.

In 2004, Lank and Phan (2004) presented the first fisheye lens for sketching data on a Pocket PC using Elastic Presentation framework (Carpendale and Montagnese, 2001). This technique allowed users to sketch in a high-resolution focus area, while still seeing the focus area in context with the rest of the drawing. To prevent long rendering time they pre-computed the distortion matrix off-line and added the distortion values to points to get an acceptable frame-rate.

Heimonen (2002) introduced and evaluated a number of information visualisation techniques as solutions to the presentation problem on handheld devices, as well as devices on which the techniques could be used. The framework presented in this work drew together the visualisation techniques and devices by comparing their corresponding properties for the first time for mobile phones and handheld computers and found out that only one third of the proposed solutions are suitable for use on mobile phones. The situation is reversed in the context of high-end display devices (handheld computers). In their case only one third of the techniques are found unsuitable for use.

Gutwin and Fedak (2004) compared three techniques for using large interfaces on small screens: a panning system similar to what is in current use, a two-level zoom system, and a fisheye views. They found that people were able to carry out a web navigation task significantly faster with the fisheye views, that the two-level zoom was significantly better for a monitoring task, and that people were slowest with the panning system. However, their real experiments were never conducted on a handheld and they just employed a small monitor connected to a normal PC running Windows XP.

6.3 Model-Based Fisheye Views

We developed a document viewer using FMOD API (version 3.70CE) (FMOD, 2004), a visual programming environment with object-oriented language (Visual Studio) and Carpendale’s Focus+Context framework (EPF (Carpendale, 2004)) for Open GL presentation of the fisheye lens to browse a PDF, PS or DOC file which has been converted to an image (Bitmap file). FMOD API and EPF toolkit are available for free under the condition of the GNU General Public License (GPL). Our initial development was on a Pocket PC. The result was not convincing due to the rendering time problem caused by slow CPU, low memory capacity and poor graphics card quality on PDAs. Thus we developed the focus-in-context technique on a laptop (Latitude D800 Dell Laptop with 1600×1200 pixels resolution running windows XP) and reduced the application’s window size to the size of PDA’s screen (320×240 pixels). We controlled the interaction via mouse or Xsens P3C, 3 degree-of-freedom linear accelerometer attached to the serial port of an HP 5550 Pocket PC and communicating via Bluetooth with the laptop (Figure 6.4).¹ The focus area is embedded in a movable frame that can be panned around the screen when moving the mouse or tilting the PDA. The context information, computed using the EPF framework, is preserved around this focus area with some compression in spatial resolution. Several visualisations are supported by the EPF toolkit for embedding focus into context. These visualisations employ “drop-off” functions to embed the focus area into the context area. In our application, a Gaussian dropoff function is used to distort the context around our focus window. The Gaussian drop-off function blends smoothly the focus into the distortion and the distortion into the context. We felt a smooth transition was important to avoid discontinuity in the visual effect being presented to the user. Figure 6.6 shows a focus region embedded into a context using the Gaussian drop-off function.

¹The author of this dissertation has programmed and coded all the developed applications in Chapter 6 (See Appendix D). The language model module (Section 6.5 on page 193) is written by Williamson (2006) and has been imported in this application by his permission.

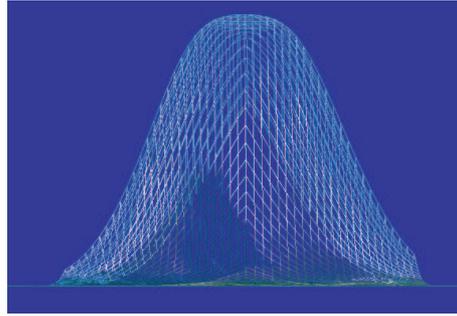


Figure 6.6: The fisheye lens with Gaussian drop-off function.

6.3.1 Design

Similar to the SDAZ, the use of state-space modeling is a well-established way of presenting a dynamic system like fisheye views as a set of first-order differential equations. It will allow us to model the internal dynamics of the fisheye views, as well as the overall input/output relationship as in transfer functions, thus this method is an obvious candidate for the representation of the coupling between the user's speed with degree of magnification in this visualisation method. The rest of this section will present a state-space model to couple the user's motion with the distortion-level, and a method for tuning components of fisheye views in the state-space.

6.3.2 Coupling between velocity and Degree-of-Magnification

Speed-Coupled Flattening (SCF)

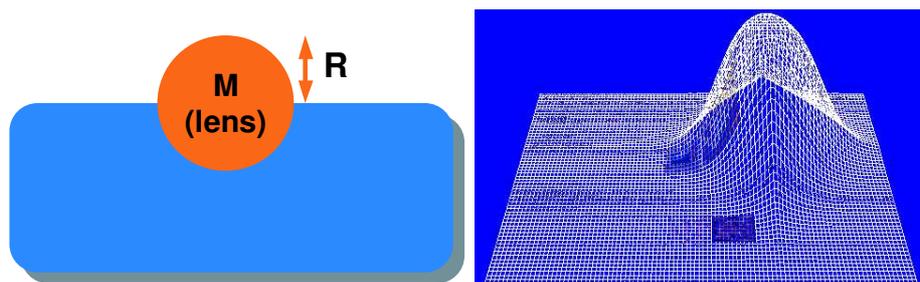
If distortion does in fact hinder targeting, then reducing distortion during targeting can reduce the problem. There are several possible ways to do this: for example, by having the user press a mouse or keyboard button to reduce distortion, or by using a dedicated control (such as the mouse wheel) to change distortion level (Gutwin, 2002). However, these solutions force users to learn and manipulate additional interface controls to carry out a very frequent task, and may also clash with existing assignments of buttons or other controls in the application. An alternate approach that does not require any extra effort on the users' part is to automatically recognise when the user is engaged in targeting, based on the motion of their pointer. This is speed-coupled flattening

(SCF) (Gutwin, 2002). The technique uses the pointer's velocity and acceleration to recognise that a targeting action is happening. The underlying idea is that when the focus is moving quickly, or is accelerating, then the user is much more likely to be navigating to a new focus point than to be inspecting details in the data. This approach is similar to tilt-controlled SDAZ, flying object (refer to Section 5.3.2 on page 111), which coupled speed to height during flight through a virtual landscape, allowing the user to get a better idea of the terrain when navigating at higher velocity.

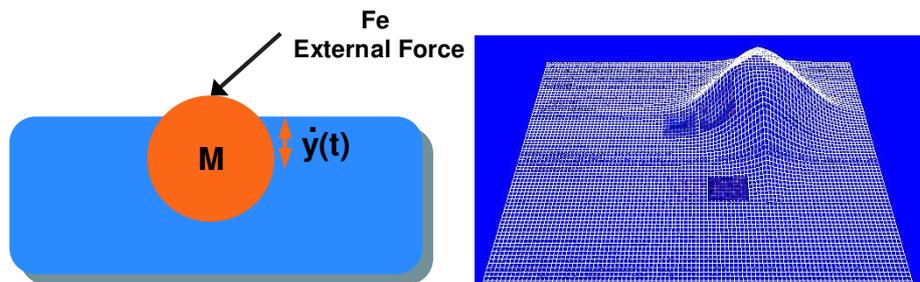
Speed-coupled flattening is designed with the following goals in mind (Gutwin, 2002):

- Any major changes to the view should occur during the motion phase of targeting, while the user is still far away from the target;
- the view should remain relatively static during the acquisition phase of targeting, in order to simplify precise positioning;
- the changes to the view should be smooth enough that the target is easy to track during the motion phase; and
- the distortion level should be restored smoothly after targeting is complete.

Focus+context views would be more useful if they could adjust the support given for focus tasks and context tasks, rather than being stuck at one point on the continuum. This adaptability could be achieved by giving the user greater control over the visualisation; however, the example of speed-coupled flattening shows that it may also be possible for systems to adjust themselves automatically to the user's current activity. Furthermore, this suggests that an interface can shift the balance of support towards one type of task over another, based on easily-obtainable user evidence, and make a significant difference in performance. With adaptive techniques like speed-coupled flattening, the goal is to give users the benefits of both sides of the tradeoff. For example, SCF could allow users to choose a higher initial distortion level to maximise the amount of space devoted to the focus region, without suffering the ill effects of attempting to navigate



(a) (Left) A floating ball in the water. (Right) A fully magnified fisheye lens.



(b) (Left) The ball after applying external force and pushing it down in the water. (Right) The DOM decreases as soon as the user starts to scroll.

Figure 6.7: Interpreting Fisheye Lens as a floating ball.

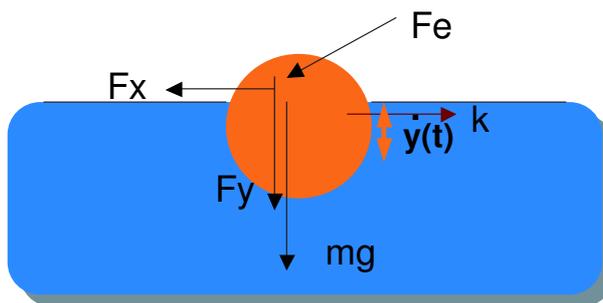


Figure 6.8: Applied forces to the floating ball.

at high magnification. In continue we investigate how a dynamic model for a fisheye lens can support the user behaviour and adapt itself to different contexts without any additional user input or any additional view controls using state-space approach.

Pseudo Physical Simulation

As our integrated system benefits from Elastic Presentation Framework (EPF), the presentation has an elastic nature. Elastic is a positive word that implies adjusting shape in a resilient manner. That is, elastic materials can al-

ways revert to their original shape with ease. Figure 6.7 illustrates a conceptual model (refer to Section 1.3 on page 7), a floating elastic ball in the water, for a fisheye lens. Thus in this analogy, changes in the height of the centre of the ball outside the water, $y(t)$, adjusts the degree of magnification (DOM) and is function of time $\dot{y}(t)$. If we show the radius of the ball with R (maximum DOM), then

$$DOM(t) = R - \dot{y}(t) \quad (6.1)$$

When we apply an external force, f_e , we push the ball down in the water (not more than its radius) thus the DOM decreases and when we release the force the DOM starts to increase (not more than its radius, see Figure 6.7). Thus the DOM is a variable which is continuously controlled by external force (mouse or tilting angles) and speed of movement. From Newton's second law of motion we can write the equation in the vertical direction:

$$m\ddot{y}(t) = f_y - k\dot{y}(t) \quad (6.2)$$

k is the damping factor caused by water resistance, and the effect of gravity and the weight of the ball is negligible. In the horizontal direction we can write:

$$\begin{aligned} ma &= f_x - kv & \text{or} \\ a &= \frac{f_x}{m} - \frac{k}{m}v \end{aligned} \quad (6.3)$$

v and a represent velocity and acceleration and k is the damping factor caused by water resistance.

We may assume f_x is a function of f_y and velocity as below:

$$f_y = cf_x - bv \quad (6.4)$$

Where b is a coefficient and c is a scaler. This assumption will couple rate of changes in the DOM to speed of movement as well as input, e.g., in higher speed the distortion level, i.e., the focus area, increases and vice versa (See Figure 6.3).

After substituting f_y in (6.2) we can rewrite it as below:

$$\ddot{y}(t) = \frac{c}{m}f_x - \frac{b}{m}v - \frac{k}{m}\dot{y}(t) \quad (6.5)$$

Viscous Damping in Control

Viscous damping feels like moving a spoon through thick syrup. Running through water deep enough to cover the thighs is another example. The rate of movement is directly proportional to the force exerted (Poulton, 1974). A similar analogy to that of friction in Section 5.3.2 can be applied to viscous damping. To prevent accidental operation while the user is tracking in a vibrating vehicle we may use different viscous damping in vertical and horizontal directions; k for horizontal direction and k' for vertical direction. Then the equation (6.5) can be rewritten as below:

$$\ddot{y}(t) = \frac{c}{m}f_x - \frac{b}{m}v - \frac{k'}{m}\dot{y}(t) \quad (6.6)$$

If we introduce x as position then velocity and acceleration will be first and second derivatives of the position respectively. The chosen state variables are $x_1(t)$ as position of cursor, $x_2(t)$ as velocity, $x_3(t)$ as rate of change of the DOM and u as f_x . Thus state variables can be written as below:

$$\dot{x}_1(t) = v = x_2(t) \quad (6.7)$$

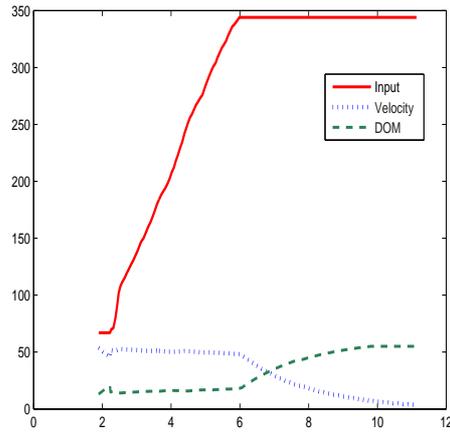
$$\dot{x}_2(t) = a = \dot{v} = \frac{-k}{m}x_2(t) + \frac{u(t)}{m} \quad (6.8)$$

$$\dot{x}_3(t) = \ddot{y}(t) = \frac{-b}{m}x_2(t) + \frac{-k'}{m}x_3(t) + \frac{c}{m}u(t) \quad (6.9)$$

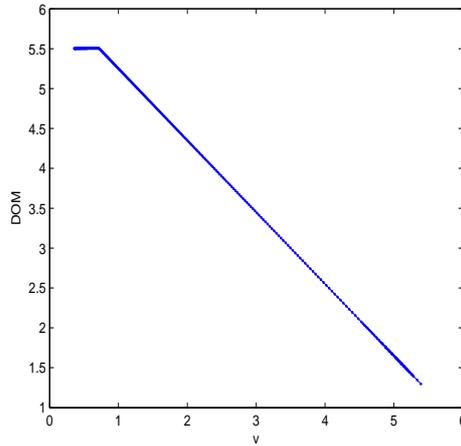
The standard matrix format of these equations is:

$$\begin{pmatrix} \dot{x}_1 \\ \dot{x}_2 \\ \dot{x}_3 \end{pmatrix} = \begin{pmatrix} 0 & 1 & 0 \\ 0 & \frac{-k}{m} & 0 \\ 0 & \frac{-b}{m} & \frac{k'}{m} \end{pmatrix} \begin{pmatrix} x_1 \\ x_2 \\ x_3 \end{pmatrix} + \begin{pmatrix} 0 \\ \frac{1}{m} \\ \frac{c}{m} \end{pmatrix} u \quad (6.10)$$

This shows how a single-degree of freedom input can control both velocity and degree of magnification. The next step is finding suitable values for k , m , b and



(a) Plots of step input, velocity and DOM of the implemented fisheye model.



(b) DOM vs. Velocity in the implemented fisheye model.

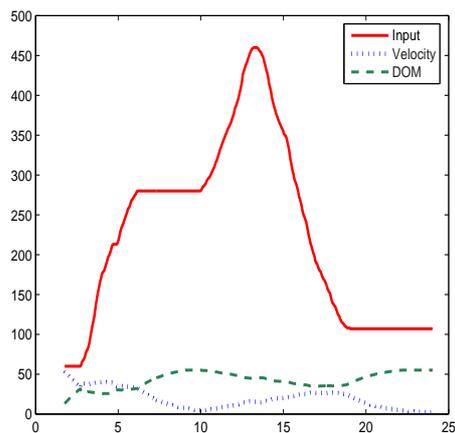
Figure 6.9: Behaviour of fisheye model to a step input in an implemented model ($m = 10 \text{ kg}$, $k = 10 \text{ kgs}^{-1}$, $k' = 10 \text{ kgs}^{-1}$, $b = 1 \text{ kgs}^{-1}$ and $c = 3$).

c coefficients in the state-space model to make the system controllable (refer to Section 3.2.9 on page 45). We can write the controllability matrix as below:

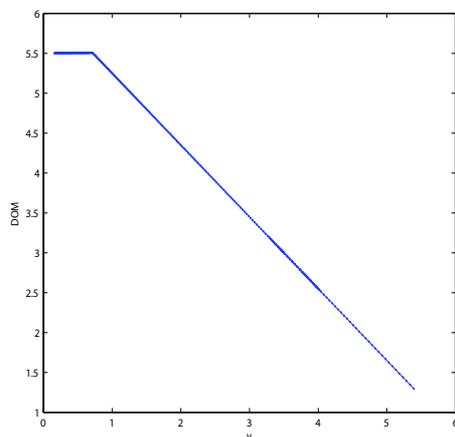
$$\text{rank}[B|AB|A^2B] = \text{rank} \begin{pmatrix} 0 & \frac{1}{m} & \frac{-k}{m^2} \\ \frac{1}{m} & \frac{-k}{m^2} & \frac{k^2}{m^3} \\ \frac{c}{m} & \frac{-b-k'c}{m^2} & \frac{bk+bk'+ck'^2}{m^3} \end{pmatrix} \quad (6.11)$$

which has a full rank for all k , k' , $m \neq 0$, $b \neq 0$ and c .

As an example we set the coefficients $m = 10 \text{ kg}$, $k = 10 \text{ kgs}^{-1}$, $k' =$



(a) Plots of step input, velocity and DOM of the implemented fisheye model.



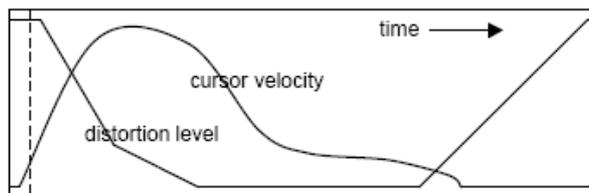
(b) DOM vs. Velocity in the implemented fisheye model.

Figure 6.10: Behaviour of fisheye model to different step inputs in the implemented model ($m = 10 \text{ kg}$, $k = 10 \text{ kgs}^{-1}$, $k' = 10 \text{ kgs}^{-1}$, $b = 1 \text{ kgs}^{-1}$ and $c = 3$).

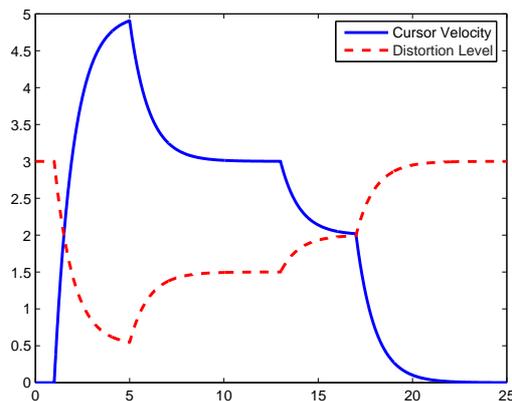
10 kgs^{-1} , $b = 1 \text{ kgs}^{-1}$ and $c = 3$ to check the system's behaviour to different input signals in real environment. Figure 6.9 presents the time domain response of the implemented system to a step input², which means scrolling down on a document and staying in a certain speed by moving mouse and stopping over a figure. The relationship between the velocity and DOM is linear indicating the system's behaviour is linear and slope of the line is almost -1.

Figure 6.10 presents the time domain response of the implemented system

²To solve the first-order differential equations in the developed application, Taylor's method was implemented in VC++ with sampling time 10 ms (Polyanin and Zaitsev, 2003).



(a) Speed-coupled flattening developed by Gutwin (2002).



(b) Distortion level is controlled by cursor velocity in the state-space model.

Figure 6.11: (a) Gutwin’s SCF (Gutwin, 2002) where in this method distortion level remains relatively static during the acquisition phase of the targeting. (b) The state-space approach allows the user to examine the detail smoothly by changing the speed before the actual targeting phase, which has happened around time = 17 seconds. Cursor velocity and distortion level are measured in pixels per second.

to a varying step inputs, which means scrolling down on a document, staying in a certain speed, landing on a figure and scrolling up by tilting the device. Despite changes in sign of the input data, the relationship between velocity and DOM remains linear. The relationship between velocity and DOM can also be nonlinear which is discussed in the next section.

Nonlinear Model

In the speed-coupled flattening the speed as a function of control input (mouse displacement, or tilt angle, depending on platform) can be linear, piecewise linear or nonlinear functions. The general state-space equations in (4.3) can be written in a nonlinear form where functions linking DOM to velocity or vice versa and functions mapping viscous damping to the DOM and velocity can be

nonlinear dynamic functions:

$$\dot{x}(t) = v \tag{6.12}$$

$$\dot{v}(t) = a = \frac{-k(v, \dot{y})}{m}v(t) + f_{v, \dot{y}}(\dot{y}) + \frac{1}{m}u(t) \tag{6.13}$$

$$\ddot{y}(t) = \frac{-k'(v, \dot{y})}{m}\dot{y}(t) + f_{\dot{y}, v}(v, \dot{v}) + \frac{c}{m}u(t) \tag{6.14}$$

Where $f_{v, \dot{y}}(\dot{y})$ and $f_{\dot{y}, v}(v, \dot{v})$ are nonlinear functions. Viscous damping, $k(v, \dot{y})$ and $k'(v, \dot{y})$, can also be nonlinear functions of velocity. In the next section, tuning parameters and calibration will be discussed.

6.3.3 Calibration and State-Space Approach

Similar to SDAZ the state-space model for the fisheye lens has many parameters that can be tuned. Multiple variables, and derivative effects (e.g., position, velocity) are coupled to the DOM, without any further coding, by just changing the entries of the A matrix, simulating combinations of springs, masses and damping effects.

To enhance the smoothness of the transition between the magnification and the zooming out after a sudden change happens in y direction when the mouse starts to scroll, we just need a straightforward switch to a particular parameterisations of the A matrix, which can be tuned to give an appropriate exponential decay in the DOM. This prevents the targeting problem (Gutwin, 2002) in focus-in-context techniques and has been illustrated in Figure 6.11. This figure compares Gutwin's speed-coupled flattening (SCF) technique with the state-space model. Related problems include rapid magnification and zooming out when making a rapid change of the direction.

In the state-space representation, our basic assumption is that DOM should lead speed when speed increases, in order to avoid extreme visual flow. DOM should, however, lag speed when $|v|$ decreases, to allow the user to slow down but still maintain the context overview while searching for a target, or magnifying the goal. This also allows, for example, the user to reduce the magnification level, without changing position in the document, by repeated positive and negative

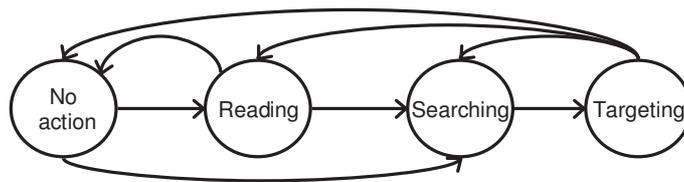


Figure 6.12: Four states of control mode in text-browsing example and transitions among them.

acceleration, which allows the reduction in the DOM be integrated up.

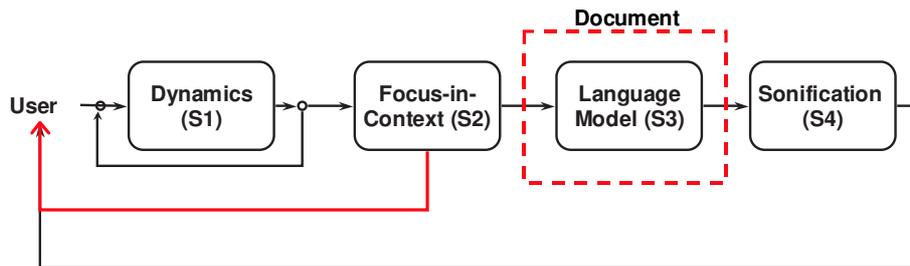
In order to move more rapidly through the document at low levels of distortion, here, we adapted B by making c in equation (6.9) a function of velocity. When the speed is above a threshold (here we call it speed threshold and set it to 0.2), $c = 3$ but below this threshold $c = 0$. We wish to avoid rapid magnifications when the user changes direction. To achieve this, we change c to be $-0.9 \times c$, when the sign of velocity and input differ.

We include saturation terms for maximum and minimum distortion levels, and there can be specific rules for behaviour at the limits associated with the start and end of the document. For example, if the user is already at the beginning of the document and s/he scrolls up it won't be taken into account by the controller. DOM has a maximum level, too which means the context cannot be magnified till infinite level.

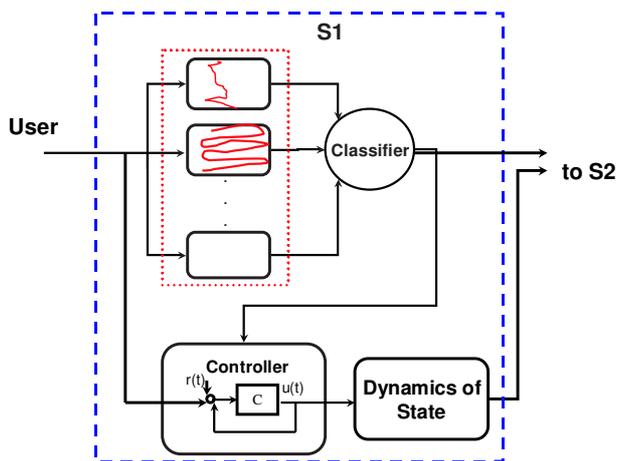
The dynamic model for fisheye information presentation technique that was studied in this section provides a few control modes and user/system behaviours that detecting them can facilitate the automatic switching and smooth transitions among different behaviours.

6.4 User Behavioural Model

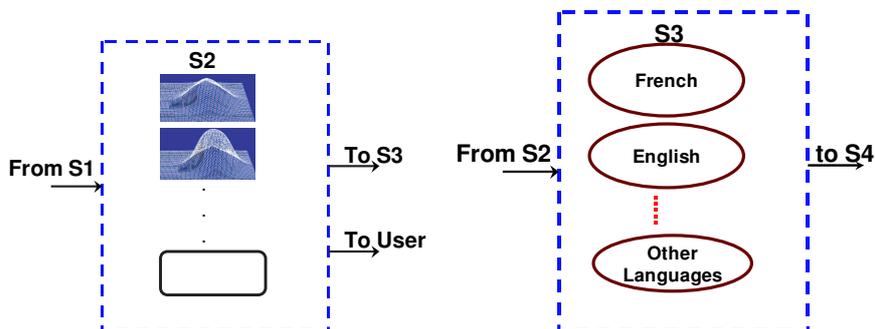
Similar to Chapter 5 in this application we have a single controller and here, we introduce a switching method and transitions among different browsing behaviours which alter the dynamics and the way the user's inputs are interpreted.



(a)

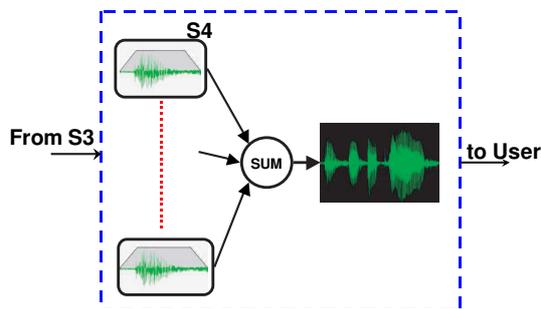


(b)



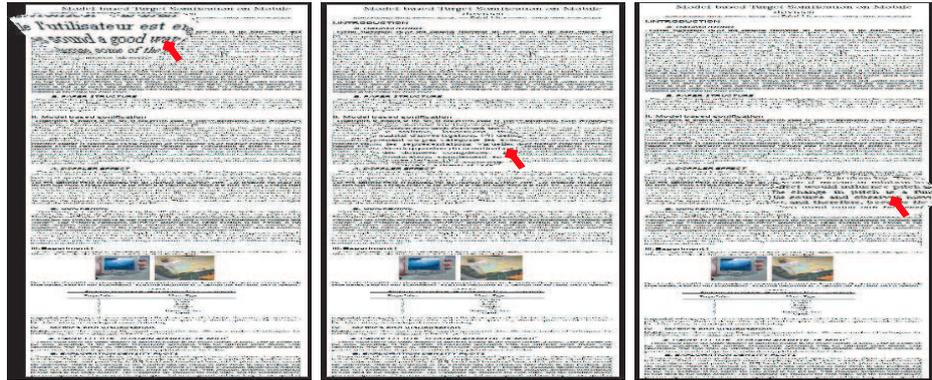
(c)

(d)

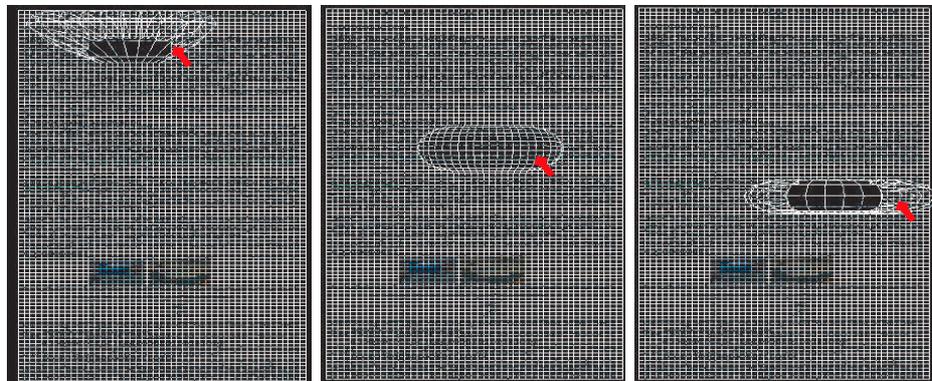


(e)

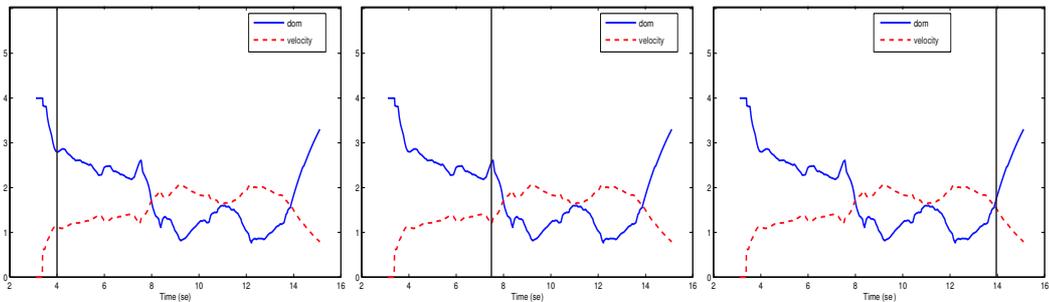
Figure 6.13: (a) A general probabilistic framework of the model-based behaviour system. (b) A Bayesian classifier classifies the user's input. Its output and the user's input come to the controller and change the dynamics (state variables). (c) State variables coupled to the focus-in-context change the size and shape of lens. (d),(e) Language identification method infers the most probable language inside the window around the lens and its output probabilities are fed to the audio synthesis algorithm.



(a) Searching and targeting behaviour in the text browser.



(b) Searching and targeting view behind the texture.



(c) Plots of velocity and DOM of the implemented fisheye model. From left to right it shows the transition happening from the searching mode to the targeting mode in the example provided in top figures ($m = 10 \text{ kg}$, $k = 10 \text{ kgs}^{-1}$, $k' = 10 \text{ kgs}^{-1}$, $b = 1 \text{ kgs}^{-1}$ and $c = 3$).

Figure 6.14: Visualising the user behaviour and mode transitions in the text browser example. (Left) The changes in y direction are more than height of the line, e.g., 12 pixels. Thus it means for the system the user has started the searching mode. In this mode speed of browsing starts to increase and the DOM decreases gradually. (Middle) The user examines the details smoothly by decreasing the speed and increasing the DOM. (Right) The user has found the target and gradually changes the speed and stops over that and the lens starts to grow.

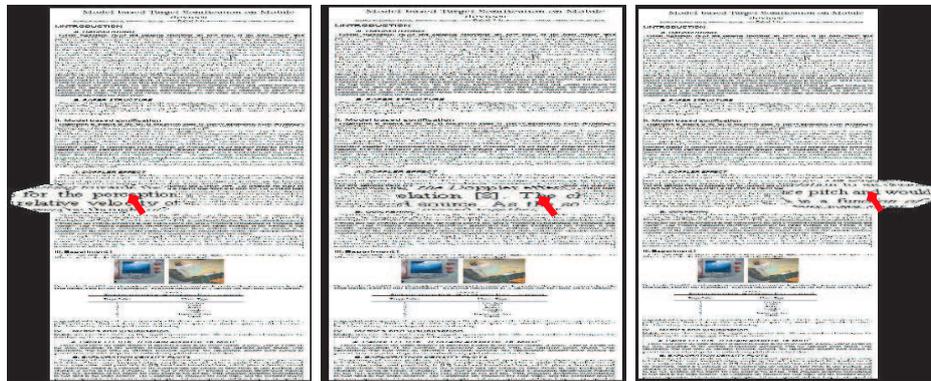
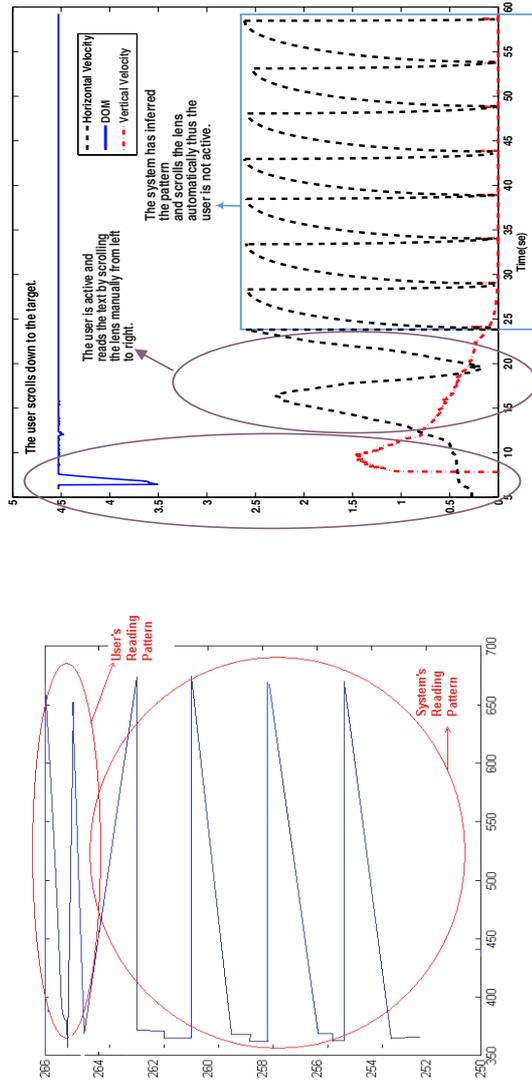


Figure 6.15: Visualising the user and the system behaviour in the reading mode. The user has found the target and started to scroll the lens from left to right (continuously increasing changes in the x direction). In the end of the line the user moves to the next line (a small change in the y direction). Later, this pattern is inferred and continued by the system unless a major change in y direction happens.



(a) The reading trajectory made by the user and the system. (top) The reading pattern starts by the user when he scrolls the lens from left to right and makes small changes in the y direction. (bottom) The system has recognised the pattern and completes the task by scrolling the lens in the x direction following the user's desired speed.

(b) Plots of the velocity in both x and y directions and the DOM of the implemented fisheye model in the reading mode. When the system starts the reading mode, the lens has the highest DOM and remains steady during this mode. Speed of scroll in the y direction only changes to a non-zero value when the lens moves to the next line and the speed in the x direction goes to zero end of each of line and increases gradually in the next line ($m = 10 \text{ kg}$, $k = 10 \text{ kg s}^{-1}$, $k' = 10 \text{ kg s}^{-1}$, $b = 1 \text{ kg s}^{-1}$ and $c = 3$).

Figure 6.16: The reading trajectory and time-series of the velocity and the DOM in task presented in Figure 6.15.

6.4.1 Behaviours in Text Browsing Application

In the model-based text browser example, the user's input, mouse data, controls what s/he perceives via visual/audio/haptic display. In this example we assume the user is acting in one of four different modes: *no-action*, *reading*, *searching* and *targeting*.

Figure 6.13 illustrates the general framework. Figure 6.13(b) shows the classification of the user behaviour being used to switch the control mode. This mode is then coupled to the visualisation parameters, as shown in Figure 6.13(c), where the control mode changes the size and shape of the lens, and the controller provides the DOM, position and speed of the lens. For example, in the reading mode the controller adjusts the DOM to stay in the maximum level, but as a long horizontal lens, while if the user 'breaks out' into general searching, the DOM is decreased smoothly to a lower level. This prevents the targeting problem (Gutwin, 2002) in focus-in-context techniques.

6.4.2 Detecting state transitions

Figure 6.12 illustrates the possible state transitions. Initially, the user is in the no-action state. Depending on the input behaviour, the user can either go to the reading or the searching mode. A qualitative description of the automatic mode transitions is given below: In the reading mode, the user is making continuous increasing changes in x direction (left-to-right) and small changes in y direction (not more than height of a line) and at the end of the line makes a sudden change from right-to-left in x direction. If the changes in y direction are more than height of the line the system switches the mode to the searching mode. After finding the target, the user slows down or stops scrolling until the lens is over the target point (targeting mode), or can return to the no-action mode directly (see Figures 6.14, 6.15 and 6.16).

A general technique for implementing this is to use a probabilistic classification of the likelihood of being in one of these four browsing behaviours according to the joint probability of the input and output time-series. From Bayes' law, we

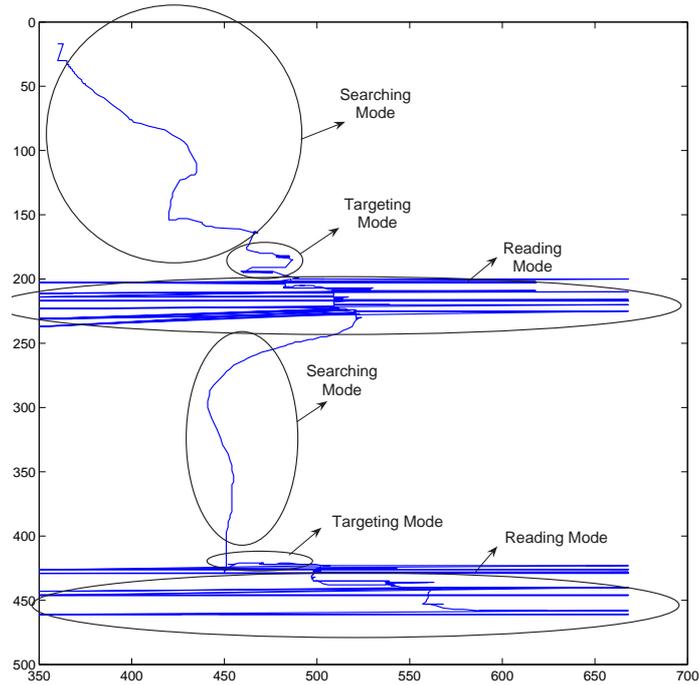


Figure 6.17: The user's trace in the text browser example. The user starts the scrolling from top-left corner (beginning of the document) and scrolls down. The searching behaviour becomes targeting and then reading behaviour. The French paragraph is at $y=185$ pixel. From the beginning of the document until $y=180$ pixel the user is in the searching mode, listening to the blurred audio samples. Around $y=190$ pixel the user hears a blip sound (representing the French language) and slows down the scrolling therefore the system switches to the targeting mode and the lens gradually grows. As the user is tending to read the text the controller automatically has scrolled the lens over the text in x direction. This action has been repeated for the next French paragraph around $y=420$ pixel.

write this as below:

$$P(\text{Mode} | X) = \frac{P(\text{Mode})P(X | \text{Mode})}{P(X)} \quad (6.15)$$

where X is an appropriate window of previous inputs and possibly also outputs. $P(X | \text{Mode})$ can be identified from experimental data collected from test users using standard density estimation models.

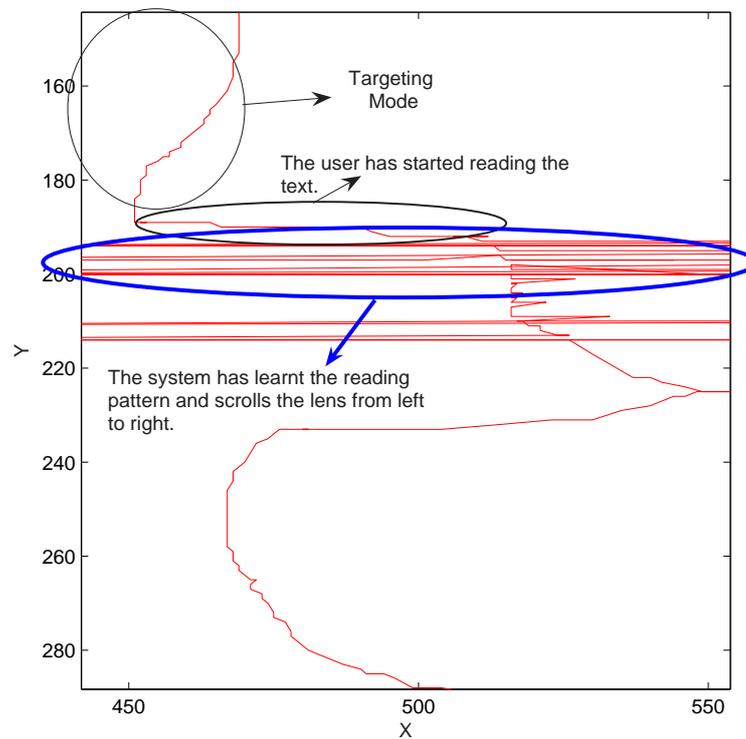


Figure 6.18: Changing from the targeting mode to the reading mode has been highlighted in this figure. For very few milliseconds the user has scrolled from left to right and that is enough for the classifier to infer that the user is in the reading mode. Then the controller automatically scrolls the lens.

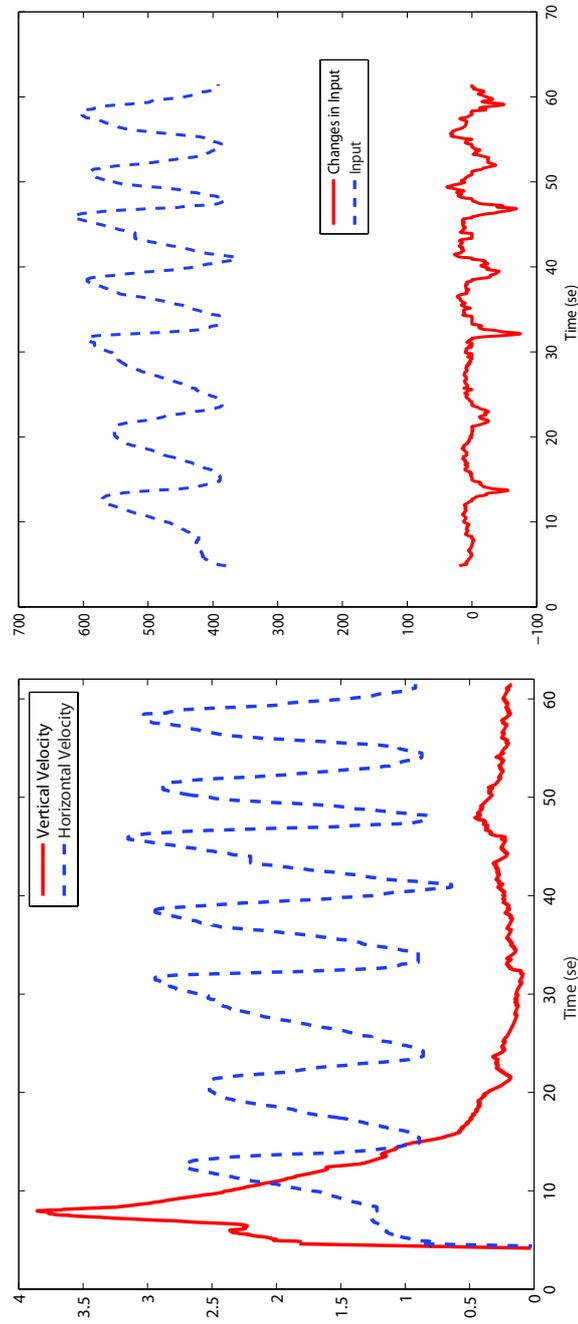


Figure 6.19: Time-series of the velocity, input (only in the horizontal direction, i.e., x) and changes in the input where the reading mode is not active. (Left) Plots of the lens' velocity in the text browser. (Right) The user's mouse input (in the x direction) and changes in the input. The user is highly active during the task and total sum of changes is 13663 unit ($m = 10$ kg, $k = 10$ kg s^{-1} , $k' = 10$ kg s^{-1} , $b = 1$ kg s^{-1} and $c = 3$).

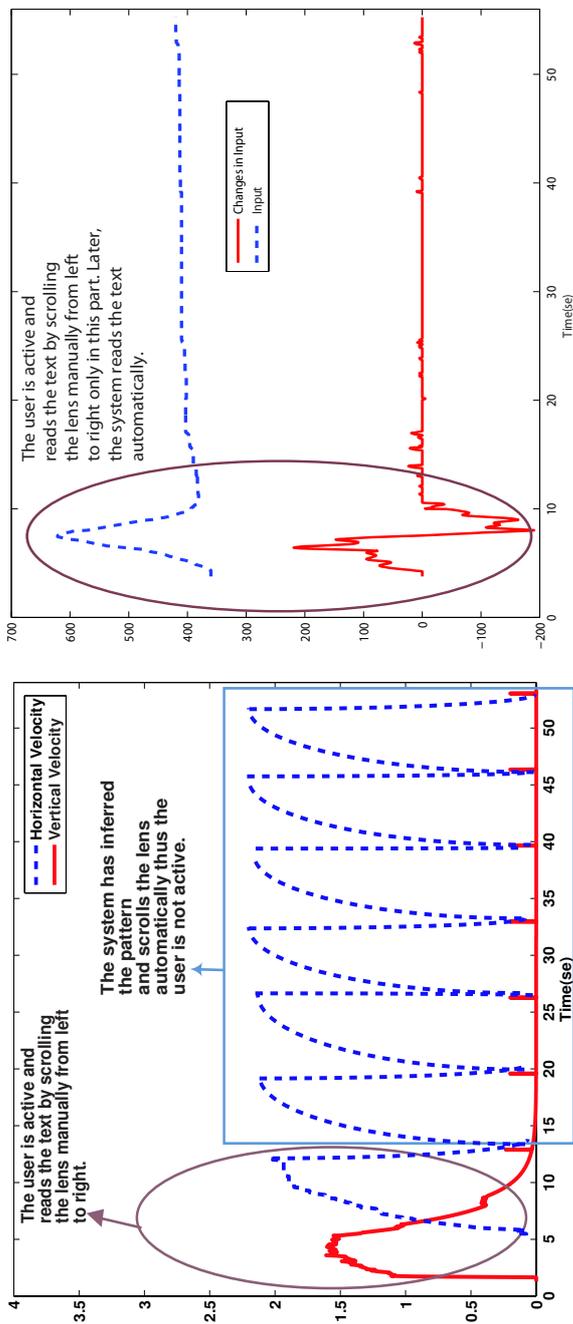


Figure 6.20: Time-series of the velocity, input (only in the horizontal direction, i.e., x) and changes in the input where the reading mode is not active. (Left) Plots of the lens' velocity in the text browser. The user is active only in the first 12 (se) and during this time the system infers the reading pattern and starts the reading mode. Then the lens scrolls from left to right with the highest DOM. Speed of scroll in the y direction only changes to a non-zero value when the lens moves to the next line and the speed in the x direction goes to zero end of each of line and increases gradually in the next line. (Right) The user's mouse input and changes in the input. Total sum of changes is 572 unit ($m = 10$ kg, $k = 10$ kg s^{-1} , $k' = 10$ kg s^{-1} , $b = 1$ kg s^{-1} and $c = 3$).

6.4.3 Inputs as Reference Signals

Given the inferred user task, the controller behaviour should be designed to support the user by enabling them to complete the task with as little effort as possible. This can include changing the interpretation of the inputs to being reference values, rather than direct control actions (see Section 5.4.3). For example, if the classifier infers that the user is in the reading mode (from equation (6.15)), then the controller automatically scrolls the lens from left to right and moves to the next line smoothly, rather than the user having to do this (see Figures 6.17 and 6.18). Any left–right movement of the mouse now controls the reference reading speed that the reading mode controller is trying to achieve, i.e., the controller not only maintains the control mode automatically but also the desired speed the user wants to read the text.

In a simple experiment we asked a user to read a French paragraph in the text without the reading mode and we asked another user to do the task with the active reading mode. We have shown these users' activities in Figure 6.20 using equations (5.22) and (5.21) on page 129. Where the reading mode is active the user's activity is much higher than the task with the disabled reading mode.

Similarly in other modes of control the system can reinterpret input as browsing speed, or as the position the user is aiming to magnify it (see Figures 6.13). Depending on the input behaviour and mode of control, which is calculated from equation (6.15), the user can control v_{ref} , x_{ref} or reading speed manually and the controller maintains the desired velocity, position or reading speed automatically and complete the task for the user. A probabilistic classification can be used to calculate the likelihood of being one of these reference values defined as R according to the joint probability of the input, X , and control mode, $Mode$. From Bayes' law, it can be written as below:

$$\begin{aligned}
 P(R | X, Mode) &= \frac{P(X | R, Mode)P(R | Mode)}{P(X | Mode)} && \text{where} \\
 P(R | Mode) &= \frac{P(R)P(Mode | R)}{P(Mode)} && (6.16)
 \end{aligned}$$

where $P(X | Mode)$, $P(Mode | R)$ and $P(X | R, Mode)$ can be identified from

experimental data from test users. Then, the controller in mode switching uses state feedback to augment control behaviour, by making the state to move towards the reference value R .

While the user performs the various tasks, his/her inputs, have different meanings (interpreted as different reference inputs) and s/he switches between control modes automatically, but that the transitions are always smooth and natural and the user is often not even aware that his/her movements are having a different effect in the different modes; because the offset variables are set such that to cancel out the input provided by the user at the point they enter new control mode and after transition the offset values gradually reset to a more sustainable position.

6.4.4 Discussion

The advent of new virtual media and visualisation means that technology offers not only new tools but also the prospect of entirely new ways of developing work in virtual space. McCullough (1998) states

what good are computers, except perhaps for mundane documentation, if you cannot even touch your work? The fact that traditional craft endures at all is because it satisfies some deep need for direct experience and most computers are not yet providing that experience.

An applied artists' instinctive grasp of constructing and visualising in three dimensions, their spatial thinking and sense of touch are integral to their process of creativity. Makers combine all their sensory modalities, such as sight, hand motions and gestures, and sound both to explore and bring intended qualities to the object they are making. *The process is open and evolving: results can only be achieved through ongoing dialogue between the maker, materials and process* (Dormer, 1994).

A significant disadvantage of focus-in-context techniques is for the user, it is impossible to see or feel the context before magnifying it; because the context is too small and far from the viewpoint. This lack of knowledge about detail of context before targeting limits the usefulness of the visual display for the

duration of the input; as the user is moving the pointer, s/he is unable to clearly see its detail. In the next section we use multimodality as a possible solution for this problem in searching and feeling a particular language in a multilingual document.

6.5 Language Identification System

Language classification consists of two major stages. From Figure 6.21 we see at the top we have the modeling stage. During this stage, the language-specific features of a text are learned and stored in a model. First, as can be seen on the upper left-hand side in this figure, the distinctive features for each language in a multi-lingual corpus are determined and stored in a language model. Later, seen on the upper right-hand side, the features of a specific text are determined and stored in a document model. In this application a language model based on partial predictive matching (Bell et al., 1990) is used to calculate the probability of the letter, l , through a conditional probability distribution $P(\text{letter} \mid \text{prefix})$, which specifies the view about future possible value of l , conditional upon the truth of that particular description *prefix* on a per-word basis. Then a tree with probability information is generated from a corpus (Williamson and Murray-Smith, 2005a). In our application these trees are built from short texts collected from *BBC* and *Le Monde* news web-sites in English and French (only a few paragraphs). For simplicity no grammar or word-level model is used, although this would be likely to improve performance significantly (Leshner and Rinkus, 2002).

At the bottom of the Figure 6.21, the classification stage is shown. During this stage, a word (the user is pointing to) of an untrained text in a document is compared to these trained language models. The language model which is the most similar to the language of this word is then selected, and represents the language of the word the user has pointed to. The actual comparison method depends on the classification technique used.

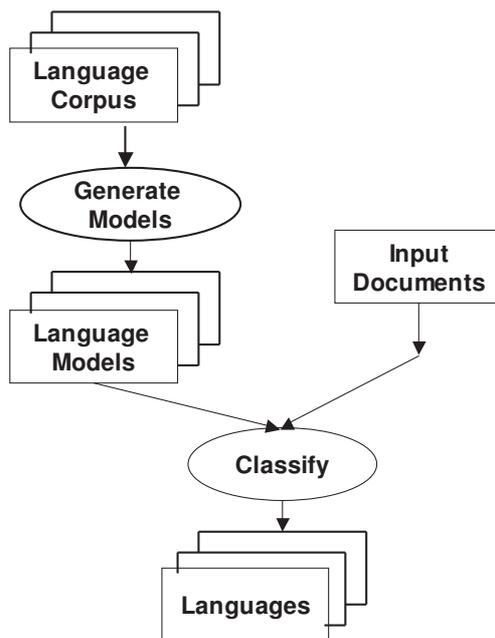


Figure 6.21: The major stages of language identification system. (Top-left) The distinctive features for each language in a multilingual corpus are determined and stored in a language model tree. (Top-right) The word the user is pointing to in an untrained text is compared to the language models during the classification stage. The language model, which is the most similar to this word is then selected.

6.5.1 Language Prediction

Prediction in this application is done using Bayes' Law to infer the most probable language given text from a document.

$$P(\text{Language} \mid \text{Word}) = \frac{P(\text{Language}) \cdot P(\text{Word} \mid \text{Language})}{P(\text{Word})} \quad (6.17)$$

The document we have considered in this applications contains sentences and paragraphs both in English and French. When the user is scrolling over the text the application provides a virtual window (with the size of the lens' width, which is dynamic and adapts with any change to the DOM) around the cursor (Figure 6.13). Then the probabilistic language models calculate the probabilities of all words in the window in each language. For example, for only two words, w_1 and w_2 in the window, we have:

$$P(\text{Language} \mid w_1, w_2) = P(w_1, w_2 \mid \text{Language}) \cdot P(\text{Language}) / P(w_1, w_2) \quad (6.18)$$

As we have made the simplifying assumption that words in the window are independent, we can write the generalised form of equation (6.18) as below:

$$P(\text{Language} \mid \text{Window}) = \left[\prod_{i=1}^{i=n} \frac{P(w_i \mid \text{Language})}{P(w_i)} \right] P(\text{Language})$$

n is window size, $\forall i = 1 \text{ to } n \quad w_i \in \text{Window}$ (6.19)

Thus, we infer the language from a number of words from a document contained by the fisheye lens.

6.6 Language Model and Granular Synthesis Feedback

As an intuitive model of the sonification process, we can imagine the words in the text to be embossed on the surface. Similar to Section 5.6 we simulate this model in our implementation by drawing an audio sample and placing that in an audio buffer, as each word belongs to a certain class of language “hits” the lens. This technique is a form of granular synthesis; (Williamson and Murray-Smith, 2005b) gives other examples of granular synthesis in interaction contexts. A real world analogy would be the perception of continuous levels of radiation via frequency of discrete pulses from a Geiger counter; here the continuous variable is the word flow rate in a specific language.

At a higher rate-of-scroll the acoustic response of the system, e.g., sampling frequency and volume of the audio sample decreases and provides the sense of distance to the text. At lower rates-of-scroll the sampling frequency and volume of the audio increases and the user feels he is getting closer to the text. Furthermore, the volume and audio frequency are inversely related to the rate of scroll, thus the audio texture as we pass over the text gives both an impression of the language of the text, as well as the speed at which we are passing it.

Similar to (Williamson and Murray-Smith, 2005b), the sonification technique can be extended to language recognition. We can sonify a probabilistic language recogniser by associating each language model with a source waveform, and each

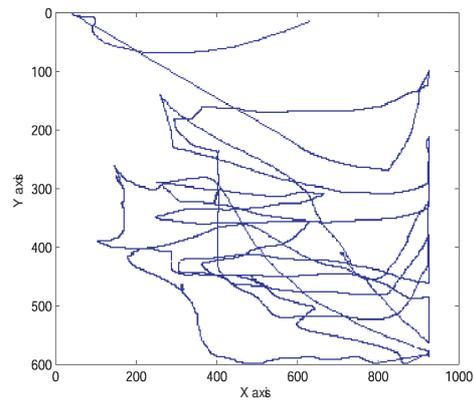
model’s output probability then directly maps to the probability of drawing a grain from the source corresponding to that model (Figures 6.13(d) and 6.13(e)). The temporal distribution of grains inside the source waveforms maps to the probability of the language of the words inside the virtual window. The overall grain density is dynamic throughout the sonification when the user scrolls over the text. In practice, during the searching mode this produces a sound that’s unclear when text features are blurred and the DOM is in the minimum level, and it means the information entropy inside the virtual window around the cursor is high. These features resolve to a clear, distinct sound as system’s mode switches to the targeting. The sonification’s primary effect is to display the current goal distribution’s entropy, i.e., language, audio and text content.

The concept of entropy in information theory describes the level of uncertainty of a random variable. An alternative way to look at this is to talk about how much information is carried by the signal. For example, in an English text, encoded as a string of letters, spaces, and punctuation the signal is a string of characters. The letter frequency for different characters is different, and we cannot perfectly predict what the next character will be in the string: it is, to some degree, ‘random’. Entropy is a measure of this randomness and was suggested by [Shannon \(1948\)](#).

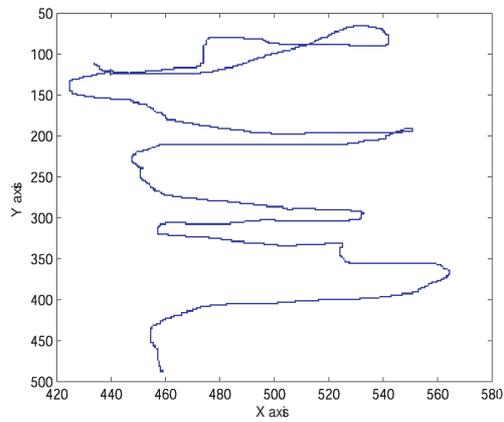
Thus model-based behaviour in this task couples the user’s input (speed of scroll) to the visualisation technique via the dynamics and the focus-in-context method couples detail-in-context to audio samples via the language identification system (Figure 6.13(a)). The next section presents an example application for browsing a document to highlight the ideas discussed and explored in the previous sections.

6.7 Example Application – A Multimodal Document Browser

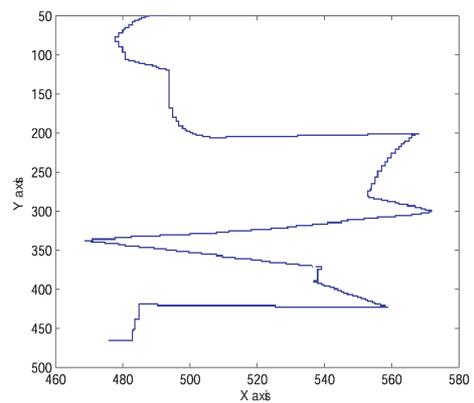
We presented a 5 page scientific document in English and a paragraph, a Figure caption and few sentences in French. The object study was conducted



(a) The application with scroll bar and mouse input.

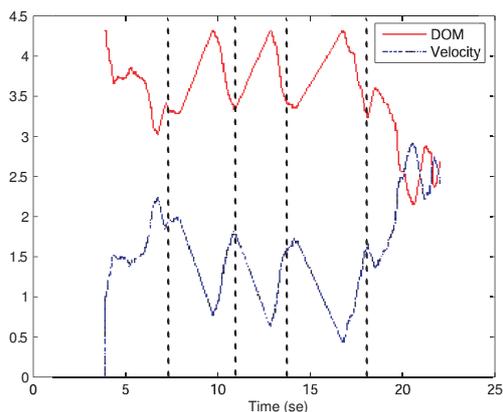


(b) The application with Focus in Context method and mouse input.

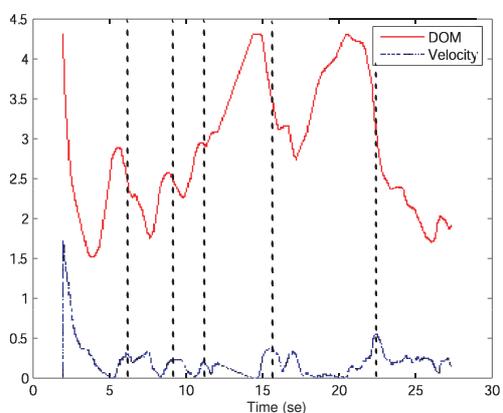


(c) The application with Focus in Context method and tilt inputs.

Figure 6.22: The user's trace in 3 applications with different input methods in searching for French sections in the document. Note that the coordinate centre is in top-left corner and the user has scrolled down.



(a) Browsing the text with mouse.

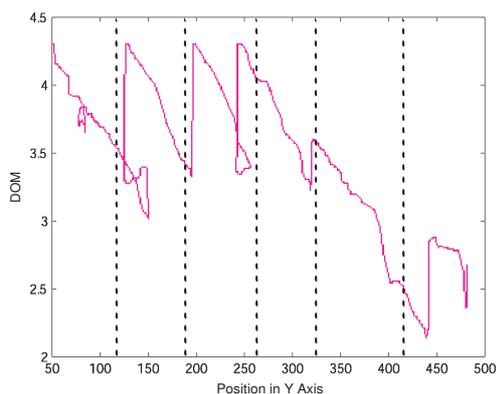


(b) Browsing the text with accelerometer.

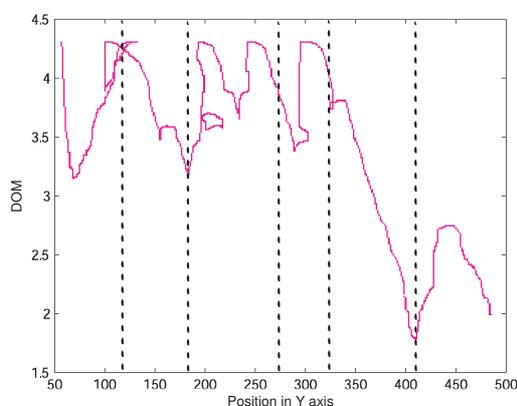
Figure 6.23: Changes in DOM and velocity versus time in searching for French sections in the document using mouse and accelerometer. In (a) the velocity has raised above a threshold around time= 7, 11 and 14 (se) and DOM has smoothly decreased. In (b) this increase in velocity happens around time = 7, 9, 11, 16, and 23 (se).

with a number of users with university education and basic knowledge of French and English (both English and French were their second or third language). All participants were new to the accelerometer but all were able to use it for browsing and scrolling after few minutes practice. In this experiment accuracy was emphasised over speed.

Participants were asked to work with the document browser using scroll bar, mouse and accelerometer and browse the multilingual document and stop over the French sections and click over them. They were given time to familiarise themselves with the system, and the specific document. The results in Figure 6.22 highlight the different navigation styles of the different interfaces and input me-



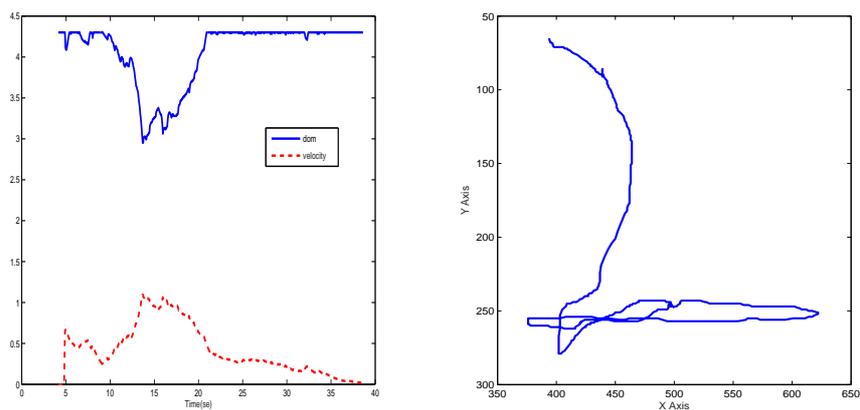
(a) Browsing the text with mouse.



(b) Browsing the text with accelerometer.

Figure 6.24: Changes in DOM versus position in finding French sections in the document around pixels 120, 190, 270, 330, and 420 using mouse and accelerometer. In (b) targets around pixels 120 and 270 are perceived but are missed by the user and the user lands almost 50 pixels after the position of the original target.

thods. With the scroll bar approach the user is in discrete movement between the text and the scroll bar to find the French sections in the document, and there was no use of zooming for an overview because the scale of the document was in full zoom and readable for users with normal eyesight. The position of the cursor at the beginning of the line (on the left) is zero and over the scroll bar (on the right) is 900 thus in this task for reading the text the mouse as well as eyes have to constantly scan from the scroll bar on the right (which we are controlling with the mouse thus need to look at) to the start of the text on the left. The feedback of the moving scroll bar can be quite small, hence it is easy to miss even if the user is looking at the text, which, given the most important information is on the left of the screen, it is highly unlikely the user will be (Brewster et al., 1994).



(a) Time-series of velocity and DOM.

(b) The user's trace in the document.

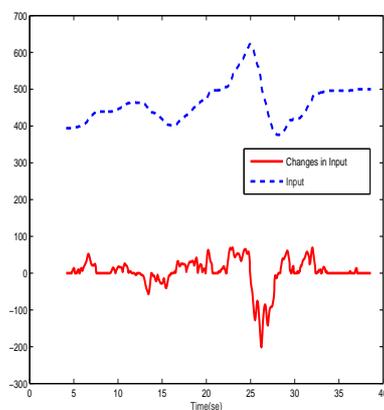
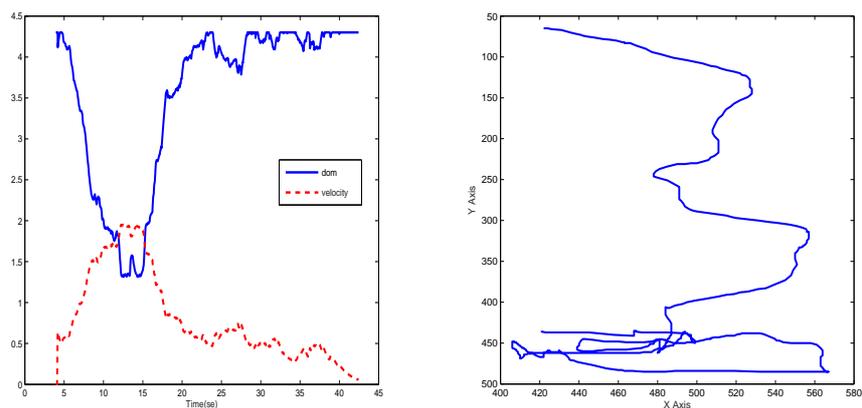
(c) User's mouse input and changes in input.
Total sum of changes is 763 unit.

Figure 6.25: Looking for a French paragraph around pixel 310 using mouse. A user is doing the task in visual only application.

With the two Focus in Context implementations the user had smoother navigation, which also included smooth changes in the DOM (See Figure 6.23). If the velocity rises above a threshold the degree of magnification smoothly decreases and the reading mode switches automatically to the searching mode, for instance in Figure 6.23(a) this has happened around $t=7, 11$ and 14 seconds. Therefore the velocity of the input device provides a smooth switch between different modes of control (See Figure 6.23(b) for the similar effect with the accelerometer). Figure 6.24 presents how the distortion level has changed when the user has found the French sections in the document, stopped for a brief check and clicked over the text. The French sections are around pixels: 120, 190, 270, 330, and 420



(a) Time-series of velocity and DOM.

(b) The user's trace in the document.

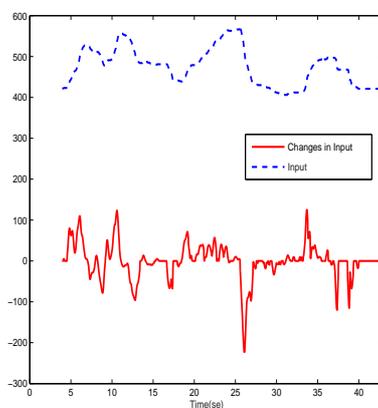
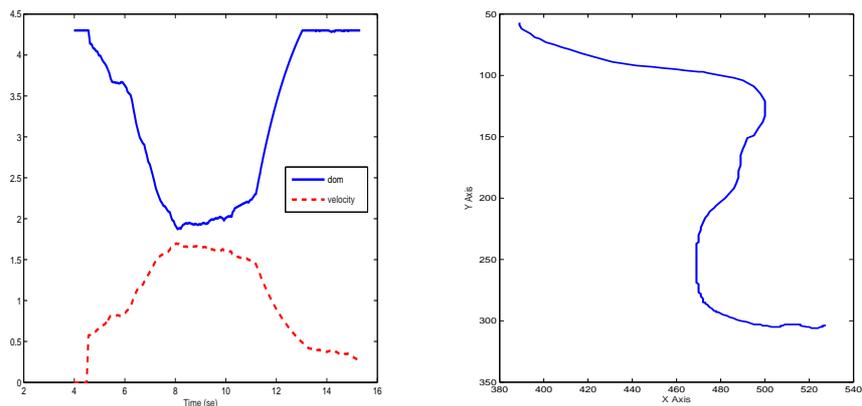
(c) User's mouse input and changes in input.
Total sum of changes is 876 unit.

Figure 6.26: Looking for a French paragraph around pixel 440 using mouse. A user is doing the task in visual only application.

and in both mouse and accelerometer input we see the user has found most of sonically highlighted sections. Users in the group, interacting with the accelerometer, commented that if they were involved with other tasks, (answering the phone, doing a task on the desktop, and so forth) they would prefer the mouse or touch-screen because they imagined it would be difficult to stay in the desired position in the document with a tilt sensor. As a temporary solution we let the users toggle tilt on and off during the task by pressing a button on the PDA. But using a classifier or a more complex controller that responds to only intended angles of tilt as suggested in Chapter 5, will be more convincing solutions for this problem.



(a) Time-series of velocity and DOM.

(b) The user's trace in the document.

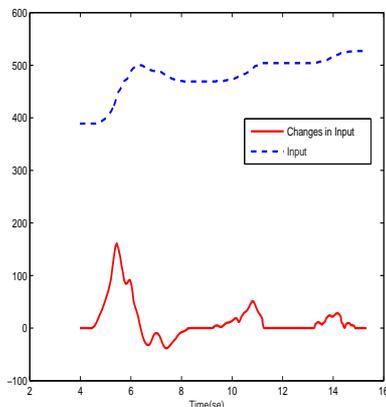
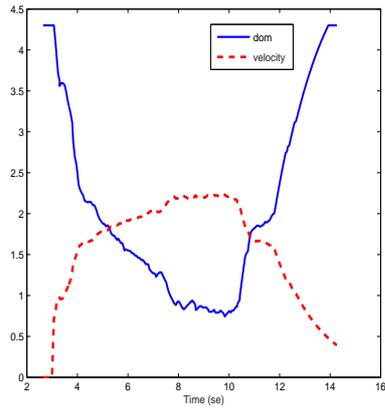
(c) User's mouse input and changes in input.
Total sum of changes is 211 unit.

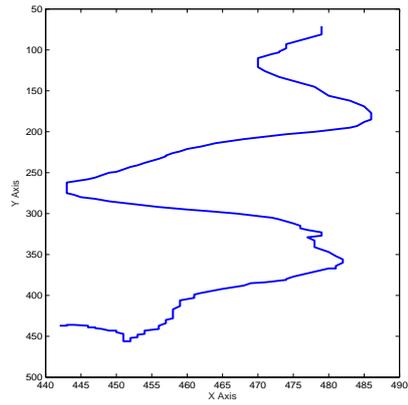
Figure 6.27: Looking for a French paragraph around pixel 310 using mouse. A user is doing the task in audio/visual application.

Additionally in this task as an example we removed the targeting mode and asked a user to do the experiment without this control mode using tilt input. Fluctuations in the results (Figure 6.29) indicate that controlling the DOM is difficult, and hunting behaviour appears when the user tries to stop over the French sections. He overshoots the targets and has to go back and adjust his behaviour to compensate, which causes decreases in the DOM again.

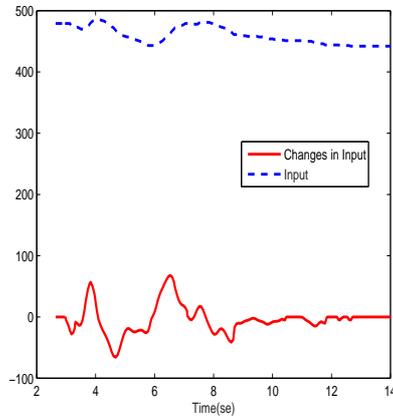
To compare the efficiency of granular synthesis feedback as an extra modality beside visual feedback versus a visual feedback only we asked two individuals to work with the system and find two different targets, two French paragraphs, with and without audio feedback using only mouse. Figures 6.25 and 6.27 show time-



(a) Time-series of velocity and DOM.



(b) The user's trace in the document.

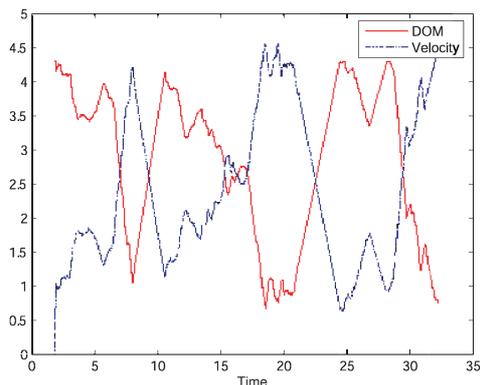


(c) User's mouse input and changes in input.
Total sum of changes is 187 unit.

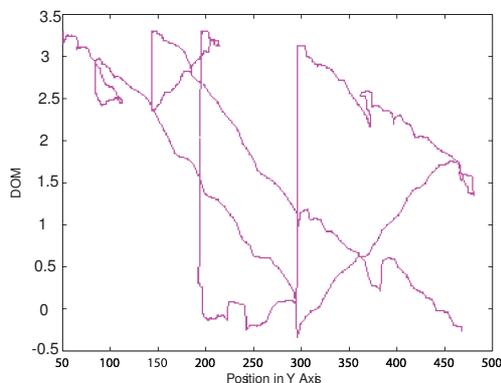
Figure 6.28: Looking for a French paragraph around pixel 440 using mouse. A user is doing the task in audio/visual application.

series of velocity and DOM, the users' activities and traces in the task, where the French paragraph is located around pixels 310. The user in audio/visual task has been faster than the user interacting with only visual display. Furthermore the cost of interaction in audio/visual one is much smaller than visual only. Locating another French paragraph around pixel 440 confirms the previous results (see Figures 6.26 and 6.28).

In a different experiment we asked four users to browse the document in two versions of the application using mouse and tilt sensor: (a) tilt control with audio feedback, no visual display (the user did the experiment blindfolded), and (b) mouse control with audio feedback, no visual display. Figure 6.30 presents a user's

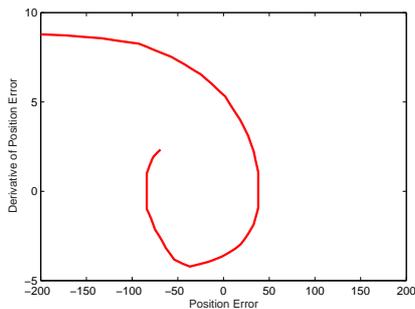


(a) DOM and velocity versus time.

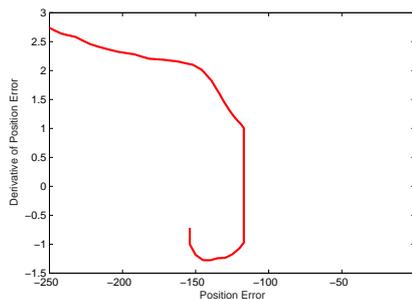


(b) DOM versus position.

Figure 6.29: The hunting effect appears after omitting the targeting control mode in tilt-controlled document browser around pixel 200, 240, 290 and 430.



(a) Mouse-controlled application.



(b) Tilt-controlled application.

Figure 6.30: Phase plots of two users who are targeting the second French paragraph in the document blindfolded using mouse and accelerometer.

phase plots while browsing the document, after being given the instruction “Find Second French Paragraph”. The results show that the audio cue was sufficient for the user to locate the target but they had stopped few pixels after the location of the original target thus they had to scroll back and return to the target. The only

difference here is the targeting error between the tilt-controlled application and mouse-controlled one; this error is slightly bigger in tilt-controlled application, which may prove some users' complain about the interface. They said the tilt sensor is sensitive to hand motion and they cannot easily control their targeting in the document. In both applications users found sonification useful in sensing different languages.

6.8 Conclusions and Summary

We presented a floating ball model as an example of how the dynamic approach can be used in designing interaction. This chapter brings together dynamics and probability theory along with multimodality in designing interaction.

6.8.1 Dynamics and Probability theory

The state-space presentation of the floating elastic ball (combination of mass, spring and viscous effects) coupled the user's intention to the visualisation technique via only a two degrees of freedom input. We demonstrated the applicability of the approach by implementing the fisheye lens for a text browsing system controlled with an accelerometer, or a mouse. We illustrated the behaviour of different interfaces by plotting users' trajectories as time-series.

A general probabilistic framework was presented for a multimodal (visual /audio feedback) model-based (e.g., floating elastic ball) text browser based on the fisheye lens developed by the state-space model. We showed the classification of the user behaviour being used to switch the control mode to one of four: states no-action, reading, searching and targeting. A probabilistic classification model calculated the likelihood of being in one of these four browsing behaviours according to the joint probability of the input and output time-series. Then the recognised mode was coupled to the visualisation parameters, where the control mode changed the size and shape of the lens, and the controller provided the DOM, position and speed of the lens.

6.8.2 Reference Signals as Inputs

It was shown that in control systems the controller can support the user to complete the task with less effort by changing the interpretation of the inputs to being reference values, rather than control commands. A probabilistic classification is used to calculate the likelihood of being in one of the browsing modes, i.e., no action, reading, searching and targeting according to the input and output time-series and switches to the mode with the maximum likelihood. For example, we showed that when the user is searching for French text in a multilingual document and he feels that he is over it he may stop and start reading the text. Spending a few milliseconds scrolling the lens from left to right and moving to the next line is enough for the classifier to infer that the user is in the reading mode. After mode transition, another probabilistic classification is used to calculate the likelihood of being some reference values according to the joint probability of the input and control mode. In the multilingual text browsing example, after switching to the reading mode, any left-right input from the user controls the reference reading speed. This simple example provided in this chapter illustrates that the user is far less active in the reading mode when the controller changes the interpretation of the input and completes the task for the user.

In this example application the user switches among different control modes and his/her inputs are interpreted as different reference inputs, but the transition is smooth and natural, and the user is often not even aware that their movements are having a different effect in the different modes.

6.8.3 Multimodal Interaction

Multimodality is a possible solution for hearing the context before magnifying that. As an example application we investigated the problem of searching and feeling a particular language in a multilingual document. Sonifying each language in the document allowed users to locate and hear targets (here the idea was searching and locating French written texts) without looking at the screen. Furthermore, we compared the efficiency of audio feedback as an extra modality

beside visual feedback versus visual feedback only system. The users' activities in the multimodal system were lower than unimodal system. It suggests that transferring information sonically will be a powerful complement to visual interfaces and supports intermittent interaction where the motion limits the usefulness of the small screen for the duration of input and the user carries on with other activities. Thus there would be an application for this system in mobile phones, small screen computing devices and shared displays, too.

The general probabilistic framework presented in this chapter brings the results in chapter 4, usefulness of quickened displays and predicting the user behaviour, and chapter 5, importance of multimodality in the intermittent interaction, together along with the probabilistic model for classifying human behaviour in browsing tasks suggested in this chapter.

In the next chapter we present a general overview of the thesis and summarise the work.

Chapter 7

Conclusions and Future Work

“The reward for work well done is the opportunity to do more work.”

Jonas Salk, MD

In this final Chapter we present a summary and discussion of the contributions of this dissertation, concluding remarks and note some potential avenues for future work.

In this thesis our focus has been on setting out a theoretical basis for the design of interactive systems on portable computing devices. This work has presented a general framework to achieve this goal as well as exploring novel areas in portable computational appliances. Concrete techniques, developed real working interfaces allowed us to collect detailed real data from users testing the prototype we developed in the thesis.

7.1 Contributions of the Thesis

This thesis addresses a theoretical basis for the design of interactive systems on small, portable computing devices. This framework includes current human-computer interfaces; it also reveals a number of unexplored areas in this context and human–mobile device interaction. Concrete techniques for applying the concepts have been discussed for example applications, in both auditory and graphical user interfaces. Working interfaces which embody these novel interaction concepts can be created with these techniques. We view this approach in

terms of a framework for specification and analysis, rather than a set of predefined techniques.

7.1.1 *Model-Based Target Sonification*

In Chapter 4, the major contribution made to the auditory displays and localisation and selection on mobile devices using tilt sensor. The experiments in this Chapter provide better understanding about users' navigation and search behaviour in audio displays. For example, in conditions where the vibration (haptic) feedback is included, the sweep search pattern is combined with circular movements around the vibration source. In these conditions where the audio feedback guides the user toward the target, and he feels that he is close enough to the target, then he starts looking for the vibration source; because a clear on/off feedback at the edge of the vibration indicates that the target has been achieved. Also, results in this Chapter show that while the interaction lacks enough feedback information the user uses his/her prior knowledge learnt from training session or from other activities, for example, left-right reading patterns and it affects their browsing behaviour.

Next, results in this Chapter provide evidence on usefulness of quickened displays and advantages and disadvantages of different audio/haptic patterns. It is highlighted that over-interpreting the quickened signal, especially in the Doppler condition is a common risk associated with quickened displays. Also, this Chapter is concerned with the predictive feedback based on human operator modeling in continuous tracking tasks, to tie together feedback mechanism of interactive auditory displays.

7.1.2 *Tilt-Controlled Zooming User Interfaces*

The importance of continuous control and modeling, which emerges to an extent in Chapter 4 is the main focus of Chapters 5 and 6, which investigate the dynamic systems approach to the design of continuous interaction interfaces. The contribution Chapter 5 makes is the development one of the first tilt controlled speed-dependent automatic zooming (SDAZ) on a PDA. Tilt-controlled SDAZ

is used for browsing long documents based on a state-space implementation of a flying object metaphor (combinations of springs, masses and damping effects) with pseudo autopilot modes. We suggest that the state-space approach has the potential to provide a general framework for development, analysis and optimisation of interfaces which induce complex, but convenient coupling among multiple states, in order to cope with one degree of freedom input.

In the general approach (i.e., interaction with higher degrees of freedom input and many controlled variables) this model makes tuning and calibration a lot easier for the system itself or when the system is coupled with the time delay and lag-lead-dynamics of human control behaviour; because proper settings, which make the closed-loop system-human stable, can only be found by observing the behaviour of the simulated system before the actual implementation. For example, by modeling the human operator like a gain and delay, plotting the Bode plots and calculating the activity of the user using a performance function, we find the most satisfying setting for the user and the system and this suggests that control model supports closed-loop dynamics. We show that having augmented velocity and position control help the user to perform more accurate browsing and landing over the targets. Interpreting inputs as reference values provides switching among different control modes, but the mode transition is designed to be smooth and natural and the user is not aware that their hand movements have different effects in different modes.

The tilt-controlled SDAZ has its own pros and cons. It facilitates single-handed control of the application without obscuring the screen, however it may cause irritating reflections from the screen. This does not happen in the touch-screen version. Thus the user can stop interaction with the device by simply taking the stylus off the screen. We improve this by auto-calibrating the device according to the comfortable starting angle (equilibrium point) of the tilt-sensor in the user's palm.

The audio/haptic feedback representation of the speed-zoom coupling involved in speed-dependent automatic zooming is the other contribution this Chapter makes. We implement and demonstrate the multimodal tilt-controlled SDAZ in-

terface for a text browser system on the PDA instrumented with the tilt sensor. Sonifying each piece of structural information in the document lets the blindfolded users feel and sense different textures. The results show that the audio/haptic cue is sufficient for the blindfolded users to distinguish where the target is, but the users' activities in the audio and haptic only interface were higher than the visual only, most likely because the vision is leading sense. This provides a general design guideline for developers to add multimodal feedback, which is an essential component of movement-based interaction techniques and supports intermittent interaction.

7.1.3 *Multimodal Motion Controlled Focus-in-Context Method: Sensing Complex Information*

We developed a motion controlled focus-in-context visualisation method based on a pseudo-physical metaphor (a floating ball) and a state-space implementation, which also presents a general framework of how dynamic system simulation and continuous control method can be linked to multimodal feedback and probabilistic language model and support human behaviour.

Supporting the user input and completing the task automatically for the user by changing the interpretation of the inputs to being reference values, rather than control commands has been shown in a few examples in this Chapter. A probabilistic classification is used to calculate the likelihood of being in one of the browsing modes, i.e no action, reading, searching and targeting according to the input and output time-series and switches to the mode with the maximum likelihood. After mode transition another probabilistic classification is used to calculate the likelihood of being some reference values according to the joint probability of the input and control mode. As an example, we provide a multilingual text browser and how the controller supports the user input and completes the reading task the user is interested and changes interpretation of inputs after mode transition. In this example application the user switches among different control modes, but the transition is smooth and natural, and the user is often not even aware that their movements are having a different effect in the different modes.

A significant disadvantage of focus-in-context techniques is the user's knowledge about the context, for example, the language of the text is very limited when the degree of the magnification is low; because the context is too small and far from the viewpoint. In this Chapter we suggest that multimodality is a possible solution for this problem. As an example application we investigate the problem of searching and feeling a particular language in a multilingual document. Sonifying each language in the document allows users to hear and locate targets without looking at the screen. In a simple example we compare the efficiency of audio feedback as an extra modality beside visual feedback versus a visual feedback only system. The performance measure indicates that the multimodal system decreases the cost more than the unimodal system and suggests that audio/haptic feedback will be a powerful complement to visual interfaces and supports intermittent interaction, where the user can spend varying amounts of attention on interaction while carrying on with other activities.

The general probabilistic framework presented in this Chapter brings the results in Chapter 4, usefulness of quickened displays and predicting the user's behaviour, and Chapter 5, importance of multimodality in the intermittent interaction, together along with the probabilistic model for classifying human behaviour combined with audio/visual feedback in browsing tasks suggested in this Chapter.

7.2 Outlook

A more thorough exploitation of the continuous control and dynamic system approach presents a promising theoretical framework for interaction models and design principles and help create better interactive systems not only on portable computing devices but also on all range of computing systems. The availability of this solid theory for use in interactive systems, allow the incorporation of analytical tools and constructive techniques from manual and automatic control theory, probabilistic models, and machine learning techniques into the interface and integrating multimodality in a principled manner. Thus, this concrete theory

provides a wide range of possibilities for future work.

In this thesis, we provided a number of examples, where the system relies on a tight coupling between the user's perception and the action. Providing predictive feedback based on human operator modeling and taking human response delays and lags into account is one of important issues in multimodal interfaces. It provides important insight about human performance or activity in the interaction with multimodal systems, for example model-based sonification application in Chapter 4 or multimodal, model-based text browser application in Chapter 6.

In continuous dynamic interactive systems the trend is that the system is adapting to the complexity of the user behaviour rather than the user adapting himself to a system's interface. We presented a few examples of this adaptability in Chapters 5 and 6, where the controller changes the interpretation of user inputs to being reference values, rather than control commands, switches among different control modes smoothly according to these reference values without being noticed by the user and completes the task without too much effort from the user. An interesting application of control systems, which adapt themselves to the user behaviour will be interactive systems whose users have different range of expertise in the interaction with the system, novice, intermediate or expert. The objective, consequently, is to determine the most appropriate parameter settings for the dynamic system model, which make the closed-loop interaction between the system and user stable. As the user learns how to interact with the system, i.e lags and delays in muscles decrease, the system switches to the model and the controller which suits the parameters of that user more.

Chapter 6 provided a number of examples of coupling between probability theory and control theory to classify and predict user behaviour in the interaction. Probability theory gives theoretical models for the combination and classification of evidence. For example, a probabilistic classification of the likelihood of different modes of control is used to change the dynamics of the controlled system, which makes the user's task easier. The idea of probabilistic classification can be used in classifying and recognising misinterpreted and unintended inputs as we show a few examples of these inputs in Chapter 5. Implementing such a classifier

is an important step forward in designing continuous tilt-controlled interfaces and supporting intermittent interaction.

The core of this dissertation is building prototypes and addressing a theoretical basis for the design of interactive systems, which help designers to build their own interfaces based on these prototypes and run usability experiments.

7.3 Final Remarks

Research in the area of designing continuous interaction is still in its infancy. The dynamic theory driven approach to the design of interactive systems on portable computing appliances allows us to utilise the concrete analytical tools and constructive techniques from manual and automatic control theory in augmenting and complementing human capabilities in the interaction and integration of multimodality in a principled manner. From this basis, this dissertation has provided a number of contributions to the research on interaction with portable computing devices, tilt-controlled applications, audio/haptic interfaces, multimodal zooming user interfaces, and probability theory.

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Appendix A

Matlab Simulation of the Mass-Spring-Damper

Example

In this Appendix, we present the Matlab code for the mass-spring-damper example in Chapter 3 (on page 46), where position and velocity are state variables.

```
m = 10; (-mass-)
```

```
b = 3; (-spring coefficient-)
```

```
k = 0.3; (-damping coefficient-)
```

```
A = [ 0 1; -b/m -k/m]; (-state Matrix-)
```

```
B = [ 0 1/m]'; (-input matrix-)
```

```
C = [1 0]; (-output matrix-)
```

```
D = 0; (-feedthrough (or feedforward) matrix -)
```

```
x0 = [0.5 0]; (-Initial condition-)
```

```
(-In this part we generate step input with 0.1 sampling time-)
```

```
T = [0.0001:0.1:30]';
```

```
u = stepfun(T,2);
```

(-Here we use lsim Matlab command to simulate the linear state-space model and plot the results.-)

```
[z,x] = lsim(A,B,C,D,u,T,x0);  
figure(1)  
plot(T,[x(:,1) x(:,2) u])  
legend('position', 'velocity', 'Input');
```

Appendix B

Matlab Simulation of Following a Reference Signal

In this Appendix, we present the Matlab code, where position state variable follows a reference signal. It can be extended to any reference signal following for other state variables in this model.

```
-----  
clear all;  
(-state space coefficients-)  
r = 10; m = 10; rr = 10; b =3; c = 3;  
(- state-space matrices- )  
A = [ 0 1 0;  
0 -r/m 0 ;  
0 -b/m -rr/m];  
B = [ 0 1/m c/m]';  
C = [1 0 0];  
D = 0;  
(-This variable gives importance (weights) to different state variable-)  
kp = 8;  
(-We are interested to see the behaviour of the position state variable when it  
follows the reference signal.-)  
L = [1 0 0];
```

AA = A - kp*B*L; (-state Matrix-)

BB = kp*B; (-input matrix-)

CC = C; (-output matrix-)

DD = D; (-feedthrough (or feedforward) matrix -)

(-In this part we generate step input with 0.1 sampling time-)

T = [0.0001:0.1:30]';

u = stepfun(T,2);

(-Here we use lsim Matlab command to simulate the linear state-space model. -)

[y,x] = lsim(AA,BB,CC,DD,u,T);

(-Here we plot the state variables, control input and reference signal-)

figure(1)

plot(T,[x(:,1) x(:,2) x(:,3) u kp*(u-y)])

legend('Position','Velocity','Zoom', 'Reference signal', 'Control Input');

Appendix C

Bode Diagrams of Open-Loop Transfer Function in Matlab

In this Appendix, we present the Matlab code, to plot Bode plots of the open-loop transfer function for the human and controller with the setting mentioned in Section 5.4.4 (on page 139).

```
clear all;
```

```
kdok=[]; gmm=0; pmm=0; K=5; D=1
```

(– Human model transfer function, K is the gain and D is the delay–)

```
Gh=tf([K],[1,D]);
```

(– Controller transfer function, a1 and b1 are coefficients in the state-space model–)

```
a1 = 1;
```

```
b1 = 0.01;
```

```
Gc=tf([b1],[1 a1]);
```

(–Open loop transfer function for human operator and controller–)

```
Gopenloop=Gh*Gc;
```

(–Phase and Gain margins are calculated and plotted–)

```

[Gm, Pm, Wcg, Wcp] = margin(Gopenloop);
margin(Gopenloop);
GmdB=20*log10(Gm);
[ GmdB Pm Wcg/(2 * pi) Wcp/(2 * pi) ];

    if GmdB >0 & Pm > 0
kdok=[kdok; [a1 b1]];
if GmdB >= gmm & Pm >= pmm
kc=[a1 b1];
gmm=GmdB;
pmm=Pm;
end;
end;
```

Appendix D

Online Materials

Online materials which accompany this thesis are briefly listed below. The up-to-date videos, publications, source codes, and the electronic version of this thesis are available online at <http://www.hamilton.ie/parisa/>.

D.1 Materials

D.1.1 Model-based Target Sonification on Small Screen Devices: Perception and Action

- Experiment I:
C++ source code for this experiment, which include training and main applications in four different audio conditions is available at http://www.hamilton.ie/parisa/Parisa_files/Experiment_I.zip
- Experiment II:
C++ source code for this experiment, which include training and main applications in three different audio conditions is available at http://www.hamilton.ie/parisa/Parisa_files/Experiment_II.zip

D.1.2 Tilt-Controlled Zooming User Interfaces on Mobile Devices

- Tilt-controlled Speed Dependent Automatic Zooming:
C++ source code for this application is available directly at
http://www.hamilton.ie/parisa/Parisa_files/SDAZ-Tilt.zip
- Multimodal Tilt-controlled Speed Dependent Automatic Zooming:
C++ source code for this application is available directly at
http://www.hamilton.ie/parisa/Parisa_files/SDAZ-Tilt-Sound.zip
- Stylus-controlled Speed Dependent Automatic Zooming:
C++ source code for this application is available directly at
http://www.hamilton.ie/parisa/Parisa_files/SDAZ-Touch.zip

D.1.3 Multimodal Motion Controlled Focus-in-Context Method: Sensing Complex Information

C++ source code for this application is available directly at
[http://www.hamilton.ie/parisa/Parisa_files/F+C\(language,sound\).zip](http://www.hamilton.ie/parisa/Parisa_files/F+C(language,sound).zip)